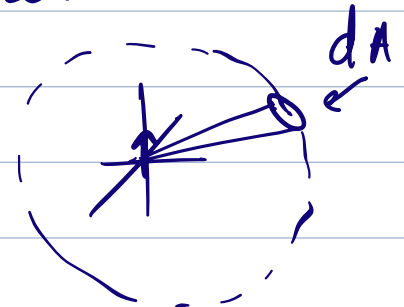


Antenna Descriptions

Starting point: Poynting vector (far field).
e.g. for a Hertz dipole:

$$\vec{S}_{\text{rad}} = \frac{\eta}{8} \left(\frac{I \Delta z}{\lambda} \right)^2 \frac{\sin^2 \theta}{r^2} \hat{r}$$

From here, the total power is

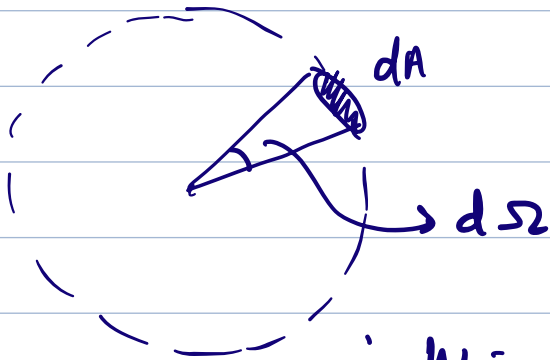


$$W = \oint \vec{S} \cdot dA \hat{r} = \int r^2 \sin \theta d\theta d\phi \hat{r}$$

Real:

$$S = \frac{1}{2} \text{Re}[E \times H^*]$$

Another way of seeing this integral:



$$\begin{aligned} \text{Solid angle} &= d\Omega \\ &= \frac{dA}{r^2} \end{aligned}$$

$$\therefore W = \oint r^2 \vec{S} \cdot d\Omega \hat{r}$$

which is equivalent to $\oint \vec{S} \cdot dA \hat{r}$

Which is more convenient to compute and more practical for discussion?

Since $|S| \propto 1/r^2 \rightarrow$ I will need to know r to talk/compute $|S|$.

But not so for $|S r^2|$ since in f.f. $S \propto \frac{1}{r^2}$.

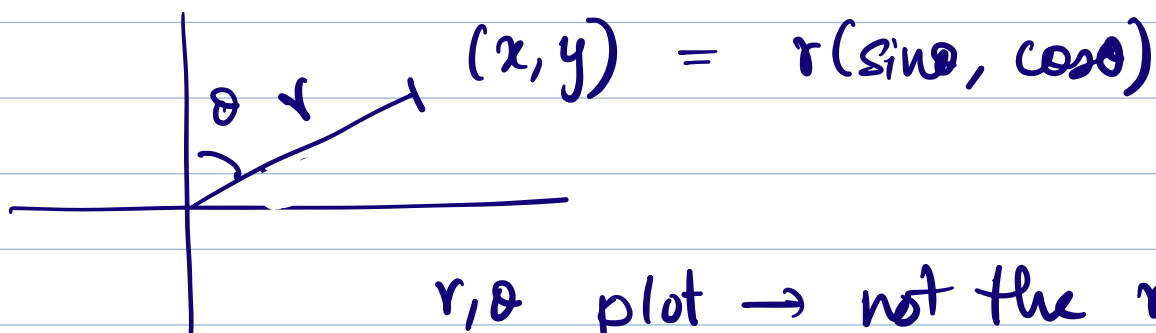
∴ More convenient qty is $U = r^2 S$
 which is called radiation intensity.
 units? U : W/solid angle.
 S : W/m²

More precisely: $U = \frac{r^2}{\eta} |E|^2$
 $= \frac{r^2}{\eta} \left[|E_\theta|^2 + |E_\phi|^2 \right]$
 depend on $\frac{1}{r}$.

e.g. for a Hertz dipole $U = U_0 \sin^2 \theta$

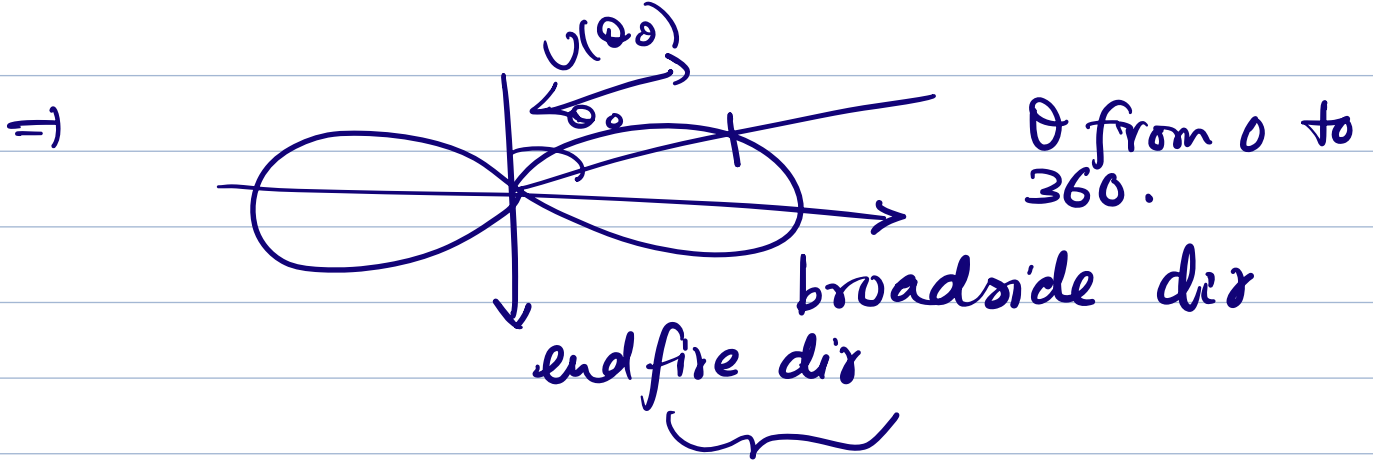
Then total radiated power = $\int U d\Omega$
 $= \iint U \sin \theta d\theta d\phi$

↳ Also a useful qty to plot in polar coordinates.

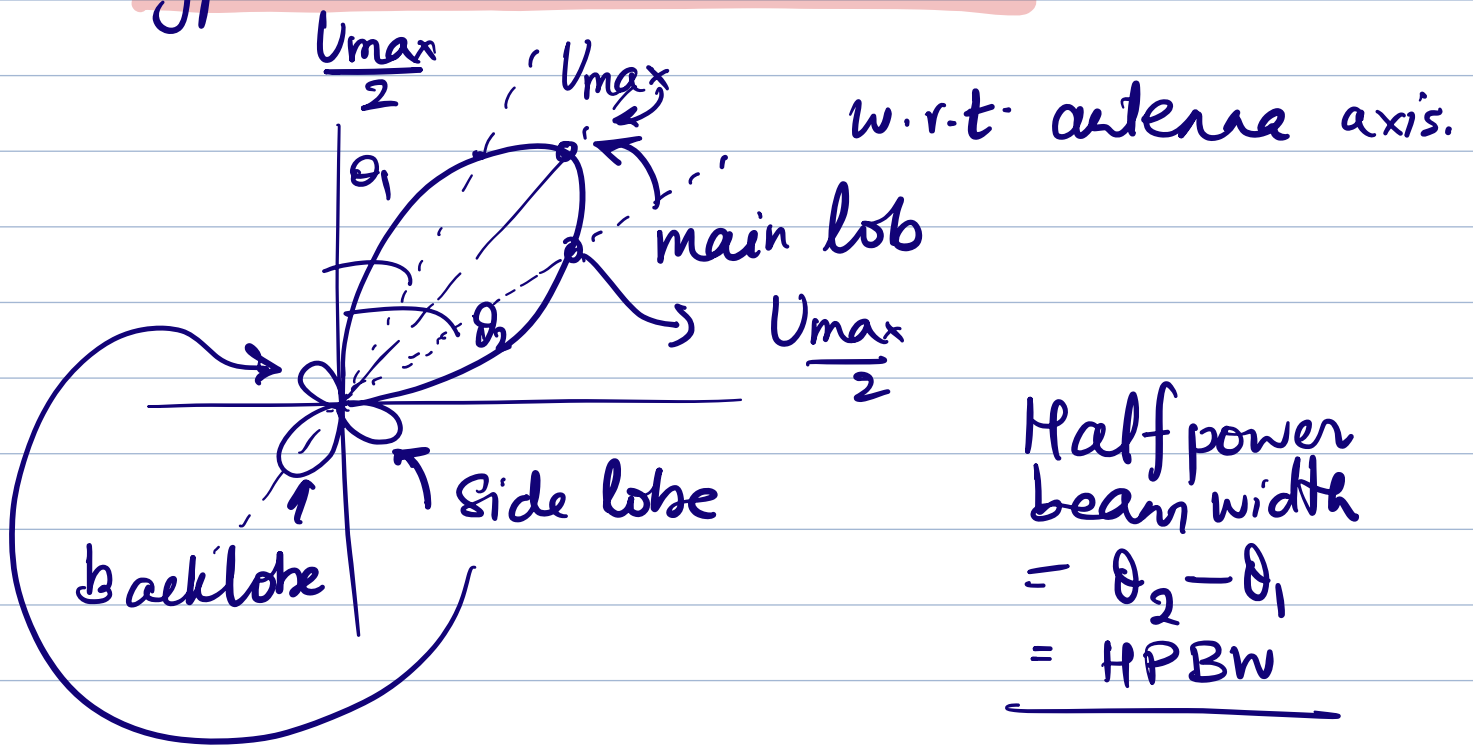


r, θ plot \rightarrow not the r, θ of the antenna but of the 2D plot.

So when we want to plot rad pattern of Hertz dipole
Map: $r \rightarrow U$
 $\theta \rightarrow \theta$



Typical Radiation Patterns



Directivity: way to characterize the focussing power of an ant.

In general: $D(\theta, \phi) = \frac{U(\theta, \phi)}{\langle U(\theta, \phi) \rangle}$

where $\langle U(\theta, \phi) \rangle = \frac{\int U(\theta, \phi) d\Omega}{\int d\Omega}$

i.e. avg intensity.

Typically when antenna directivity is mentioned without qualification, it refers to $D(\theta, \phi)|_{\max}$.

e.g. Hertz dipole $U = U_0 \sin^2 \theta$

$$\Rightarrow \langle U \rangle = \frac{U_0 \int_0^{2\pi} \int_0^\pi \sin^2 \theta \sin \theta \, d\theta \, d\phi}{4\pi}$$

and $D_{\max} = 3/2 \iff 1.76 \text{ dB}$

an isotropic antenna would be $D = 1 \Rightarrow 0 \text{ dB}$.

Antenna gain: Takes ohmic losses into account.

$$P_{\text{input}} = W_{\text{rad}} + P_{\text{loss}}$$

$$\text{efficiency} = \eta_r = \frac{W_r}{P_i}$$

So gain = $G = \eta_r \times D$ book uses G_d .

$$G_{\text{dB}} = 10 \log \eta_r + D_{\text{dB}}$$

$\underbrace{\hspace{10em}}_{< 0}$

Another related term: Realized gain

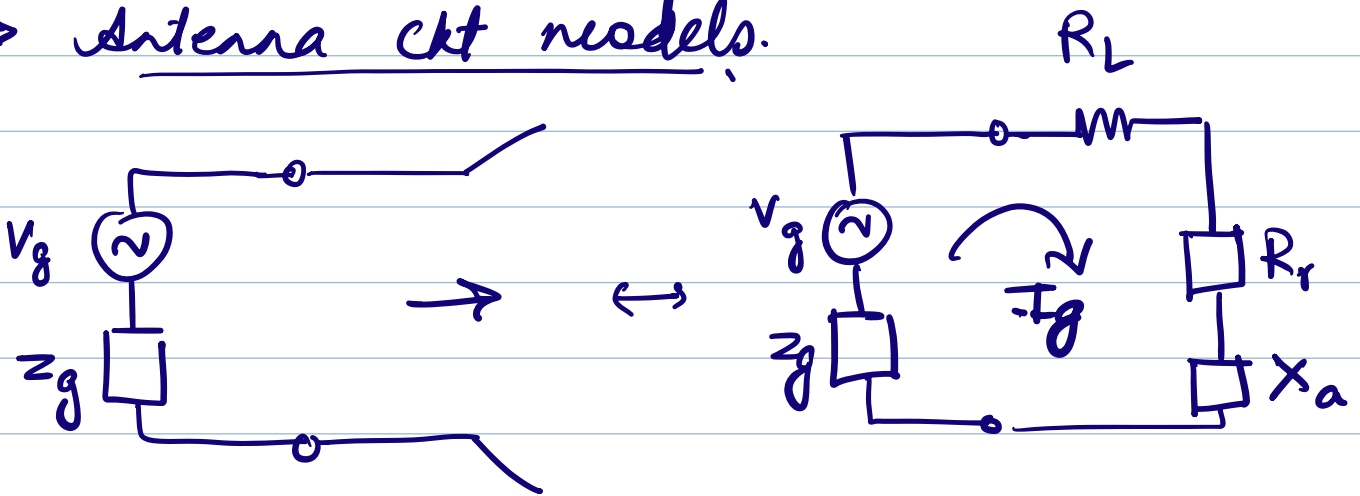
Above we assumed that input is matched to antenna impedance.

$$\text{If not, } G_{re} = (1 - |\Gamma|^2) \eta_r D$$

reflection loss.

book uses e_r

↳ Antenna ckt models.



generator antenna

Z_a $\left\{ \begin{array}{l} R_L: \text{loss resistance} \\ R_r: \text{Rad resistance} \\ X_a: \text{Ant reactance} \end{array} \right.$

Max power corresponds to near field reactive energy.

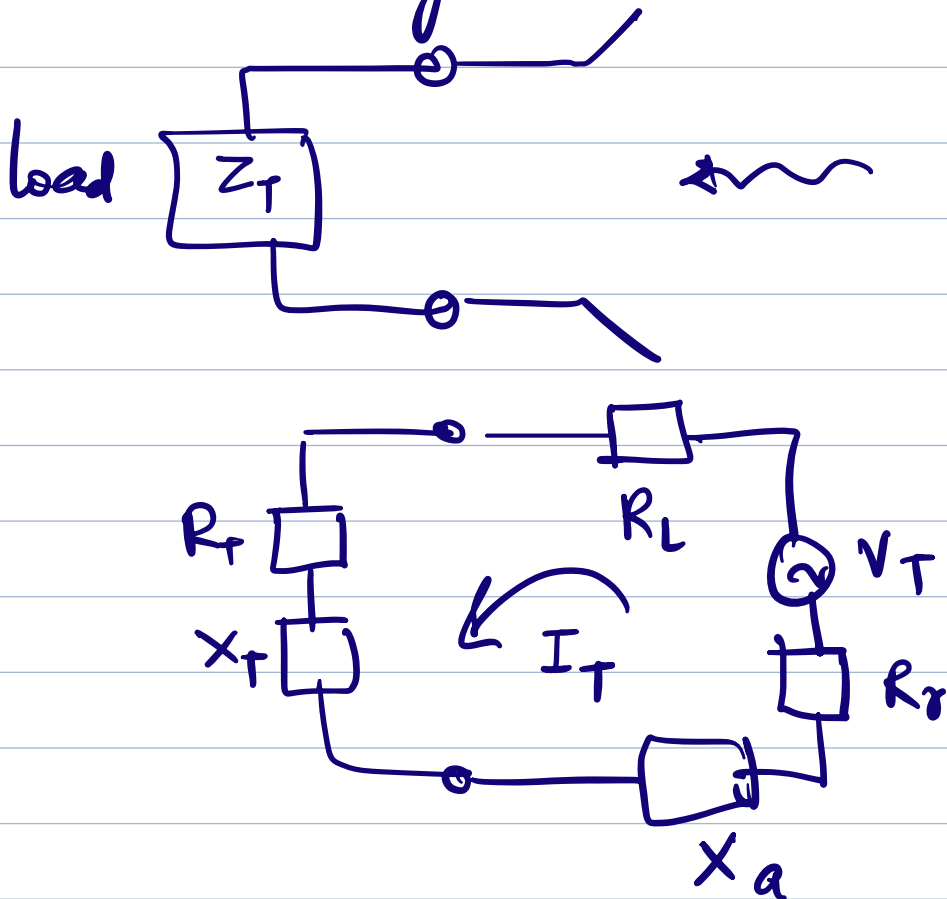
$$Z_g = Z_a^* \text{, i.e.}$$

$$R_g = R_L + R_r$$

$$X_g = -X_a$$

Power radiated by ant: $P_r = \frac{1}{2} |I_0|^2 R_r$

Similarly in the R_x mode



In this case, collected power = $P_c = \frac{1}{2} |I_T|^2 R_T$

$$P_T = \frac{1}{2} |I_T|^2 R_T \rightarrow \text{to load}$$

$$P_r = \frac{1}{2} |I_T|^2 R_r \rightarrow \text{scattered / re radiated}$$

$$P_L = \frac{1}{2} |I_T|^2 R_L \rightarrow \text{heat}$$

$$\text{Total } P_c = \frac{1}{2} V_T I_T^* \rightarrow \text{collected power.}$$