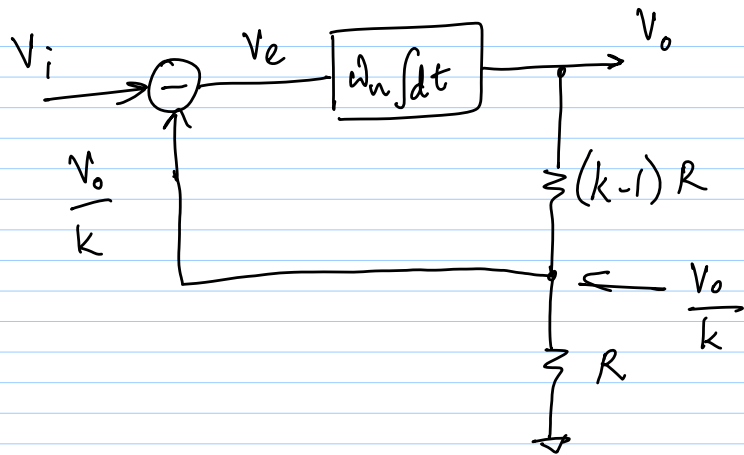
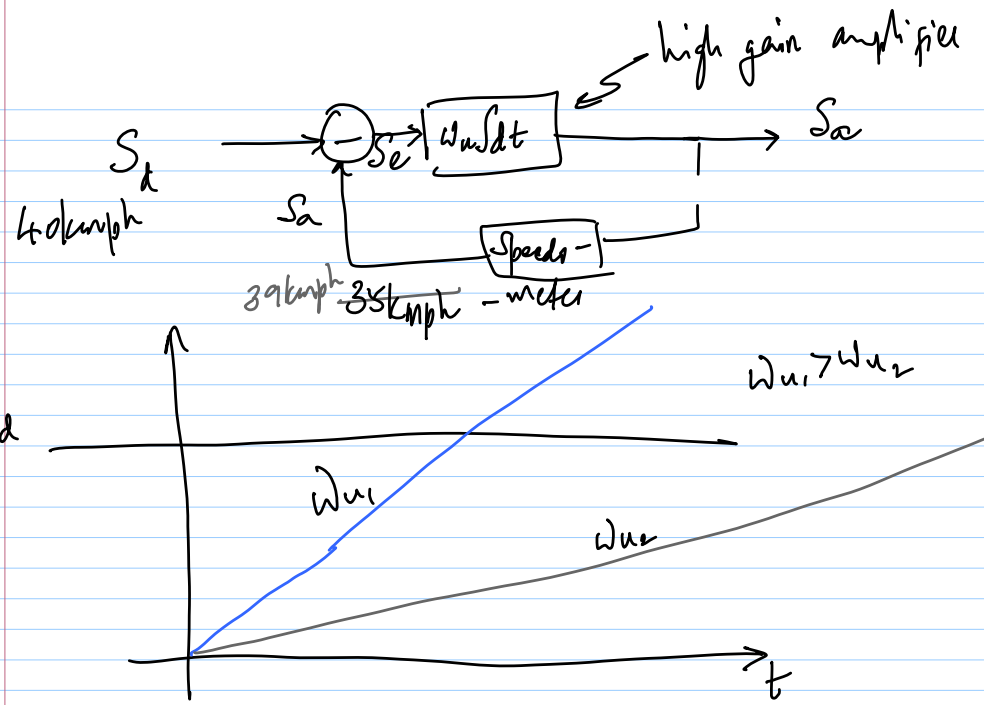


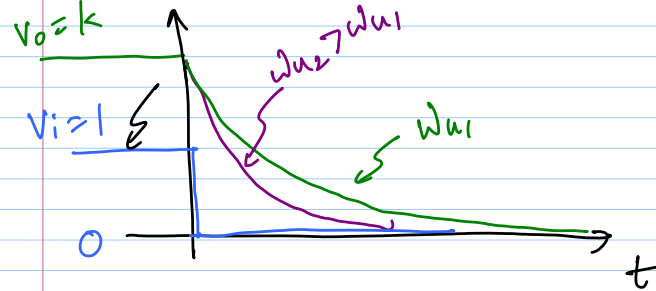
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Lec 15
Feedback

- * Desired value
- * Compare actual value w/ desired value
- * drive actual towards desired



$$V_e = V_i - \frac{V_o}{k} \rightarrow 0$$



1) $V_e = -\frac{V_o}{k} \quad @ \quad t \gg 0$

$$V_o = W_u \int V_e dt \Rightarrow \frac{dV_o}{dt} = -\frac{W_u}{k} \cdot V_o$$

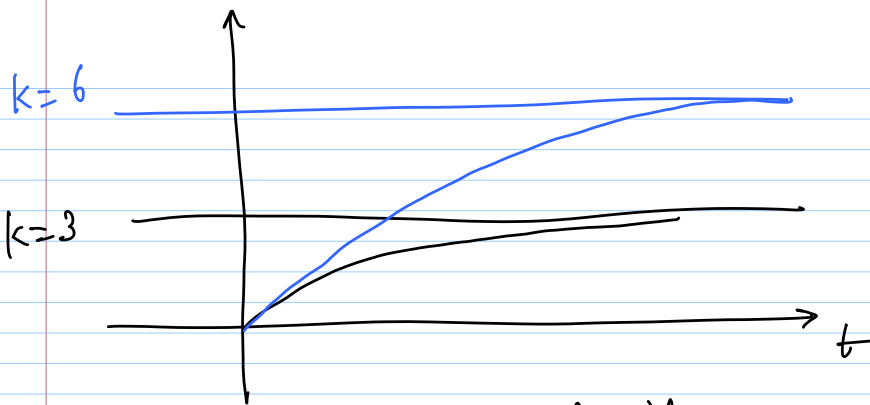
$$\frac{dV_o}{V_o} = \frac{-\omega_u}{k} \cdot dt$$

$$V_o = k e^{-\omega_u/k t}$$

2) $V_{i, \text{final}} = V_i$

$$V_e = V_i - \frac{V_o}{k}$$

$$\frac{dV_o}{V_i - \frac{V_o}{k}} = \omega_u dt$$



initial slope = $\omega_u \cdot V_i$

higher $k \Rightarrow$ slower settling

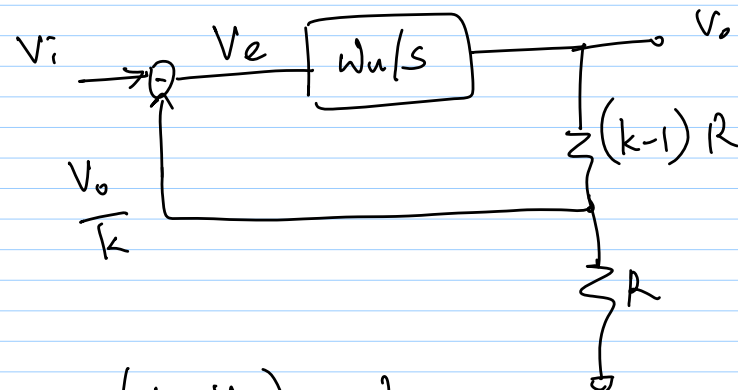
$$V_o = k V_i + e^{-\omega_u/k t} \left[\frac{V_o(0)}{k} - V_i \right]$$

$$= V_o(0) e^{-\frac{\omega_u}{k} t}$$

$$+ k V_i \left[1 - e^{-\frac{\omega_u}{k} t} \right]$$

forced response

3) Laplace solution



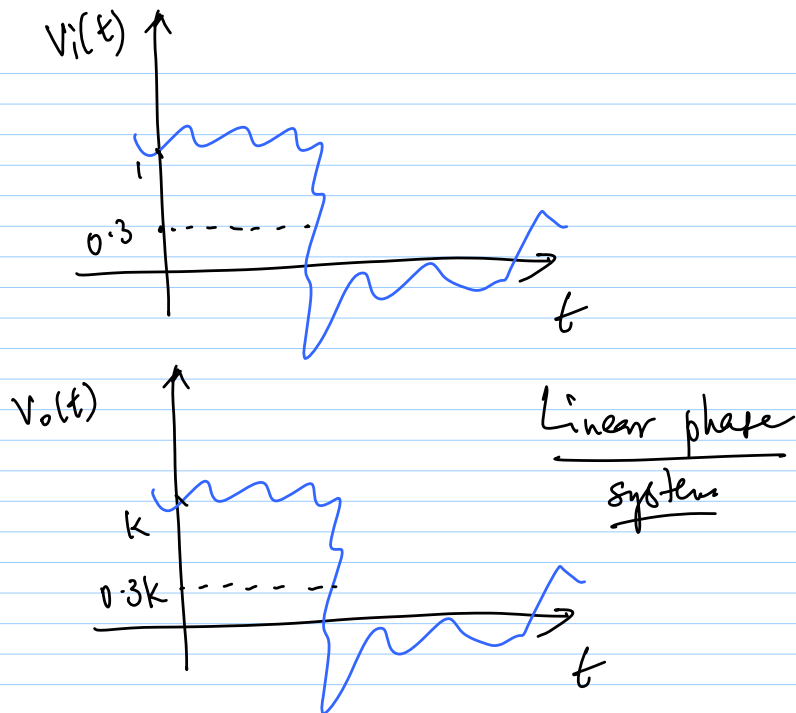
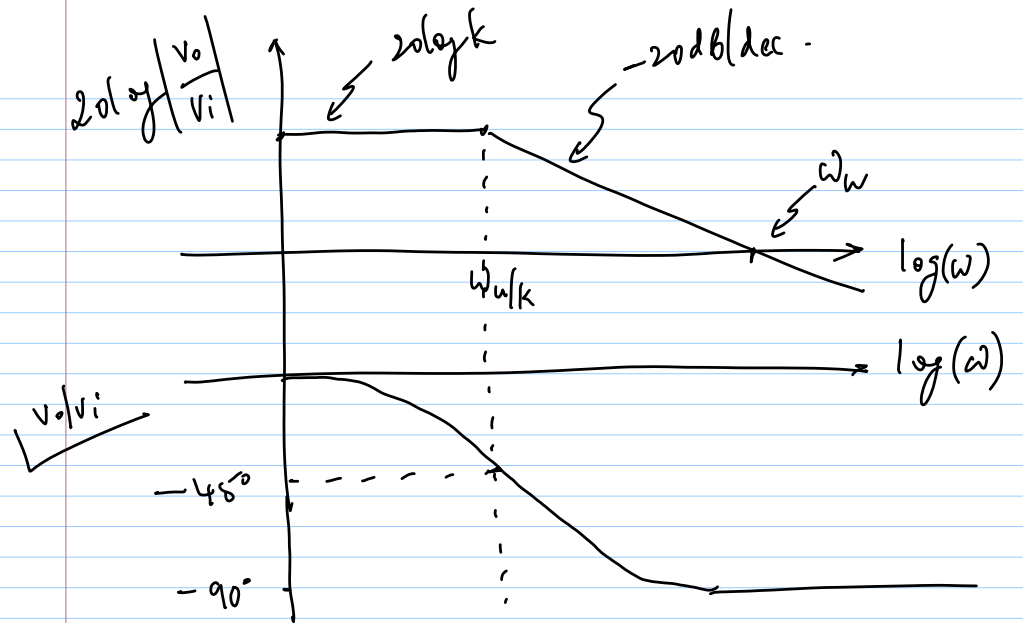
$$\left(V_i - \frac{V_o}{k} \right) \cdot \frac{\omega_u}{s} = V_o$$

$$\frac{V_o}{V_i}(s) = \frac{w_u s}{1 + \frac{w_u}{k} s}$$

$$\frac{V_o}{V_i}(s) = k \cdot \frac{1}{1 + \frac{s}{(w_u/k)}}$$

$$\left| \frac{V_o}{V_i} \right| = \frac{k}{\sqrt{1 + \frac{w^2 k^2}{w_u^2}}}$$

$$\angle \frac{V_o}{V_i} = -\tan^{-1} \left(\frac{k w}{w_u} \right)$$



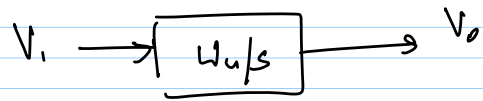
Linear phase $\Rightarrow w \ll w_u/k$

$$\frac{V_o}{V_i} = k \Rightarrow w \ll w_u/k$$

$\frac{w_u}{k} = \text{BW of amplifier}$

$$w \gg \frac{w_u}{k} \Rightarrow \left| \frac{V_o}{V_i} \right| = \frac{w_u}{w}$$

$$\angle \frac{V_o}{V_i} = -90^\circ$$



a) $\omega \gg \frac{\omega_n}{k} \Rightarrow$ no feedback

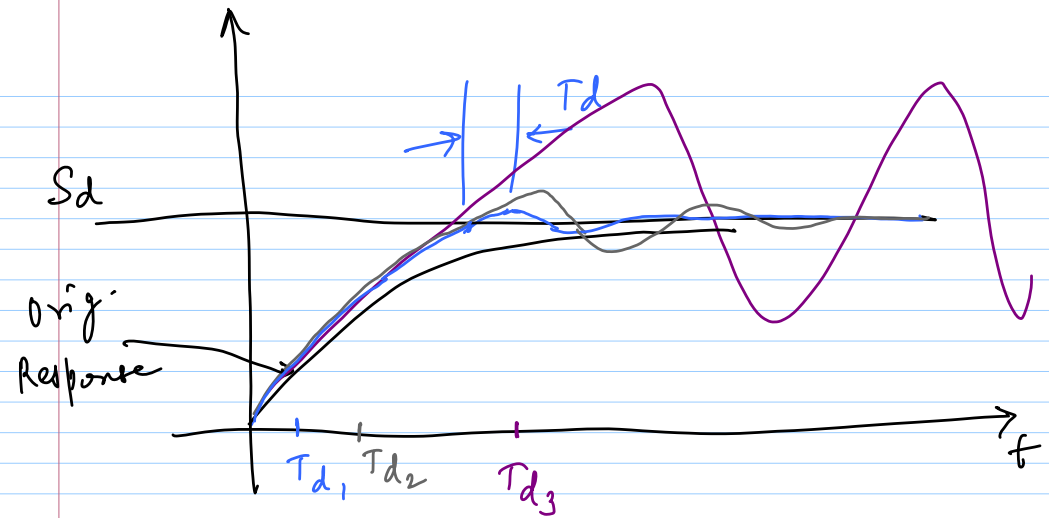
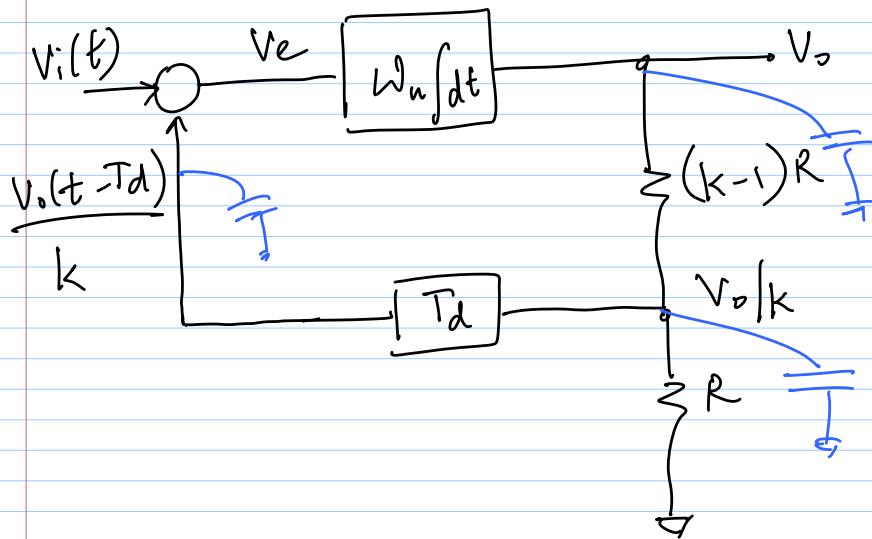
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Lec 16

$$\text{pole freq.} = -\frac{\omega_n}{k}$$

$$\text{BW} = \frac{\omega_n}{k}$$

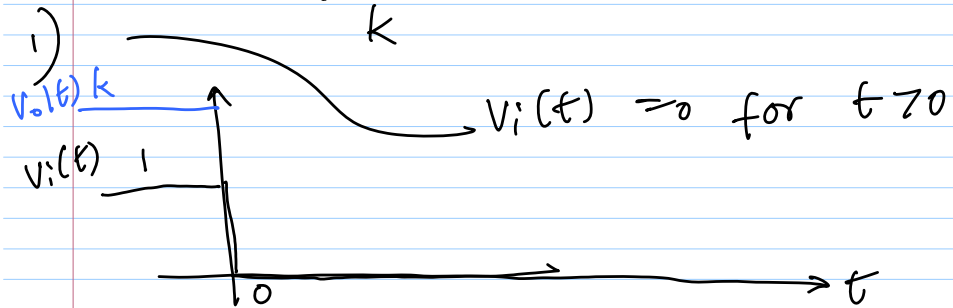
$$\tau = \frac{k}{\omega_n}$$



$$V_e(t) = V_i(t) - \frac{V_o(t - T_d)}{k}$$

$$V_o(t) = \omega_n \int V_e(t) dt$$

$$\frac{dV_o}{V_i(t) - \frac{V_o(t - T_d)}{k}} = \omega_n dt$$



$$\frac{dV_o}{V_o(t - T_d)} = -\frac{\omega_n}{k} dt$$

$$\frac{dV_o}{dt} = -\frac{\omega_n}{k} V_o(t - T_d)$$

$$e^{t+z} = e^z \cdot e^t$$

- 1) exponential solution possible
- 2) sinusoidal solution possible

assume solution is of the form $e^{\sigma t}$

Diff. equation is:

$$\sigma e^{\sigma t} = -\frac{\omega_n}{k} e^{\sigma(t - T_d)}$$

$$\sigma + \frac{\omega_n}{k} e^{-\sigma T_d} = 0$$

$f_1(\sigma)$ points to σ and $f_2(\sigma)$ points to $\frac{\omega_n}{k} e^{-\sigma T_d}$

$$\sigma' = \frac{k\sigma}{\omega_n}$$

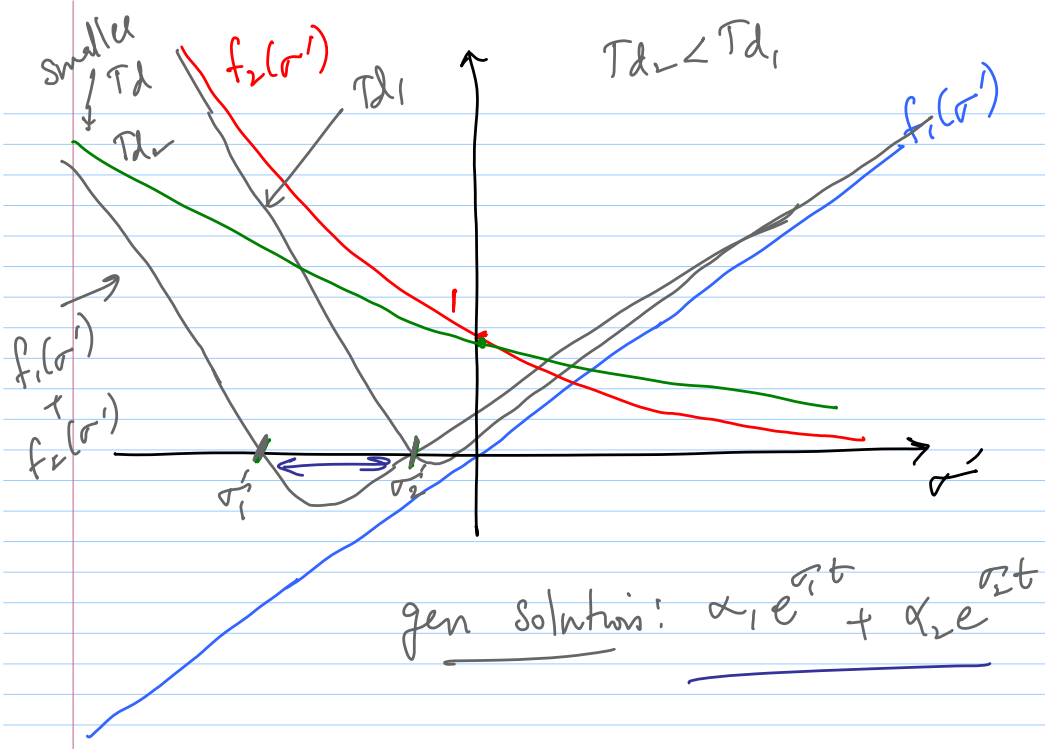
$$\sigma' + e^{-T_d \cdot \left(\frac{\omega_n \sigma'}{k}\right)}$$

$$z = \frac{T_d \omega_n}{k}$$

$$\sigma' + e^{-\sigma' z} = 0$$

$f_1(\sigma')$ points to σ' and $f_2(\sigma')$ points to $e^{-\sigma' z}$

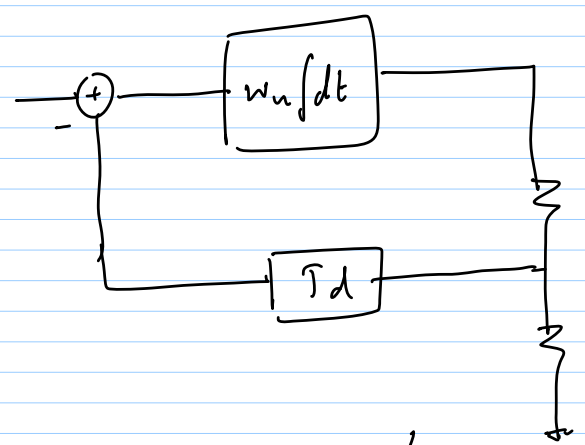
σ'_1 & σ'_2
 \Downarrow
 σ_1 & σ_2



- 1) for large enough T_d , $\leftarrow T_{dc1}$
 $f_1(s') + f_2(s')$ may not touch x -axis
 * no real solutions
 * $s' = \sigma + j\omega$
- 2) T_d even larger $\leftarrow T_{dc2}$
 $\sigma = 0$, $j\omega$ solutions
- 3) Critical T_d for which settling is fastest

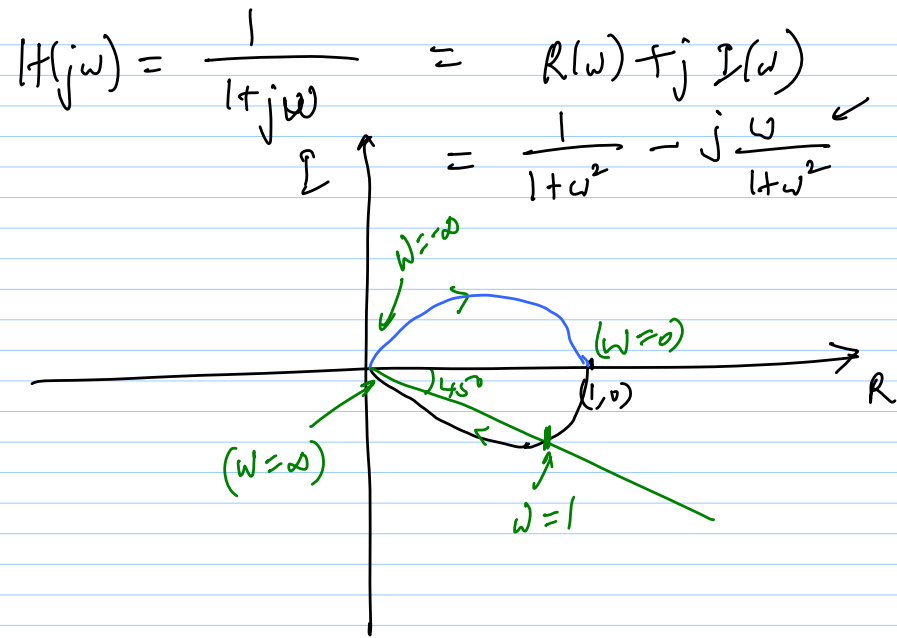
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Lec 17



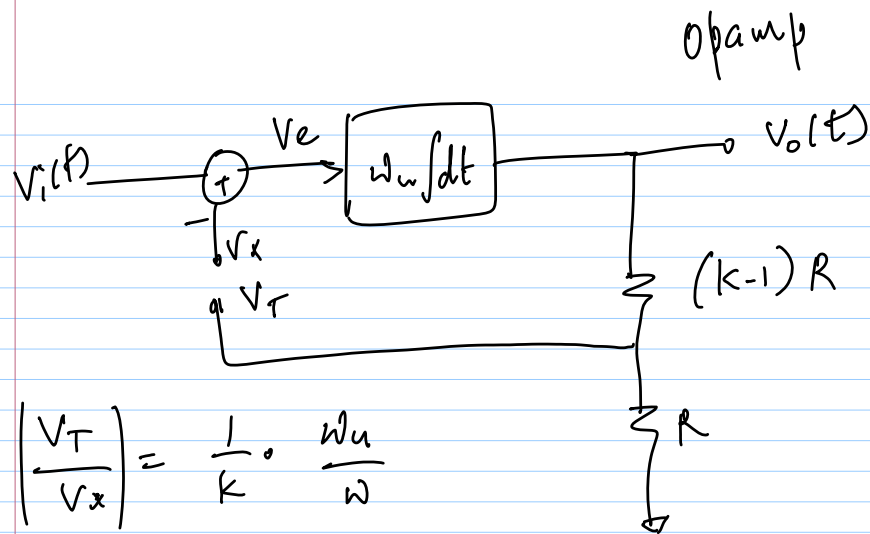
- 1) Root locus plot / Nyquist plot
- 2) Gain & phase margin

$\frac{1}{\text{gain}}$ @ phase = -180° is Gain Margin
 $(180^\circ + \text{phase})$ @ gain = 1 is phase margin
 \rightarrow good for rational polynomial systems



* # of encirclements of $(-1, 0) \leftarrow$
 $=$ # of RHP

$$CLTF = \frac{1}{f} \cdot \frac{L(s)}{1+L(s)}$$



$$\left| \frac{V_T}{V_X} \right| = \frac{1}{k} \cdot \frac{\omega_u}{\omega}$$

ideal opamp; $\omega_u = \infty$

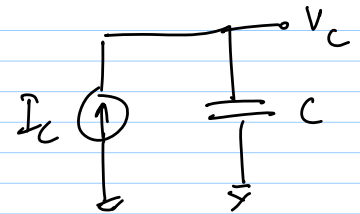
* Integration:
 use capacitors

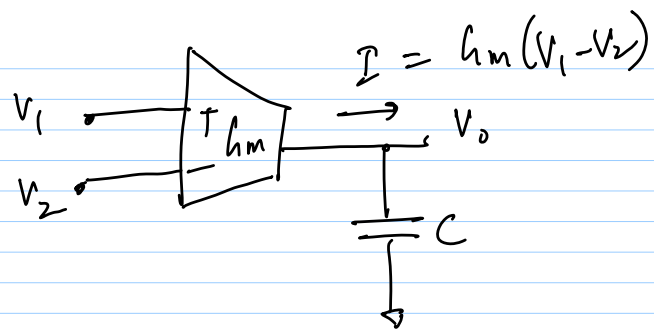
$$I = C \frac{dV}{dt}$$

$$1) \quad V_c = \frac{1}{C} \int I_c dt$$

$$2) \quad I_c \propto (V_1 - V_2) \leftarrow \begin{matrix} V_{CCS} \\ \text{or} \\ \text{transconductor} \end{matrix}$$

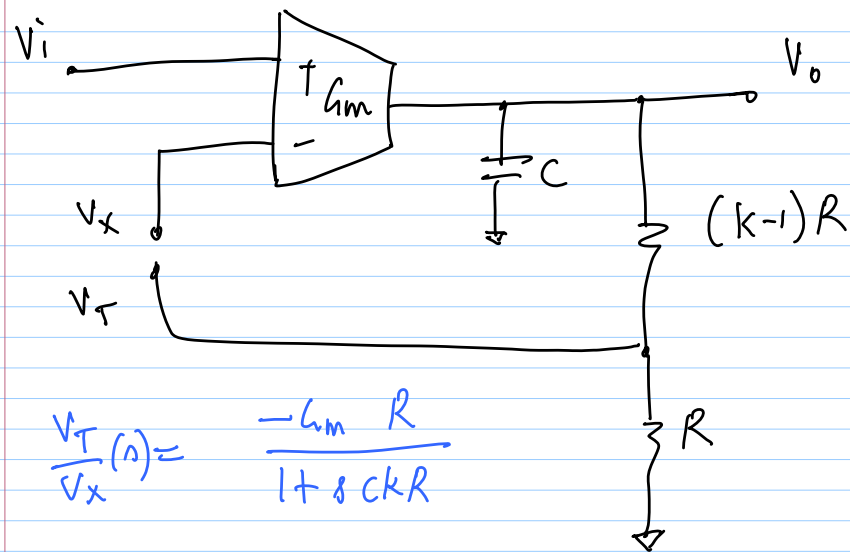
$$I_c = g_m (V_1 - V_2)$$



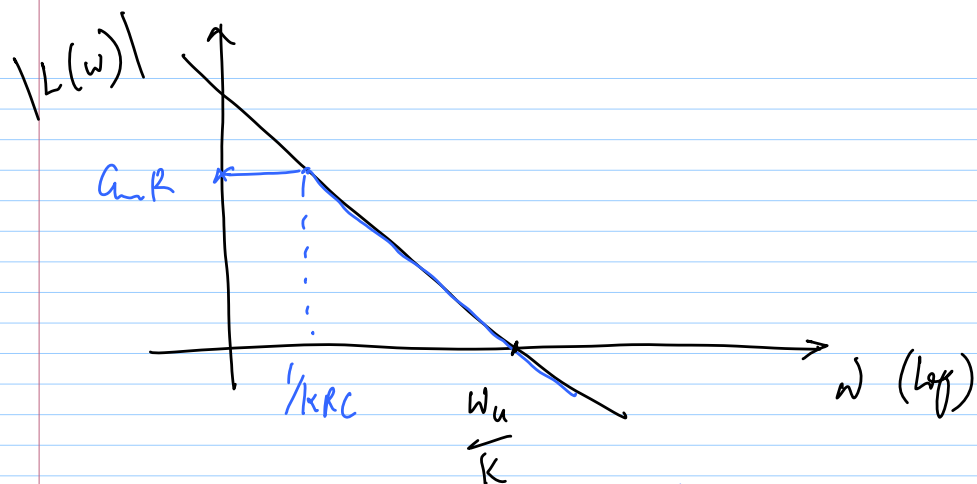


$$v_o = \frac{g_m}{C} \int (v_1 - v_2) dt$$

||
↓ ω



$$\frac{v_T}{v_x}(\omega) = \frac{-g_m R}{1 + sCR}$$



* DC gain = $g_m R$
 * pole @ $\frac{1}{kRC}$

* $\frac{v_T}{v_x}(\omega) = 1$
 when $\omega \approx \left(\frac{g_m}{kC}\right)$
 if $g_m R \gg 1$

