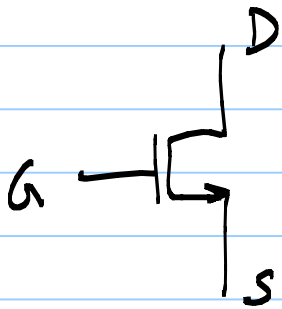


29/10/2020

Lecture 47

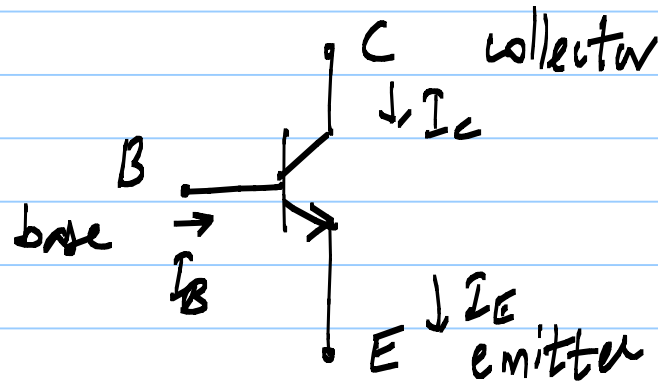
Bipolar Junction Transistor (BJT)



NMOS

cause - V_{gs}

effect - I_D



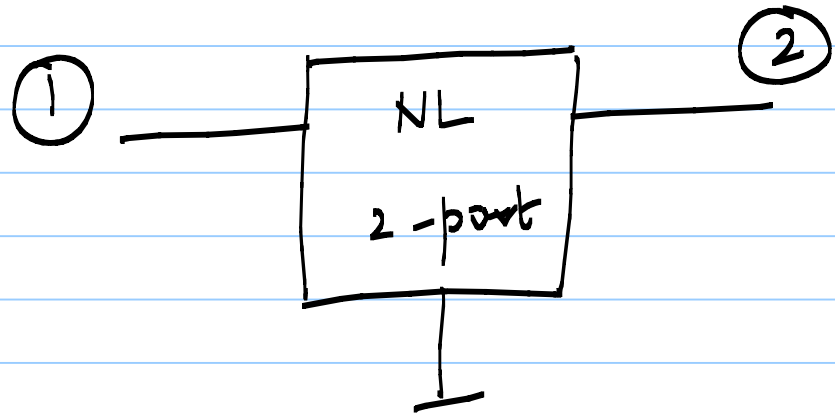
NPN transistor

V_{BE} voltage

controls I_C

cause - V_{BE}

effect - I_C



$$[y] = \begin{bmatrix} 0 & 0 \\ y_{21} & 0 \end{bmatrix}$$

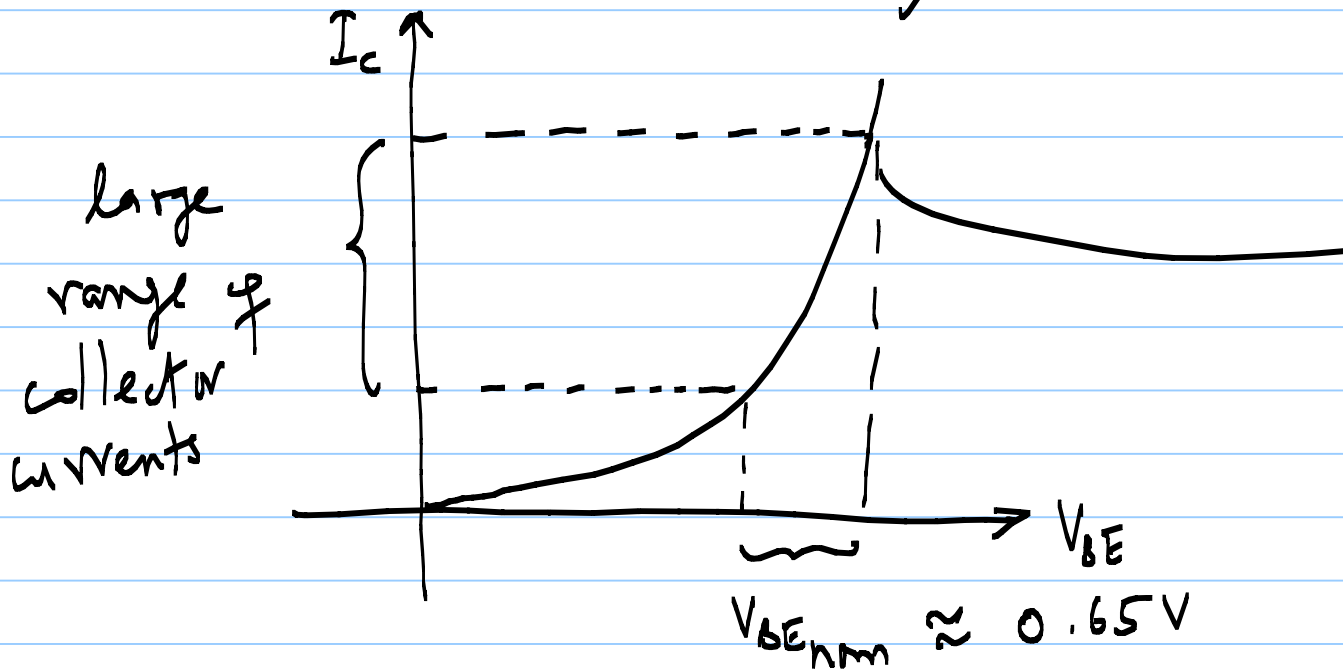
|
as large as possible

$$I_1 = \text{constant}$$

$$I_2 = g(V_1)$$

BJT also

shares these characteristics

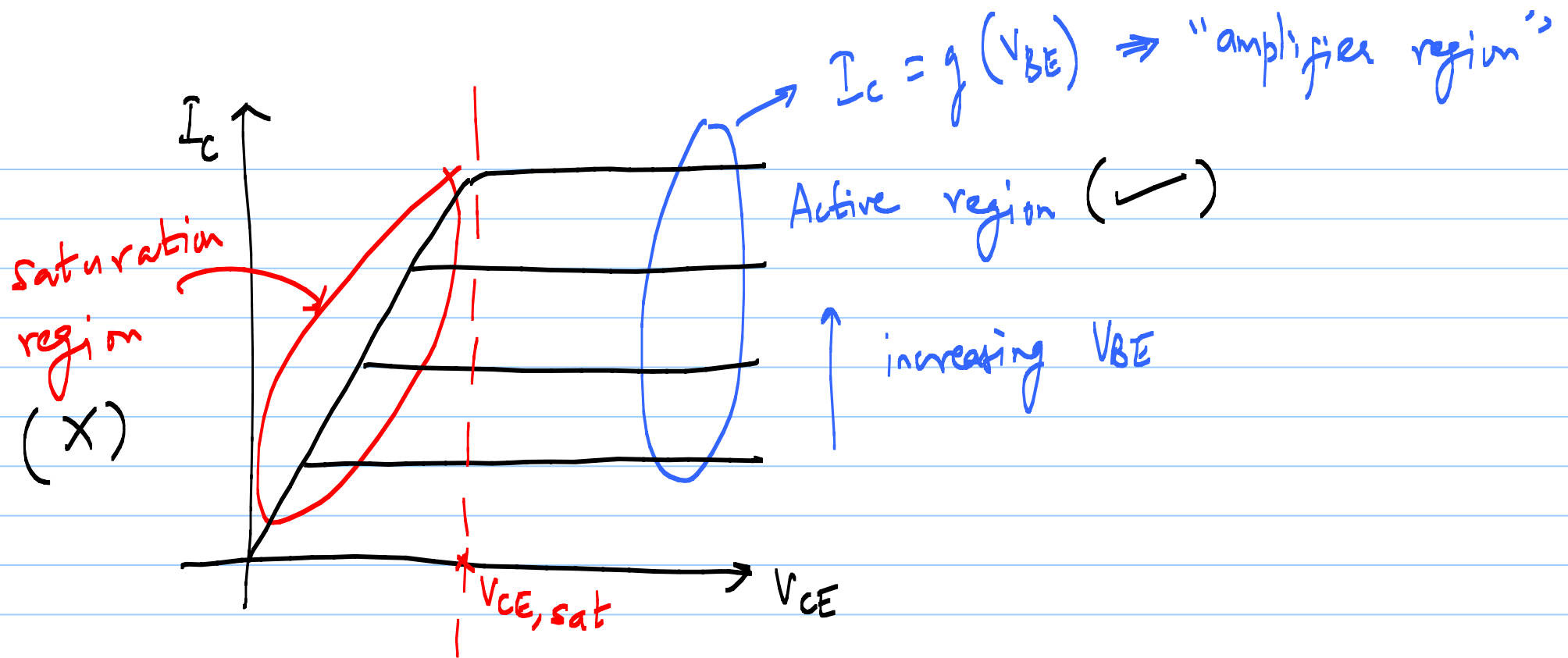


large range of collector currents

$$I_c = I_s \left[\exp\left[\frac{V_{BE}}{V_t}\right] - 1 \right]$$

$I_B = \text{very small}$

$$V_t = \frac{kT}{q} \approx 25\text{mV}$$



When $V_{CE} > V_{CE,sat} \Rightarrow$ good amplifier

$$V_{BE,on} \approx 0.65V, \quad V_t \approx 25mV$$

* $I_C \approx I_S \exp\left(\frac{V_{BE}}{V_t}\right)$

* $V_{BE} = V_t \ln\left(\frac{I_C}{I_S}\right)$

$$* \quad I_B = \frac{I_C}{\beta}$$

β = current gain of BJT
 $\sim 50 - 200$, typically

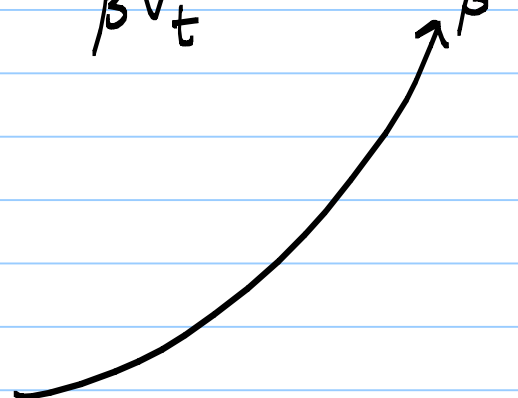
$$* \quad I_E = I_C + I_B = (\beta + 1) I_B = \left(\frac{\beta + 1}{\beta} \right) I_C$$

* Small signal parameters:

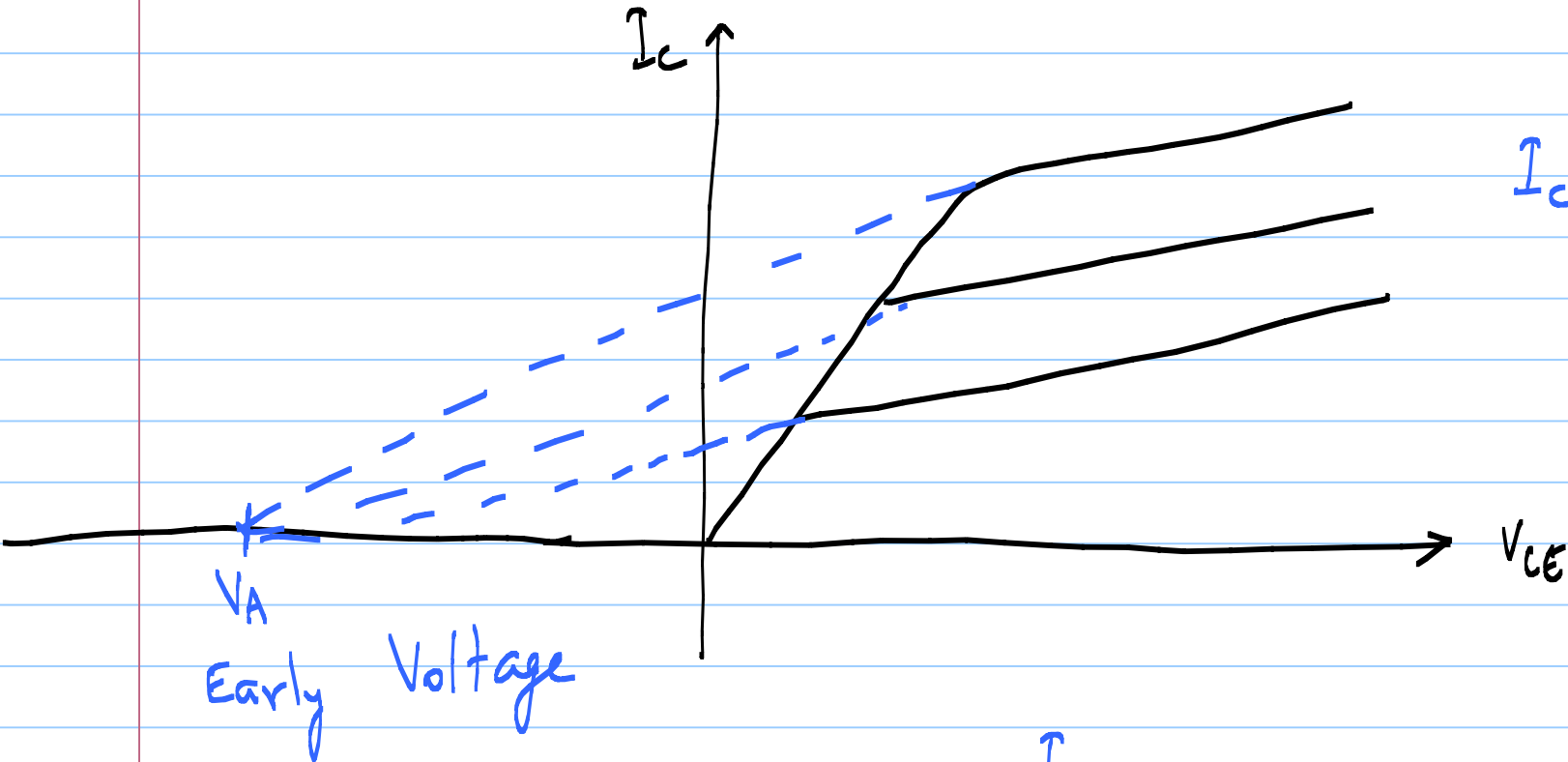
$$y_{11} = \frac{\partial I_B}{\partial V_{BE}} = \frac{1}{\beta} \frac{\partial I_C}{\partial V_{BE}} = \frac{I_C}{\beta V_t} = \frac{g_m}{\beta}$$

$$y_{12} = \frac{\partial I_B}{\partial V_{CE}} = 0$$

$$y_{21} = \frac{\partial I_C}{\partial V_{BE}} = \frac{I_C}{V_t} = g_m$$



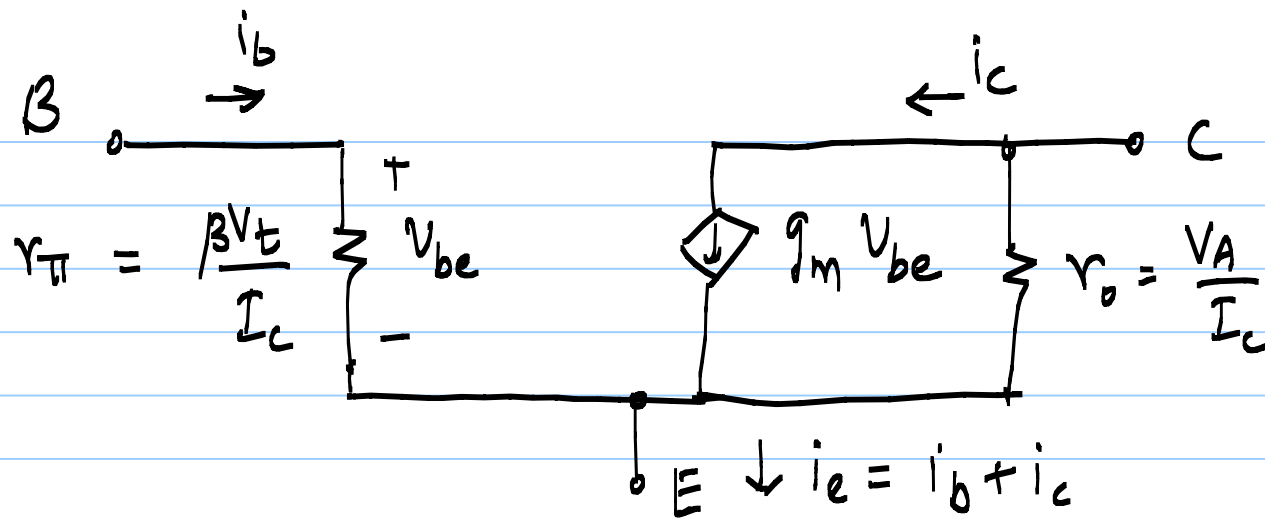
$$y_{22} = \frac{\partial I_c}{\partial V_{CE}} = 0 \quad \left\{ \begin{array}{l} \text{very small in a} \\ \text{real device} \end{array} \right\}$$



$$I_c = \left[I_s \exp\left(\frac{V_{BE}}{V_T}\right) \right] \left[1 + \frac{V_{CE}}{V_A} \right]$$

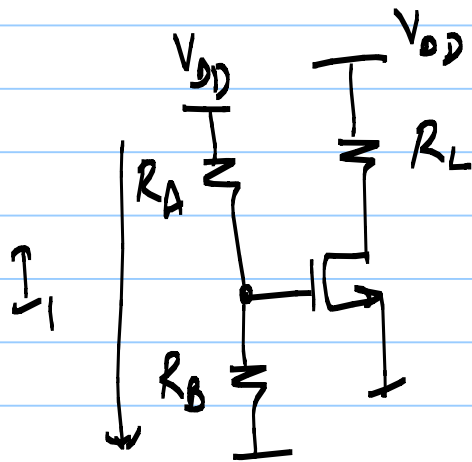
$V_A = -\infty$ for an ideal device with $y_{22} = 0$

actual $y_{22} = \frac{I_c}{V_A}$

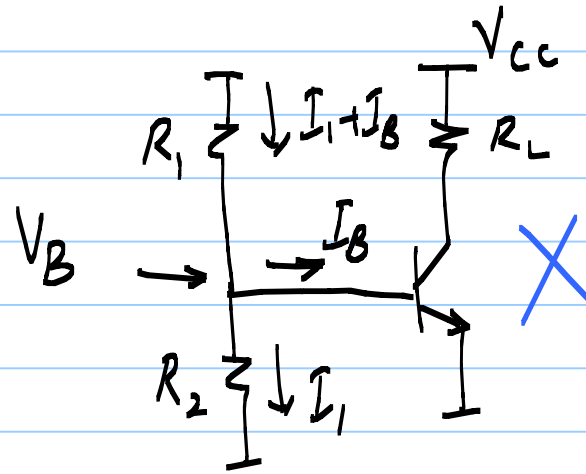


Other small-signal representations exist

BJT Amplifiers

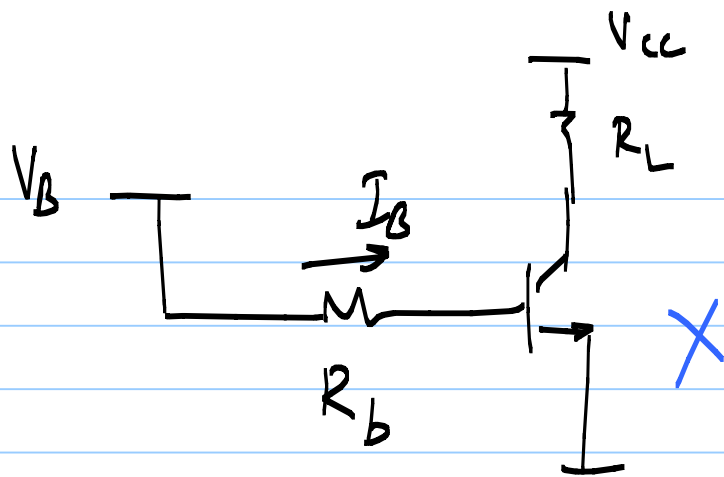


choose R_A, R_B so that
 $R_A || R_B \gg R_S$



i.e. $V_B = f(I_B)$
 $= f(I_C)$

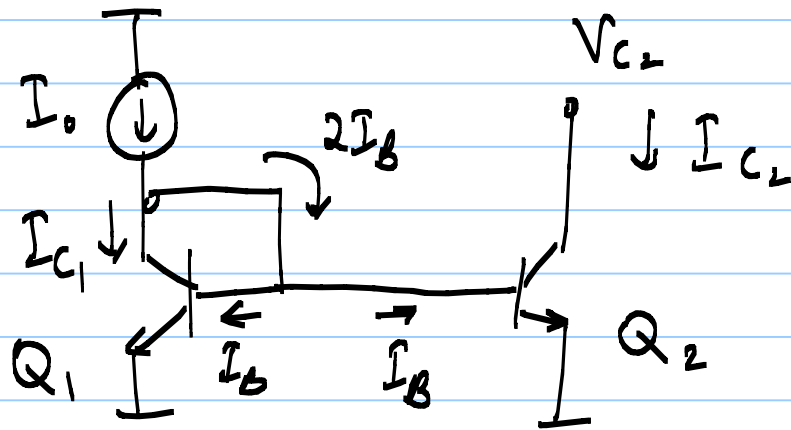
V_B will not be equal to desired bias value due to additional drop across R_1



BJT current mirror

o)

$Q_1 \cong Q_2$



$$I_{C1} = I_0 - 2I_B$$

$$I_B = \frac{I_{C1}}{\beta}$$

$$I_{C1} = \frac{I_0 \cdot \beta}{\beta + 2}$$

$$V_{BE1} = V_{BE2} \Rightarrow I_{C1} = I_{C2} \Rightarrow I_{B1} = I_{B2} = I_B$$

When $V_{C2} > V_{CEsat}$