

## EE7500: Advanced Electromagnetics — Homework Assignment 2

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Released: 25 Mar, due: 14 Apr 2026

Total: 100 points

*Typed solutions (e.g. LaTeX) are highly preferred to handwritten & scanned submissions.*

### Academic Integrity:

- This homework must be completed and submitted individually.
- If you discuss the general approach with classmates, [acknowledge them by name](#) in your submission (no penalty for doing so).
- If you use AI tools (ChatGPT, Claude, etc.), clearly state which problems, how you used them, and the specific prompts. *If you use machine learning tools as a black box without building your own understanding, it is only the machines that will learn—not you.*
- Your PDF must begin with: “I hereby certify that this submission was generated by me with the highest academic integrity — *your name*”
- Submit: PDF with all solutions/plots, and MATLAB .m files for computational problems as one consolidated zip file. MATLAB files must be commented and named `questionXX.m`; the PDF filename must be your roll number.

### 1. Small Current Loop and the Duality Theorem

A small circular loop of electric current  $I_0$  with radius  $a \ll \lambda$  lies in the  $xy$ -plane, centered at the origin. Its magnetic dipole moment is  $m = I_0 \pi a^2$  (SI units:  $\text{A m}^2$ ).

(a) (6 points) Starting from the vector potential integral

$$\mathbf{A}(\mathbf{r}) = \frac{\mu I_0 a}{4\pi} \int_0^{2\pi} \hat{\phi}' \frac{e^{-jkR}}{R} d\phi', \quad R = |\mathbf{r} - \mathbf{r}'|,$$

use the far-field approximation  $R \approx r - a \sin \theta \cos(\phi - \phi')$  for amplitude and phase, and the small-loop condition  $ka \ll 1$ , to show that

$$\mathbf{A} = \frac{j\mu k m \sin \theta}{4\pi r} e^{-jkr} \hat{\phi}.$$

From this, derive the far-field  $H_\theta$  and  $E_\phi$ .

*Hint:* After expanding  $e^{jka \sin \theta \cos(\phi - \phi')} \approx 1 + jka \sin \theta \cos(\phi - \phi')$ , the zeroth-order integral vanishes and you will need  $\int_0^{2\pi} \hat{\phi}' \cos(\phi - \phi') d\phi' = \pi \hat{\phi}$ , where  $\hat{\phi}' = (-\sin \phi', \cos \phi', 0)$  and  $\hat{\phi} = (-\sin \phi, \cos \phi, 0)$ .

(b) (6 points) Recall the far-field of a Hertz electric dipole (current  $I_0$ , length  $\ell$ ):

$$E_\theta = j\eta \frac{kI_0 \ell \sin \theta}{4\pi r} e^{-jkr}, \quad H_\phi = \frac{E_\theta}{\eta}.$$

Apply the duality substitution ( $\mathbf{E}_A \rightarrow \mathbf{H}_F$ ,  $\mathbf{H}_A \rightarrow -\mathbf{E}_F$ ,  $\eta \rightarrow 1/\eta$ ,  $I_0 \ell \rightarrow I_m \ell$ ) to obtain  $H_\theta$  and  $E_\phi$  for a magnetic dipole  $\mathbf{M} = I_m \ell \hat{z}$ . By comparing with the loop results of part (a), find the equivalence between the small loop and the magnetic dipole currents, and also verify dimensional consistency.

### 2. Uniqueness Theorem — The Critical Role of Loss

(a) (4 points) Suppose two solutions  $\{\mathbf{E}_1, \mathbf{H}_1\}$  and  $\{\mathbf{E}_2, \mathbf{H}_2\}$  satisfy Maxwell's equations in a bounded region  $V$  (bounded by surface  $S$ ) with the same sources  $\mathbf{J}, \mathbf{M}$  and the same tangential  $\mathbf{E}$  prescribed

on  $S$ . Define difference fields  $\delta\mathbf{E} = \mathbf{E}_1 - \mathbf{E}_2$ ,  $\delta\mathbf{H} = \mathbf{H}_1 - \mathbf{H}_2$ . Write down the complex Poynting theorem for the difference fields integrated over  $V$ , and use the boundary condition to show that

$$\oint_S (\delta\mathbf{E} \times \delta\mathbf{H}^*) \cdot d\mathbf{S} = 0.$$

Then take the real part of the volume integral form of the Poynting theorem and state what it implies.

- (b) (4 points) Identify the *one step* in the proof above that breaks down for a perfectly lossless medium (i.e.  $\epsilon'' = 0$ ,  $\mu'' = 0$ ,  $\sigma = 0$ ). Describe, with a brief physical example, a situation where fields in a lossless region are genuinely non-unique.

### 3. LTE (4G) Base Station Coverage

A 4G LTE base station (eNodeB) operates at  $f = 1.8$  GHz (LTE Band 3) with the following parameters obtained from standards and datasheets:

- Transmit power:  $P_T = 20$  W (43 dBm) [3GPP TS 36.104]
  - Base station antenna gain:  $G_T = 18$  dBi [typical sector panel antenna]
  - Mobile handset antenna gain:  $G_R = 0$  dBi (isotropic reference)
  - Radiation efficiencies:  $\eta_T = 0.90$  (base station),  $\eta_R = 0.75$  (handset with body effects)
  - Minimum required received power:  $P_{\min} = -100$  dBm [3GPP TS 36.101, §7.3]
- (a) (6 points) Using the Friis transmission equation  $P_R = P_T G_T G_R \eta_T \eta_R \left(\frac{\lambda}{4\pi R}\right)^2$ , compute the maximum coverage radius  $R$  (in km) under free-space propagation. Show all steps clearly.
- (b) (4 points) Compute the corresponding coverage area (in km<sup>2</sup>). Real-world LTE macro cells have radii of 1–50 km depending on terrain. By what approximate factor does your free-space result overestimate the practical coverage radius, and what is the primary physical reason? To answer this, assume a real-world cell radius to be 10 km. *Hint*: In part (a) we saw that the path loss factor was  $\propto R^{-2}$ . In real world scenarios this is not so, and the empirical factor is of the type  $R^{-n}$  where  $n > 2$ . Do some background reading to understand why  $n \neq 2$  and estimate it in this problem.

### 4. Antenna RCS Minimization without the Resonance Assumption

The scattered field from an antenna with load  $Z_L$  is given by (Balanis 2-127 and 2-129):

$$\mathbf{E}^s(Z_L) = \mathbf{E}^s(0) - \frac{I_s}{I_t} \frac{Z_L}{Z_L + Z_A} \mathbf{E}^t \quad (2-127)$$

$$\mathbf{E}^s(Z_L) = \mathbf{E}^s(0) - \frac{I_s}{I_t} \frac{1 + \Gamma_A}{2} \mathbf{E}^t, \quad \Gamma_A = \frac{Z_L - Z_A}{Z_L + Z_A} \quad (2-129)$$

where  $Z_A = R_A + jX_A$  is the antenna impedance,  $\mathbf{E}^s(0)$  is the scattered field under short-circuit load, and  $\mathbf{E}^t$  is the transmit-mode far field with terminal current  $I_t$ . Also use Balanis (2-131):  $I_s Z_A = 2R_A I_m^*$ , where  $I_m^*$  is the terminal current at conjugate match  $Z_L = Z_A^*$ .

- (a) (6 points) Without assuming  $X_A = 0$ , substitute  $Z_L = Z_A^*$  into (2-129) to find  $\mathbf{E}^s(Z_A^*)$ . Subtract this from the general (2-129) to arrive at a decomposition of the form

$$\mathbf{E}^s(Z_L) = \underbrace{\mathbf{E}^s(Z_A^*)}_{\text{structural}} - \underbrace{\frac{I_m^*}{I_t} \Gamma_c \mathbf{E}^t}_{\text{antenna mode}},$$

where  $\Gamma_c \equiv (Z_L - Z_A^*) / (Z_L + Z_A)$ . Show all algebra explicitly.

*Note*: Balanis uses  $\Gamma^* = (Z_L - Z_A^*) / (Z_L + Z_A^*)$ ; explain under what condition  $\Gamma_c = \Gamma^*$ .

- (b) (6 points) The RCS (from the magnitude of 2-129) in any observation direction  $(\theta_0, \phi_0)$  can be written as

$$\sigma = \left| \sqrt{\sigma_s} - (1 + \Gamma_A) \sqrt{\sigma_a} e^{j\phi_r} \right|^2,$$

where  $\sigma_s, \sigma_a$  are the structural and antenna-mode RCS, and  $\phi_r$  is their relative phase. For a fixed antenna geometry (fixed  $Z_A, \sigma_s, \sigma_a, \phi_r$ ), derive the optimal load  $Z_L$  that sets  $\sigma(\theta_0, \phi_0) = 0$ , and express it in terms of  $\alpha \equiv \sqrt{\sigma_s/\sigma_a}$  and  $\phi_r$ . State the condition on  $\alpha$  for the solution to require an active (non-passive) load.

## 5. Hertz Dipole Radiation Pattern — MATLAB

The radiation intensity of a Hertz dipole is  $U(\theta) = U_0 \sin^2 \theta$  (W/sr), independent of  $\phi$ .

**Reference:** <https://www.mathworks.com/help/matlab/ref/polarplot.html>

- (a) (4 points) **Pattern visualization.** Write a MATLAB script that plots  $U(\theta)/U_0$  in a 2D polar plot as a function of  $\theta \in [0^\circ, 360^\circ]$ , with labeled axes and a title.
- (b) (6 points) **Directivity calculation.** Write MATLAB code to numerically compute the directivity:

$$D_{\max} = \frac{4\pi U_{\max}}{P_{\text{rad}}}, \quad P_{\text{rad}} = \int_0^\pi \int_0^{2\pi} U(\theta) \sin \theta \, d\theta \, d\phi.$$

Use a fine angular grid (e.g.  $10^4$  points in  $\theta$ , uniform over  $[0, \pi]$ ). Verify numerically that  $D_{\max} = 3/2$  (confirm to at least 3 significant figures), and identify the direction(s) of maximum radiation.

**Deliverables:** MATLAB .m file with comments, the 2D polar plot with labeled axes, the numerical value of  $D_{\max}$  printed to the command window, and a 2–3 sentence summary of what the plot reveals about the Hertz dipole radiation pattern.

## 6. Quarter-Wave Monopole and Image Theory

- (a) (5 points) A quarter-wave ( $\lambda/4$ ) vertical monopole antenna is mounted on an infinite PEC ground plane. Using image theory, identify the image source, describe the equivalent problem valid for  $z > 0$ , and write down the far-field  $E_\theta$  of the monopole for  $0 \leq \theta \leq \pi/2$ . You may use the result for the far-field of a center-fed half-wave dipole in free space (total length  $\lambda/2$ , current  $I_0$ ) from existing sources without derivation.
- (b) (5 points) Given that the radiation resistance of a half-wave dipole is  $R_{\text{rad}}^{\text{dipole}} = 73 \Omega$ , find the radiation resistance  $R_{\text{rad}}^{\text{mono}}$  of the quarter-wave monopole. Provide a careful argument based on radiated power and the symmetry of the radiation pattern. *Hint:* Go to the fundamental definition of radiation resistance.

## 7. Effective Aperture and the Friis Formula

- (a) (4 points) Starting from the Friis transmission equation  $P_r = P_t G_t G_r (\lambda/4\pi R)^2$  (Balanis 2-116, lossless matched case), derive the relation  $A_e = G\lambda^2/(4\pi)$  (Balanis 2-71) by identifying the effective aperture as  $A_e \equiv P_r/S_{\text{inc}}$ , where  $S_{\text{inc}}$  is the power density incident on the receiving antenna. State clearly which antenna's gain and aperture appear in your expression.
- (b) (4 points) A half-wave dipole antenna ( $D_{\max} = 1.64$ ,  $R_{\text{rad}} = 73 \Omega$ , radiation efficiency  $\eta_{\text{rad}} = 100\%$ ) is used as a receive antenna at  $f = 500$  MHz. A plane wave with power density  $S_{\text{inc}} = 10 \mu\text{W}/\text{m}^2$  is incident from the direction of maximum gain, with matching polarization and a matched load. Compute: (i) the maximum effective aperture  $A_e$  in  $\text{cm}^2$ ; (ii) the power delivered to the matched load.

## 8. Two-Element Phased Array — MATLAB

Two isotropic point sources are placed along the  $x$ -axis, separated by  $d = \lambda/2$ . The sources carry currents  $I_1 = I$  and  $I_2 = Ie^{j\delta}$ . The array factor is:

$$\text{AF}(\phi) = 1 + e^{j(\pi \cos \phi + \delta)},$$

where  $\phi$  is the azimuth angle measured from the  $+x$  axis.

**Reference:** <https://www.mathworks.com/help/matlab/ref/polarplot.html>

- (6 points) Write a MATLAB script to compute and plot  $|\text{AF}(\phi)|$  vs.  $\phi \in [0^\circ, 360^\circ]$  as polar plots on a single figure for three cases:  $\delta = 0$  (broadside),  $\delta = -\pi/2$  (beam steered toward  $\phi = 60^\circ$ ), and  $\delta = -\pi$  (endfire toward  $\phi = 0^\circ$ ). Label each curve. For each case, state the angle(s) of maximum  $|\text{AF}|$ .
- (4 points) For the broadside case ( $\delta = 0$ ), derive the half-power beamwidth (HPBW) analytically. Verify your result numerically by finding the two half-power angles in MATLAB and confirming they match within  $1^\circ$ .

**Deliverables:** MATLAB .m file with comments, the polar plot with all three curves labeled, and the numerically determined HPBW printed to the command window.

## 9. Near-Field vs. Far-Field Transition — MATLAB

The  $H_\phi$  field of a Hertz dipole (in the  $\theta = 90^\circ$  plane,  $\sin \theta = 1$ ) is:

$$H_\phi = \underbrace{\frac{kI_0\ell}{4\pi r}}_{\text{far-field term}} \quad j \quad + \quad \underbrace{\frac{I_0\ell}{4\pi r^2}}_{\text{near-field term}},$$

with far-field amplitude  $|H_{\text{FF}}| = kI_0\ell/(4\pi r)$  and near-field amplitude  $|H_{\text{NF}}| = I_0\ell/(4\pi r^2)$ .

- (5 points) Write a MATLAB script that plots  $|H_{\text{FF}}|$  and  $|H_{\text{NF}}|$  (normalized to  $I_0\ell/(4\pi)$ , so the two plotted quantities are  $k/r = kr/r^2$  and  $1/r^2$ ) on a single log-log plot as a function of  $kr$  over the range  $kr \in [0.01, 100]$ . Include axis labels, a legend, and a vertical line at the transition point.
- (5 points) Determine analytically the value of  $kr$  at which  $|H_{\text{FF}}| = |H_{\text{NF}}|$  (the near-field/far-field transition). At  $f = 1$  GHz, what is the corresponding physical distance  $r$ ? Express this distance both in meters and in wavelengths  $\lambda$ .

**Deliverables:** MATLAB .m file, the log-log plot with labeled axes and vertical transition line, and a 2–3 sentence physical interpretation of the transition printed as a comment.

## 10. Friis Radar Range Equation

A monostatic radar operates at  $f = 10$  GHz (X-band) with the following parameters: peak transmit power  $P_T = 50$  kW, transmit/receive antenna gain  $G_T = G_R = 30$  dBi, and minimum detectable received power  $P_{\text{min}} = -90$  dBm. The radar range equation is:

$$P_R = \frac{P_T G_T G_R \lambda^2 \sigma}{(4\pi)^3 R^4},$$

where  $\sigma$  is the target's radar cross-section (RCS).

- (5 points) Compute the maximum detection range  $R$  (in km) for a target with  $\sigma = 1$  m<sup>2</sup> (approximately 0 dBsm, roughly a human body). Show all steps.
- (5 points) Repeat for a stealth aircraft with  $\sigma = 10^{-3}$  m<sup>2</sup> (−30 dBsm). By what factor does the maximum detection range decrease compared to part (a)? Express this factor also in dB.