

## Designing a Buck converter

Specifications are given:

1.  $V_{in}$
2.  $V_{out}$
3. Line & load regulation
4. Line & load transient
5. Output ripple
6. Accuracy
7. Load current
8. Switching frequency may or may not be given
9. Efficiency may or may not be given (  $>90\%$  )

## deciding switching Frequency, L & C

→ switching losses should be negligible at higher load currents.

→  $\eta > 90\%$  ⇒ total loss  $\approx 10\%$ ,

$$V_{in} = 1.8V, \quad V_{out} = 1.2V, \quad I_{load\_max} = 1A$$

$$\eta = \frac{P_{out}}{P_{in}} = \frac{P_{out}}{P_{out} + P_{loss}}$$

$$1 + \frac{P_{loss}}{P_{out}} = \frac{1}{\eta}$$

$$\Rightarrow P_{loss} = \left( \frac{1}{\eta} - 1 \right) \times P_{out} = \left( \frac{1}{0.9} - 1 \right) \times P_{out} \\ \approx 11\%$$

$$11\% \text{ of } 1.2W = 132mW$$

$$P_{\text{loss-total}} = P_{\text{loss-cord}} + P_{\text{loss-sw}} + P_{\text{loss-magnetic}} + P_{\text{loss-}\phi}$$

At higher load currents.

$P_{\text{loss-cord}}$  should be dominant.

$P_{\text{loss-cord}} \geq 90\%$  of total loss.

$$P_{\text{loss-cord}} \approx 120 \text{ mW}$$

$$P_{\text{loss-total}} - P_{\text{loss-cord}} \approx 12 \text{ mW}$$

$$P_{\text{loss-cord}} = I_{\text{load}}^2 \times R_{\text{cord}}$$

$$R_{\text{cord}} = \frac{120 \text{ mW}}{(1)^2} = 120 \text{ m}\Omega$$

$$R_{\text{cord}} = R_{\text{dc}} + R_{\text{ac}}$$

→ Choosing lower  $R_{\text{ac}}$  will increase area & sweating loss.

→ we look for inductors with smallest possible  $R_{\text{dc}}$ .

Let's say  $R_{dcr} = 50 \text{ m}\Omega$

$$R_m = 70 \text{ m}\Omega$$

We need to size power FETs to have  $R_{dcr} = 70 \text{ m}\Omega$

$$R_m = D \cdot R_{mp} + (1-D) R_{mr}$$

$$D = 0.7$$

Case-1:  $R_{mp} = R_{mr} = 70 \text{ m}\Omega$

$$R_m = 70 \text{ m}\Omega$$

Case-2  $R_{mp} \neq R_{mr}$

$$R_{mp} = 50 \text{ m}\Omega$$

$$R_{mr} = 90 \text{ m}\Omega$$

$$R_m = 0.7 \times 50 \text{ m}\Omega + (1-0.7) 90 \text{ m}\Omega$$

$$= 35 \text{ m}\Omega + 27 \text{ m}\Omega = 62 \text{ m}\Omega$$

$$I_{d1} = \mu_{\text{cox}} \frac{W}{L} \left[ (V_{gs} - V_{th}) V_{ds} - \frac{V_{ds}^2}{2} \right]$$

for linear region  $V_{ds} \ll$

$$\frac{V_{ds}^2}{2} \approx 0$$

$$I_{d1} \approx \mu_{\text{cox}} \frac{W}{L} (V_{gs} - V_{th}) V_{ds}$$

$$R_{ds} = \frac{\partial V_{ds}}{\partial I_{d1}} = \frac{1}{\mu_{\text{cox}} \frac{W}{L} (V_{gs} - V_{th})}$$

↓  
drain-source voltage.

$$V_{dd} = 1.8V, V_{th} \approx 0.5V$$

$$R_{ds} = \frac{1}{\mu_{\text{cox}} \frac{W}{L} (1.3)}$$

$$R_{ds} = 70\Omega$$

$$W/L = \frac{1}{\mu_{\text{cox}} (70\Omega) (1.3)}$$

$$\mu_{p \text{ cor}} = 70 \mu A / V^2$$

$$\left( \frac{\omega}{L} \right)_{\text{pms}} = \frac{1}{70 \times 10^6 (70 \times 10^{-3}) (1.3)} = \frac{10^9}{70 \times 70 \times 1.3}$$

$$\approx 1.6 \times 10^5 = \omega / L$$

$$L = 180 \mu\text{m}$$

$$\omega = 0.288 \times 10^5 \mu\text{m}$$

$$= \underline{\underline{28.8 \text{ mm}}}$$