

18-1-12

Lec 8

Noise in MOSFETs

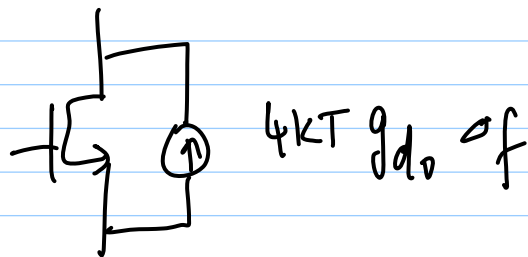
1) Thermal noise

a) Triode region:

$$I_D = k' \left(\frac{W}{L} \right) \left[(V_{GS} - V_T) V_{DS} - \frac{V_{DS}^2}{2} \right]$$

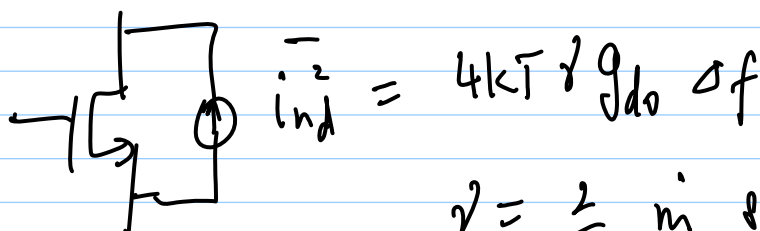
$$g_d = \frac{\partial I_D}{\partial V_{DS}} = k' \left(\frac{W}{L} \right) [V_{GS} - V_T - V_{DS}]$$

$$g_{d0} = k' \left(\frac{W}{L} \right) (V_{GS} - V_T)$$



$$\overline{i_{nd}^2} = 4kT \gamma g_{d0} \Delta f \quad [\gamma \approx 1 \text{ in triode}]$$

b) long-channel device in sat.



$\gamma = \frac{2}{3}$ in sat. region for L.C. device

$$I_D = \frac{k'}{2} \left(\frac{W}{L} \right) (V_{DS} - V_T)^2$$

$$g_m = \frac{\partial I_D}{\partial V_{DS}} = k' \left(\frac{W}{L} \right) (V_{DS} - V_T) = g_{do}$$

$$\boxed{\overline{i_{nd}^2} = 4kT \cdot \frac{2}{3} g_m \Delta f} \quad \text{common form}$$

c) S.C. device

$$\overline{i_{nd}^2} = 4kT \gamma g_{do} \Delta f$$

$$\gamma > 2/3 ; g_{do} > g_m \quad (g_{do} = \frac{g_m}{\alpha})$$

2) Flicker noise ($1/f$ noise)

$$\overline{i_{n,1/f}^2} = \frac{k}{f} \cdot \frac{g_m^2}{WL C_{ox}^2} \cdot \Delta f$$

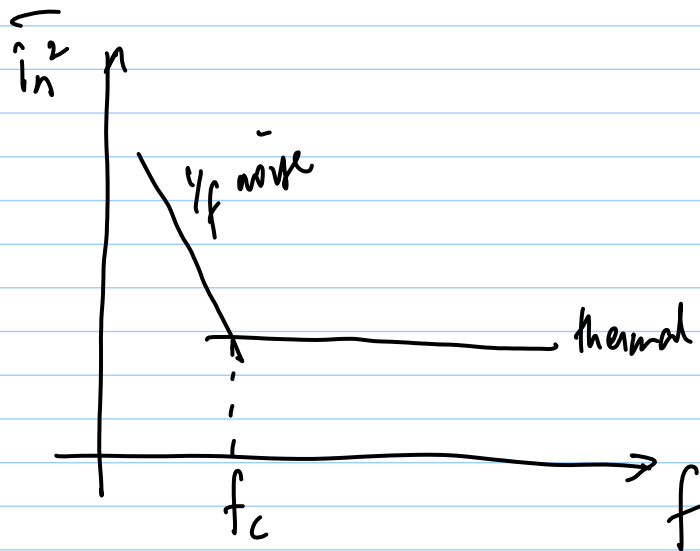
$$= \frac{k'}{f} \cdot W_T^2 \cdot W \cdot L \cdot \Delta f$$

$$\overline{v_{n,1/f}^2} = \frac{k}{f} \cdot \frac{1}{WL C_{ox}^2} \Delta f$$

$$k_n \sim 50 \cdot k_p ; k_p \sim 10^{-28} \text{ C}^2/\text{m}^2 \left[\begin{array}{l} \text{PMOS may have} \\ \text{lower } 1/f \text{ noise} \end{array} \right]$$

* Use larger area for low flicker noise

* flicker noise important @ low freq.

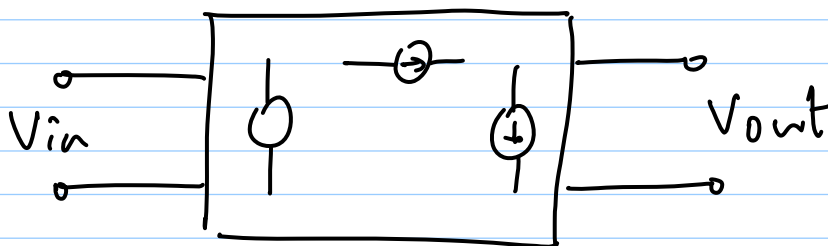


$$f_c \approx \frac{k_{1/f}}{4kT\gamma} \cdot f_T$$

Shot noise in Diodes

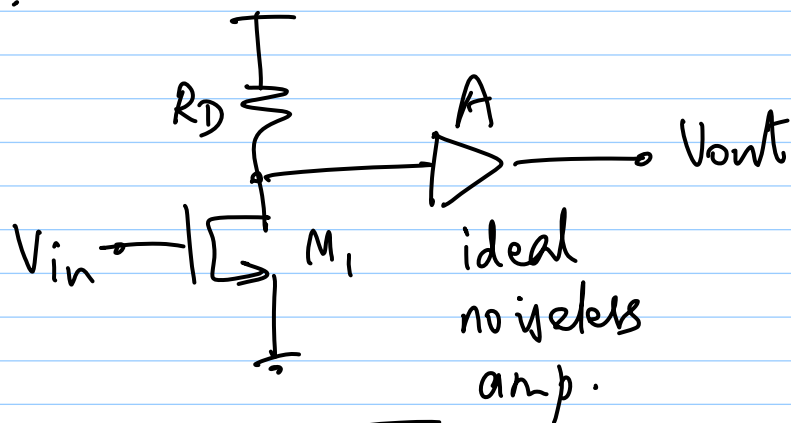
$$\overline{i_n^2} = 2q I_{DC} \text{ of } (\text{use in BJTs})$$

Noise representation in dets



* Set $V_{in} = 0$ & measure $\overline{V_{n,out}^2}$
 $\rightarrow$ depends on gain of system

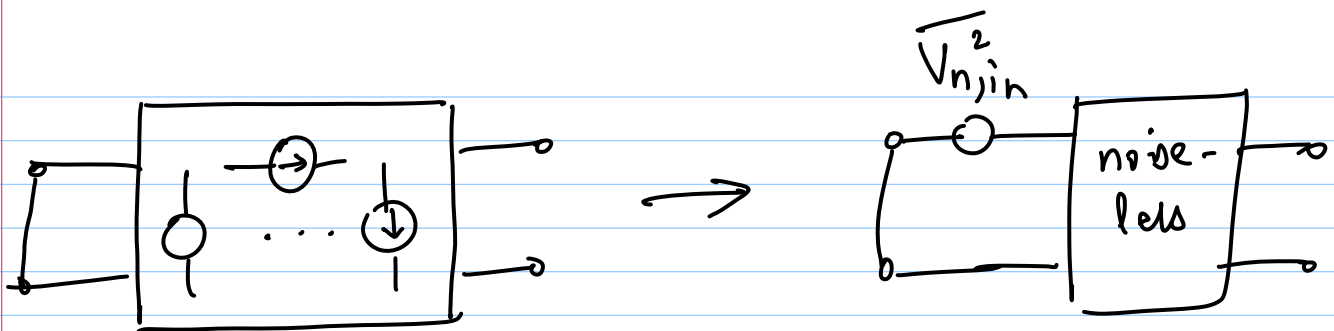
e.g.



* as $A \uparrow$, $\overline{V_{n,out}^2} \uparrow$, but signal power also $\uparrow$

→ define noise performance as "input-referred noise"

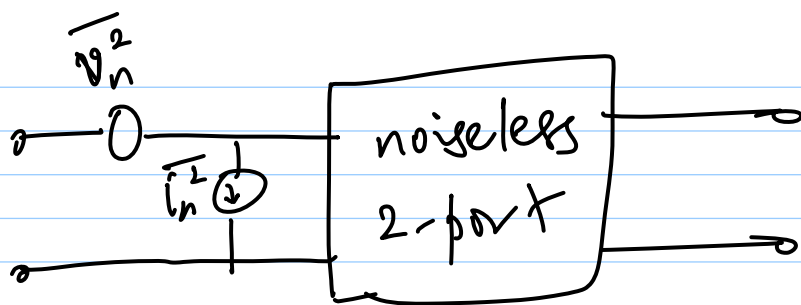
→ fictitious quantity (cannot be measured)



$$\overline{V_{n,out}^2} = A_v^2 \cdot \overline{V_{n,in}^2}$$

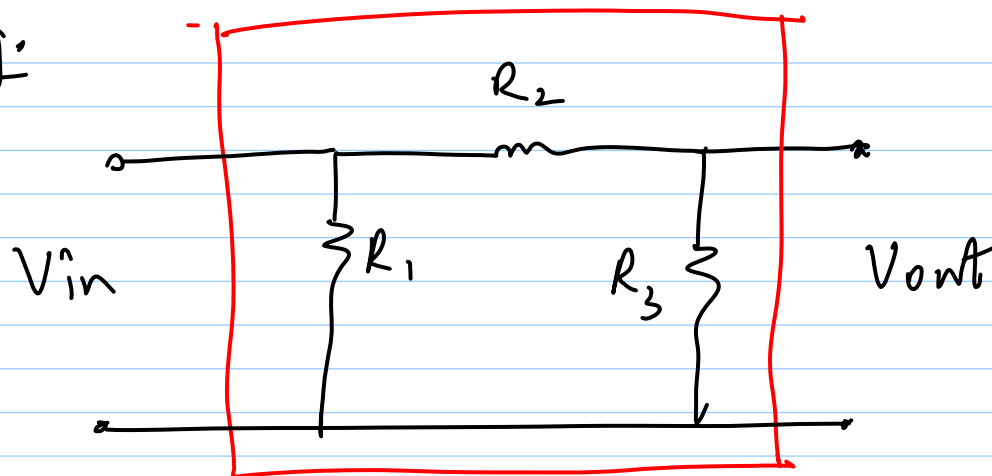
as source imp. $\rightarrow \infty \Rightarrow$ no noise current drawn from $\overline{V_{n,in}}$

$\Rightarrow$ seems as if ckt is not noisy

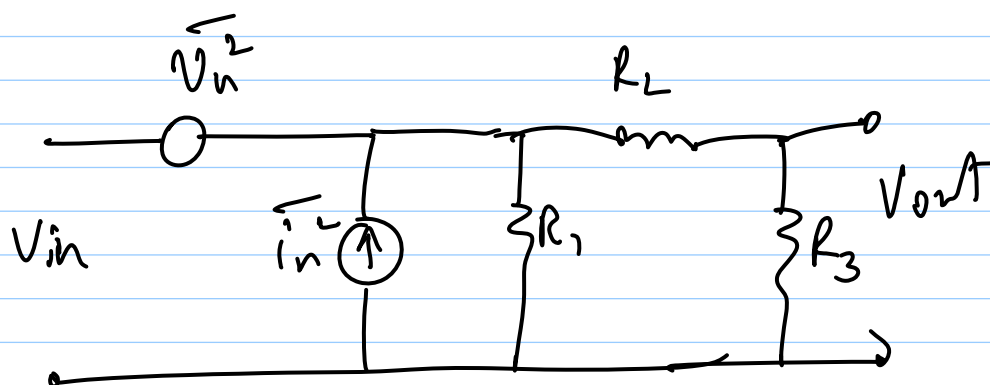


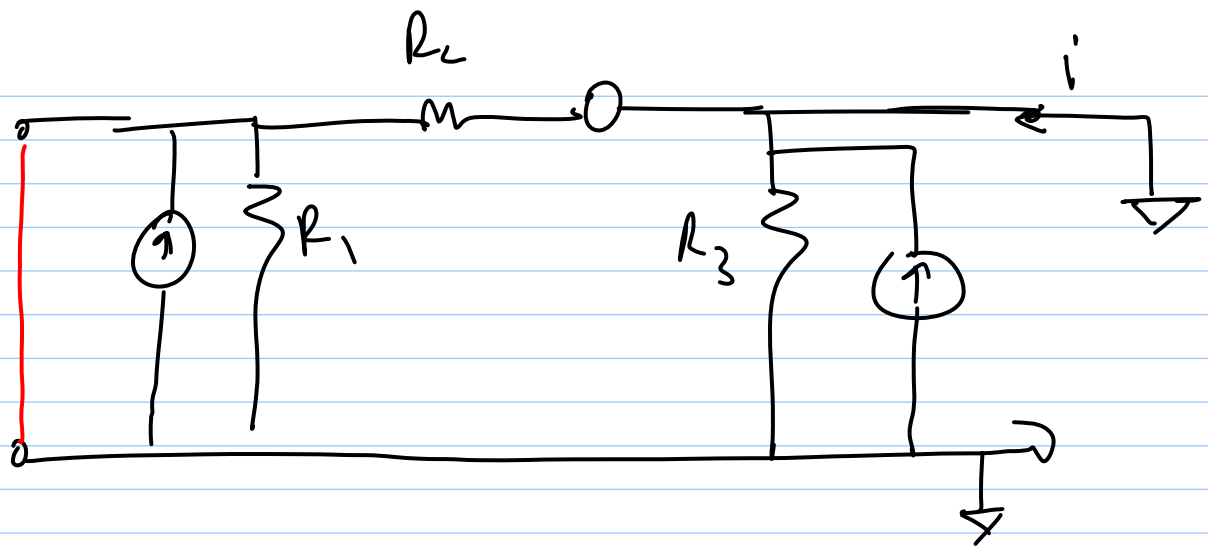
* In general, $\bar{v}_n$ & $\bar{i}_n$ may be correlated (same noise sources in the dkt)

e.g.



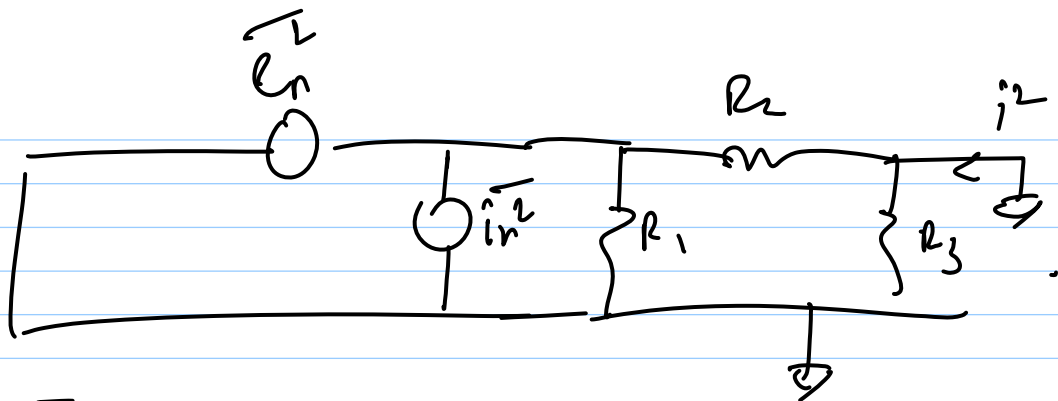
eq. $\longleftrightarrow$
to





1) short i/p :

$$\begin{aligned} \overline{i^2} &= \frac{4kT}{R_3} \Delta f + \frac{4kT R_2 \Delta f}{R_2^2} \\ &= 4kT \Delta f \left(\frac{1}{R_2} + \frac{1}{R_3} \right) \end{aligned}$$



$$\overline{i^2} = \frac{\overline{e_n^2}}{R_2^2}$$

equate :

$$\overline{e_n^2} = 4kT \Delta f R_2^2 \left(\frac{1}{R_2} + \frac{1}{R_3} \right)$$

2) o-c input:

$$\overline{i^2} = \frac{4kT\Delta f}{R_1} \left(\frac{R_1}{R_1 + R_2} \right)^2$$

$$+ \frac{4kT\Delta f}{R_3} + \frac{4kTR_2\Delta f}{(R_1 + R_2)^2}$$

$$\frac{2-pwr}{\overline{i^2}} = \overline{i_n^2} \left(\frac{R_1}{R_1 + R_2} \right)^2$$

⇒ equate;

$$\overline{i_n^2} = \overline{i^2} \cdot \left(\frac{R_1 + R_2}{R_1} \right)^2$$

$$= 4kT\Delta f \left\{ \frac{1}{R_1} + \frac{(R_1 + R_2)^2}{R_2 R_3} + \frac{R_2}{R_1^2} \right\}$$