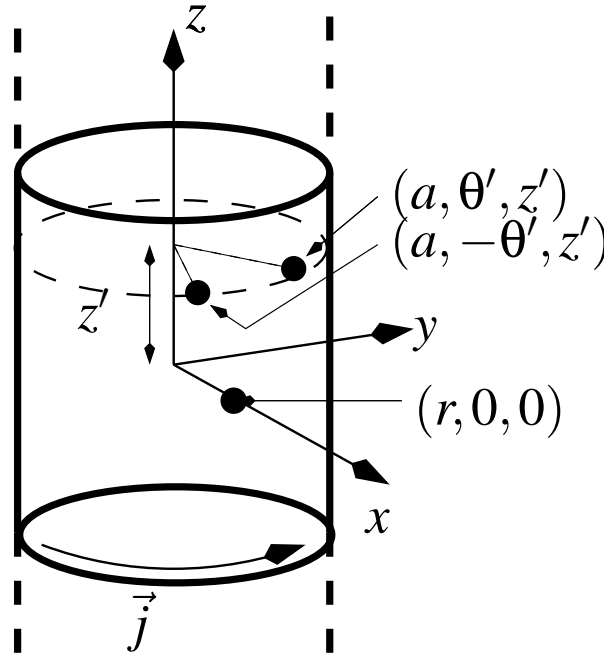


# Finding the field due to a solenoid

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Consider an ideal solenoid of radius  $a$ , with  $n$  turns per metre, carrying current  $I_0$ . We wish to compute the magnetic field  $\vec{B}$  due to these currents.



As discussed in the class, we have a problem that is symmetric in  $\theta$  and  $z$ . Thus,

$$\vec{B}(\vec{r}) = B_r(r)\hat{r} + B_\theta(r)\hat{\theta} + B_z(r)\hat{z} \quad (1)$$

From the fact that magnetic field has zero divergence ... why zero divergence?

$$\begin{aligned} \nabla \cdot \vec{B}(\vec{r}) &= \frac{\mu_0}{4\pi} \int \nabla \cdot \left( \vec{j}(\vec{r}') \times \nabla \frac{1}{R_{12}} \right) dV' \\ &= -\frac{\mu_0}{4\pi} \int \nabla \cdot \left( \nabla \times \frac{\vec{j}(\vec{r}')}{R_{12}} \right) dV' \\ &= 0 \end{aligned}$$

since the divergence of a curl is always zero, from stokes theorem. Note that our  $\epsilon$  notation for curl (see the vector identities writeup) helps us derive step 2 from step 1:

$$\begin{aligned} \vec{j}(\vec{r}') \times \nabla \frac{1}{R_{12}} &= \epsilon_{klm} \hat{x}_k j_l \partial_m \frac{1}{R_{12}} \\ &= -\epsilon_{kml} \hat{x}_k \partial_m \left( \frac{j_l}{R_{12}} \right) \\ &= -\nabla \times \left( \frac{\vec{j}(\vec{r}')}{R_{12}} \right) \end{aligned}$$

It is worth noting that relativity said force due to magnetic fields were given by  $(1/4\pi\epsilon_0 c^2) I_1 \vec{dl}_1 \times (I_2 \vec{dl}_2 \times \vec{R}_{12}/R_{12}^3)$ , and this same form now implies that the divergence of  $\vec{B}$  is zero. This property of magnetic fields is built into the very process by which they are derived from Coulomb's law.

So going back to Eq. 1, we obtain

$$\nabla \cdot \vec{B} = \frac{1}{r} \partial_r (rB_r) + \frac{1}{r} \partial_\theta B_\theta + \partial_z B_z = \frac{1}{r} \partial_r (rB_r) = 0$$

Hence  $B_r = B_0/r$ , which is not allowed if the domain includes  $r = 0$ . i.e.,  $B_r \equiv 0$ . So,

$$\vec{B}(\vec{r}) = B_\theta \hat{\theta} + B_z \hat{z}$$

This magnetic field is obtained from

$$\vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \int \vec{j}(\vec{r}') \times \nabla \frac{1}{R_{12}} dV'$$

where  $\vec{j} = I_0 n \hat{\theta}' \delta(r' - a)$ . To make progress we go to the Vector Potential

$$\vec{A}(\vec{r}) = \frac{\mu_0}{4\pi} \int \frac{\vec{j}(\vec{r}')}{R_{12}} dV'$$

Since the problem is symmetric in  $\theta$  and  $z$ , we assume  $\theta = 0$  and  $z = 0$ .  $\vec{j}(\vec{r}')$  is along  $\hat{\theta}'$ , i.e., along  $-\hat{x} \sin \theta' + \hat{y} \cos \theta'$ . Then,

$$\begin{aligned} \vec{A}(r) &= \frac{\mu_0}{4\pi} \int_{-\infty}^{\infty} dz' \int_{-\pi}^{\pi} ad\theta' \frac{I_0 n (-\sin(\theta') \hat{x} + \cos(\theta') \hat{y})}{\sqrt{(x - a \cos \theta')^2 + a^2 \sin^2 \theta' + z'^2}} \\ &= \frac{\mu_0}{4\pi} \int_{-\infty}^{\infty} dz' \int_{-\pi}^{\pi} ad\theta' \frac{I_0 n \cos(\theta') \hat{y}}{\sqrt{(x - a \cos \theta')^2 + a^2 \sin^2 \theta' + z'^2}} \\ &= \frac{\mu_0}{4\pi} I_0 n \hat{y} \int_{-\infty}^{\infty} dz' \int_{-\pi}^{\pi} ad\theta' \frac{\cos(\theta')}{\sqrt{(x - a \cos \theta')^2 + a^2 \sin^2 \theta' + z'^2}} \end{aligned}$$

For  $\theta = 0$ ,  $\hat{y}$  is the same as  $\hat{\theta}$ , since  $\hat{r}$  is along  $\hat{x}$ . Thus, this shows us that  $\vec{A}(r)$  is along  $\hat{\theta}$  which is what we wanted to get out of this exercise.

We are now almost done. If  $\vec{A}$  is along  $\theta$  and depends only on  $r$ , its curl

$$\frac{1}{r} \det \begin{vmatrix} \hat{r} & r\hat{\theta} & \hat{z} \\ \partial_r & \partial_\theta & \partial_z \\ 0 & rA_\theta & 0 \end{vmatrix} = \frac{1}{r} \partial_r (rA_\theta) \hat{z}$$

$\vec{B}$  is purely along  $\hat{z}$  and depends only on  $r$ . We could use the above formulae to calculate it, but there is now an easier way. We use Stoke's theorem on a loop in the  $r - z$  plane, with unit length along  $z$ , and its two sides at  $r = 0$  and at  $r$ .

$$\begin{aligned} \oint \vec{B} \cdot d\vec{l} &= B_z(0) - B_z(r) \\ &= \mu_0 I_{\text{encl}} \end{aligned}$$

Thus, we immediately conclude (assuming  $B_z \rightarrow 0$  as  $r \rightarrow \infty$ )

$$B_z(r) = \begin{cases} \mu_0 n I_0 & r < a \\ 0 & r > a \end{cases}$$

## Finite Solenoid

What happens when the solenoid is not infinitely long?

$\partial_z$  is no longer zero, and so,  $B_r$  can now be present:

$$\nabla \cdot \vec{B} = \frac{1}{r} \partial_r (rB_r) + \partial_z B_z = 0 \quad (2)$$

The arguments we used for  $\vec{A}$  do not change; the only difference is that the limits in  $z$  are now finite. So we have

$$\vec{A}(\vec{r}) = A_\theta(r, z) \hat{\theta}$$

Taking the curl yields

$$\vec{B}(\vec{r}) = -\hat{r} \partial_z A_\theta + \hat{z} \frac{1}{r} \partial_r (rA_\theta)$$

The divergence should automatically go to zero, as it does:

$$\frac{1}{r} \partial_r (-r \partial_z A_\theta) + \partial_z \left( \frac{1}{r} \partial_r (r A_\theta) \right) = 0$$

since second partial derivatives commute.

As a special case, consider  $r \ll a$ . The expression for  $A_\theta$  becomes, for small  $x$

$$\begin{aligned} A_\theta &= \frac{\mu_0}{4\pi} I_0 n \hat{y} \int_{-L/2}^{L/2} d\zeta \int_{-\pi}^{\pi} ad\theta' \frac{\cos(\theta')}{\sqrt{(x - a \cos \theta')^2 + a^2 \sin^2 \theta' + \zeta^2}} \\ &\simeq \frac{\mu_0}{4\pi} I_0 n \hat{y} \int_{-L/2-z}^{L/2-z} d\zeta \int_{-\pi}^{\pi} ad\theta' \frac{\cos(\theta')}{\sqrt{a^2 + \zeta^2 - 2ax \cos \theta'}} \\ &\simeq \frac{\mu_0}{4\pi} I_0 n \hat{y} \int_{-L/2-z}^{L/2-z} d\zeta \int_{-\pi}^{\pi} ad\theta' \frac{\cos(\theta')}{\sqrt{a^2 + \zeta^2}} \left( 1 + \frac{ax \cos(\theta')}{a^2 + \zeta^2} \right) \\ &= \frac{\mu_0}{4} I_0 n \hat{y} a^2 x \int_{-L/2-z}^{L/2-z} d\zeta \frac{1}{(a^2 + \zeta^2)^{3/2}} \end{aligned}$$

The integral is known in closed form (look up your favourite table of integrals. It is in all of them):

$$\int_{\alpha}^{\beta} dz \frac{a^2}{(a^2 + z^2)^{3/2}} = \frac{\beta}{\sqrt{\beta^2 + a^2}} - \frac{\alpha}{\sqrt{\alpha^2 + a^2}}$$

Applying the formula above, we obtain  $A_\theta$  and  $B_z$  for the infinite case:

$$\begin{aligned} A_\theta &= \frac{\mu_0}{2} I_0 n r \\ B_z &= \frac{1}{r} \partial_r (r A_\theta) = \frac{\mu_0}{2} \frac{I_0 n}{r} \partial_r (r^2) = \mu_0 n I_0 \end{aligned}$$

For the finite case, this becomes

$$\begin{aligned} B_z &= \mu_0 n I_0 \int_{-L/2-z}^{L/2-z} d\zeta \frac{a^2}{2(a^2 + \zeta^2)^{3/2}} \\ &= \mu_0 n I_0 \left[ \frac{L/2-z}{\sqrt{(L/2-z)^2 + a^2}} - \frac{-L/2-z}{\sqrt{(-L/2-z)^2 + a^2}} \right] \end{aligned}$$

It is worth noting that the fringing fields of a solenoid *do not fall off exponentially*! Remember the case of the capacitor. There the fringing fields fell off exponentially. The difference between the two cases is that for the capacitor, we specified *voltage* rather than  $\sigma(x)$  on the plates. Here, we have specified the precise currents. When we do that, we do not allow for “self-consistent” currents, and the fringing fields can penetrate a lot further.