

Tutorial 7 - Solutions

$$1) \quad \vec{E}(\vec{r}, t) = \vec{A}_e(\vec{r}) \cdot \cos(\omega t - \varphi_e(\vec{r}))$$

$$\vec{H}(\vec{r}, t) = \vec{A}_h(\vec{r}) \cos(\omega t - \varphi_h(\vec{r}))$$

a) Complex envelope of a monochromatic vector field $\vec{v}(\vec{r}, t)$ is given by

$$\vec{v}(\vec{r}, t) = \text{Re} \left\{ \underbrace{\tilde{v}(\vec{r})}_{\substack{\text{complex} \\ \text{envelope}}} \cdot e^{i\omega t} \right\}$$

Now, from above eq^(m)

$$\vec{E}(\vec{r}, t) = \text{Re} \left\{ \underbrace{\vec{A}_e(\vec{r}) e^{-i\varphi_e(\vec{r})}}_{\tilde{E}(\vec{r})} \cdot e^{i\omega t} \right\}$$

$$\vec{H}(\vec{r}, t) = \text{Re} \left\{ \underbrace{\vec{A}_h(\vec{r}) e^{-i\varphi_h(\vec{r})}}_{\tilde{H}(\vec{r})} \cdot e^{i\omega t} \right\}$$

b) In terms of complex envelope $\tilde{E}(\vec{r}), \tilde{H}(\vec{r})$

$$\vec{E}(\vec{r}, t) = \text{Re} \left\{ \tilde{E}(\vec{r}) \cdot e^{i\omega t} \right\} = \frac{\tilde{E}(\vec{r}) \cdot e^{i\omega t} + \tilde{E}^*(\vec{r}) e^{-i\omega t}}{2}$$

$$\vec{H}(\vec{r}, t) = \text{Re} \left\{ \tilde{H}(\vec{r}) \cdot e^{i\omega t} \right\} = \frac{\tilde{H}(\vec{r}) \cdot e^{i\omega t} + \tilde{H}^*(\vec{r}) e^{-i\omega t}}{2}$$

$$\vec{S}(\vec{r}, t) = \vec{E}(\vec{r}, t) \times \vec{H}(\vec{r}, t)$$

$$= \frac{1}{4} \left[\tilde{E}(\vec{r}) \times \tilde{H}^*(\vec{r}) + \tilde{E}^*(\vec{r}) \times \tilde{H}(\vec{r}) + \tilde{E}(\vec{r}) \times \tilde{H}(\vec{r}) \cdot e^{2i\omega t} + \tilde{E}^*(\vec{r}) \times \tilde{H}^*(\vec{r}) \cdot e^{-2i\omega t} \right]$$

$$\Rightarrow \langle S(\vec{r}, t) \rangle = \tilde{S}(\vec{r}) = \frac{\tilde{E} \times \tilde{H}^*(\vec{r}) + \tilde{E}^*(\vec{r}) \times \tilde{H}(\vec{r})}{2 \times 2} \quad \left(\text{used } \langle e^{\pm 2i\omega t} \rangle = 0 \right)$$

$$= \frac{1}{2} \text{Re} \left\{ \tilde{E}(\vec{r}) \times \tilde{H}^*(\vec{r}) \right\}$$

$$2) a) \tilde{E}_f(x) = \hat{z} E_0 e^{-ik_0 x} \quad \tilde{E}_b(x) = \hat{z} e^{-i\phi_0} E_0 e^{ik_0 x}$$

Net complex envelope

$$\begin{aligned} \tilde{E}(x) &= \hat{z} E_0 [e^{-ik_0 x} + e^{-i\phi_0} e^{ik_0 x}] \\ &= \hat{z} E_0 e^{-i\phi_0/2} [e^{i(k_0 x - \phi_0/2)} + e^{i(k_0 x - \phi_0/2)}] \\ &= 2\hat{z} E_0 e^{-i\phi_0/2} \cos(k_0 x - \frac{\phi_0}{2}) \end{aligned}$$

The real electric field:

$$\vec{E}(x,t) = \text{Re}\{\tilde{E}(x) \cdot e^{i\omega t}\}$$

$$\boxed{\vec{E}(x,t) = 2 E_0 \cos(\omega t - \frac{\phi_0}{2}) \cos(k_0 x - \frac{\phi_0}{2}) \hat{z}}$$

To compute $\vec{H}(x,t)$, use Faraday's law:

$$\nabla \times \vec{E}(x,t) = -\mu_0 \frac{\partial \vec{H}(x,t)}{\partial t}$$

Now

$$\nabla \times \vec{E}(x,t) = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{\partial}{\partial x} & 0 & 0 \\ 0 & 0 & 2E_0 \cos(k_0 x - \frac{\phi_0}{2}) \cos(\omega t - \frac{\phi_0}{2}) \end{vmatrix}$$

$$= \hat{y} 2E_0 k_0 \sin(k_0 x - \frac{\phi_0}{2}) \cos(\omega t - \frac{\phi_0}{2})$$

$$\Rightarrow \boxed{\vec{H}(x,t) = -\frac{2E_0 k_0}{\omega \mu_0} \hat{y} \sin(k_0 x - \frac{\phi_0}{2}) \sin(\omega t - \frac{\phi_0}{2})}$$

b) Poynting vector

$$\vec{S}(x,t) = \vec{E}(x,t) \times \vec{H}(x,t)$$

$$= \frac{4E_0^2 k_0}{\omega \mu_0} \hat{x} \sin(k_0 x - \frac{\phi_0}{2}) \cos(k_0 x - \frac{\phi_0}{2}) \sin(\omega t - \frac{\phi_0}{2}) \cos(\omega t - \frac{\phi_0}{2})$$

$$= \frac{E_0^2 k_0}{\omega \mu_0} \sin(2k_0 x - \phi_0) \sin(2\omega t - \phi_0)$$

Hence

$$\langle \vec{S}(x,t) \rangle = 0 \quad \left(\text{since } \langle \sin(2\omega t - \frac{\phi_0}{2}) \rangle = 0 \right)$$

Physically this is expected since the forward and backward travelling waves ~~are~~ have equal amplitudes and hence carry the same power per unit area — this bidirectional flow of power results in 0 net power transfer. However, it should be noted that the instantaneous power transfer is not 0, only average power transfer is 0. (i.e. $\vec{S}(x,t) \neq 0$, $\langle \vec{S}(x,t) \rangle = 0$).

3) In conductor

$$k^2 = \omega^2 \mu_0 \epsilon_0 \left[\epsilon - \frac{i\sigma}{\omega \epsilon_0} \right] \quad \text{--- (1)}$$

and a forward propagating wave has a complex envelope (time variation $\sim e^{+i\omega t}$).

$$\vec{E}(x,0) = E_0 \hat{z} e^{-ikx} \quad \text{--- (2)}$$

From (1), k is complex. Also, let $k = k_R - ik_I$ (note that $k_I > 0$, else (2) would imply an electric field which grows exponentially with x along propagation direction). Thus

$$\vec{E}(x) = \hat{z} E_0 e^{-ik_R x} e^{-k_I x}$$

and

$$\vec{E}(x,t) = \hat{z} E_0 e^{-k_I x} \cos(k_R x - \omega t)$$

The electrical energy per unit volume is given by

$$u_E(x,t) = \frac{1}{2} \epsilon_0 \epsilon E^2 = \frac{1}{2} \epsilon_0 \epsilon E_0^2 e^{-2k_I x} \cos^2(k_R x - \omega t)$$

Thus $\langle u_E(x,t) \rangle = \frac{1}{4} \epsilon_0 \epsilon E_0^2 e^{-2k_I x}$.

To compute magnetic field, we first calculate $\tilde{H}(x)$ using Faraday's law (you can also directly calculate $\vec{H}(x,t)$, but this is an alternative procedure which might be somewhat simpler).

$$\begin{aligned} \nabla \times \tilde{E}(x) &= -i\omega\mu_0 \tilde{H}(x) \\ \Rightarrow \tilde{H}(x) &= \frac{i}{\omega\mu_0} \nabla \times \tilde{E}(x) = -\frac{i}{\omega\mu_0} \frac{\partial \tilde{E}}{\partial x} \cdot \hat{y} \\ &\quad \xrightarrow{\text{(Prove this)}} \\ &= \frac{i}{\omega\mu_0} (k_I + ik_R) \cdot E_0 e^{-k_I x} e^{-ik_R x} \hat{y} \end{aligned}$$

Thus
$$\begin{aligned} \vec{H}(x,t) &= \text{Re} \left[\tilde{H}(x) \cdot e^{i\omega t} \right] \\ &= \text{Re} \left[\frac{i}{\omega\mu_0} (k_I + ik_R) E_0 e^{-k_I x} e^{-ik_R x} \hat{y} \right] \\ &= \frac{E_0 [k_I^2 + k_R^2]^{1/2}}{\omega\mu_0} \cos(k_R x + \omega t + \frac{\pi}{2} + \tan^{-1} \frac{k_R}{k_I}) e^{-k_I x} \hat{y} \end{aligned}$$

Hence
$$u_H(x,t) = \frac{1}{2} \mu_0 H^2 = \frac{E_0^2 (k_I^2 + k_R^2)}{2\omega^2 \mu_0} e^{-2k_I x} \cos^2 \left(\omega t - k_R x + \frac{\pi}{2} + \tan^{-1} \frac{k_R}{k_I} \right)$$

$$\Rightarrow \langle u_H(x,t) \rangle = \frac{E_0^2}{4\omega^2 \mu_0} (k_I^2 + k_R^2) \cdot e^{-2k_I x}$$

To compare the two, consider the ratio:

$$\frac{\langle u_H(x,t) \rangle}{\langle u_E(x,t) \rangle} = \left[\frac{k_I^2 + k_R^2}{\omega^2 \mu_0 \epsilon_0 \epsilon} \right]$$

Now, for large σ , we have from Eq. ①

$$k^2 = (k_R - i k_I)^2 \approx - \frac{\omega^2 \mu_0 \epsilon_0 \cdot i \sigma}{\omega \epsilon_0} = + \omega \mu_0 \sigma e^{-i\pi/2}$$

$$\Rightarrow k_R - i k_I = \sqrt{\omega \mu_0 \sigma} e^{-i\pi/4} = \sqrt{\frac{\omega \mu_0 \sigma}{2}} (1 - i)$$

$$\Rightarrow k_R = k_I = \sqrt{\frac{\omega \mu_0 \sigma}{2}}$$

and

$$\frac{\langle u_H \rangle}{\langle u_E \rangle} = \frac{\omega^2 \mu_0 \sigma}{\omega^2 \mu_0 \epsilon_0 \epsilon} = \frac{\sigma}{\omega \epsilon_0 \epsilon} \gg 1$$

therefore magnetic energy dominates in this media.

4) a) $\vec{E}(x=0, t) = \hat{z} E_0 e^{i\omega_0 t} e^{-t^2/\tau_0^2} = \int_{-\infty}^{\infty} \tilde{E}(\omega) e^{i\omega t} d\omega$

$$\Rightarrow \tilde{E}(\omega) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \hat{z} E_0 e^{i\omega_0 t} e^{-t^2/\tau_0^2} e^{-i\omega t} dt$$

$$= \frac{E_0 \hat{z}}{2\pi} \sqrt{\frac{\pi}{1/\tau_0^2}} e^{-\frac{\tau_0^2(\omega - \omega_0)^2}{4}}$$

(use the standard integral: $\int_{-\infty}^{\infty} e^{-(ax^2+bx)} dx = \sqrt{\frac{\pi}{a}} e^{b^2/4a}$)

$$\tilde{E}(\omega) = \frac{1}{2\sqrt{\pi}} E_0 \tau \hat{z} e^{-\frac{\tau_0^2}{4}(\omega - \omega_0)^2}$$

$$b) \vec{E}(z,t) = \int_{-\infty}^{\infty} \vec{E}(\omega) \cdot e^{i(\omega t - k(\omega)z)} d\omega$$

$$= \int_{-\infty}^{\infty} \frac{E_0 \tau_0 \hat{z}}{2\sqrt{\pi}} e^{-\frac{\tau_0^2}{4}(\omega - \omega_0)^2} e^{i\omega t} e^{-i\left\{\frac{\omega_0}{v_p} + \frac{\omega - \omega_0}{v_g} + \frac{\alpha}{2}(\omega - \omega_0)^2\right\}z} d\omega$$

Making change of variables $\omega - \omega_0 = \Omega$

$$\vec{E}(z,t) = \frac{E_0 \tau_0 \hat{z}}{2\sqrt{\pi}} \left[\int_{-\infty}^{\infty} d\Omega \cdot e^{-\frac{\tau_0^2 \Omega^2}{4}} e^{i\Omega(t - \frac{z}{v_g})} e^{-i\frac{\alpha \Omega^2 z}{2}} \right]$$

$$\times e^{i(\omega_0 t - \frac{\omega_0 z}{v_p})}$$

$$= \frac{\hat{z} E_0 \tau_0}{2\sqrt{\pi}} e^{i\omega_0(t - \frac{z}{v_p})} \left[\int_{-\infty}^{\infty} d\Omega \cdot e^{-\left(\frac{\tau_0^2}{4} + i\frac{\alpha z}{2}\right)\Omega^2} e^{i\Omega(t - \frac{z}{v_g})} \right]$$

$$= \frac{\hat{z} E_0 \tau_0}{2\sqrt{\pi}} e^{i\omega_0(t - \frac{z}{v_p})} \left[\frac{\sqrt{\pi}}{\frac{\tau_0^2}{4} + i\frac{\alpha z}{2}} \right]^{1/2} e^{-\left\{\frac{(t - z/v_g)^2}{\tau_0^2 + 2i\alpha z}\right\}}$$

(using: $\int_{-\infty}^{\infty} e^{-(ax^2 + bx)} dx = e^{\frac{b^2}{4a}} \sqrt{\frac{\pi}{a}}$)

$$\vec{E}(z,t) = \frac{\hat{z} E_0}{\left[1 + \frac{2i\alpha z}{\tau_0^2}\right]^{1/2}} e^{-\frac{(t - z/v_g)^2}{\tau_0^2 + 2i\alpha z}} e^{i\omega_0(t - \frac{z}{v_p})}$$

c) The amplitude of electric field:

$$|\vec{E} \cdot \hat{z}| = \frac{E_0}{\left[1 + \frac{4\alpha^2 z^2}{\tau_0^4}\right]^{1/4}} \left| e^{-\frac{(t - z/v_g)^2}{\tau_0^2 + 2i\alpha z}} \right|$$

$$= \frac{E_0}{\left[1 + \frac{4\alpha^2 z^2}{\tau_0^4}\right]^{1/2}} \cdot e^{-\frac{(t - z/v_g)^2}{\tau_0^2 + 4\alpha^2 z^2}} \cdot \tau_0^2 \left| e^{\frac{2i\alpha z}{\tau_0^4 + 4\alpha^2 z^2} (t - z/v_g)^2} \right|$$

$$|\vec{E}, \hat{z}| = \frac{E_0}{\left(1 + \frac{4\alpha^2 x^2}{\tau_0^4}\right)^{1/4}} e^{-\frac{(t - x/v_g)^2}{(\tau_0^2 + 4\alpha^2 x^2/\tau_0^2)}}$$

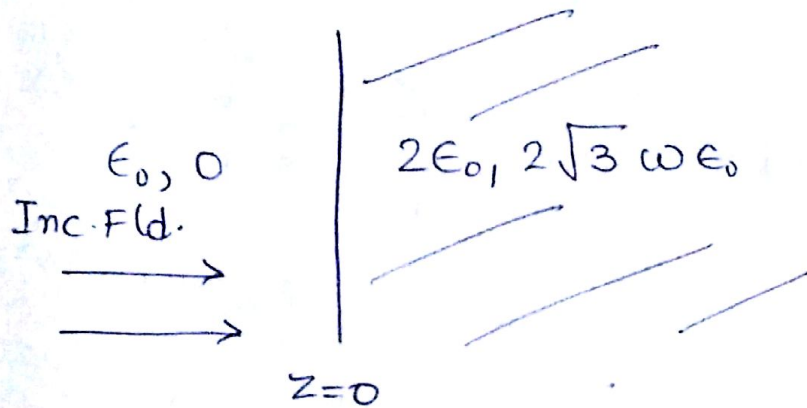
Thus

$$\tau(x) = \sqrt{\tau_0^2 + \frac{4\alpha^2 x^2}{\tau_0^2}} > \tau_0$$

and hence the electric field pulse broadens with ~~time~~ propagation.

For large x , $\tau(x) \approx \frac{2\alpha x}{\tau_0} \Rightarrow \frac{\Delta\tau}{\Delta x} = \frac{2\alpha}{\tau_0}$

5) a).



Since incident field is in vacuum

$$k = \frac{\omega}{c}$$

The complex electric field:

$$\vec{E}_{inc} = \hat{x} E_0 e^{-ikz}$$

$$\Rightarrow \vec{H}_{inc} = \frac{k E_0}{\omega \mu_0} \hat{y} e^{-ikz}$$

$$\Rightarrow \vec{H}_{inc} = \frac{k E_0}{\omega \mu_0} \cos(\omega t - k z) \hat{y}$$

We will solve problem in terms of complex fields.

b) let

$$\vec{E}_{\text{refl}} = \Gamma E_0 e^{+ik_c z} \hat{y} \quad (\text{reflected backward travelling wave}).$$

$$\vec{E}_{\text{tran}} = \tau E_0 e^{-ik_c z} \hat{y} \quad (\text{transmitted forward travelling wave}).$$

where Γ is reflection coefficient, τ is transmission coefficient and k_c is wave-number / prop. constant in the conductor.

$$k_c^2 = \omega^2 \mu_0 \epsilon_0 \left[\epsilon_r - \frac{i\sigma}{\omega \epsilon_0} \right]$$

$$= \frac{\omega^2}{c^2} \left[2 - i2\sqrt{3} \right]$$

$$= \frac{\omega^2}{c^2} \cdot 4 \left[\frac{1}{2} - i\frac{\sqrt{3}}{2} \right] = \frac{4\omega^2}{c^2} e^{-i\pi/3}$$

$$\Rightarrow k_c = \frac{2\omega}{c} e^{-i\pi/6} = \frac{2\omega}{c} \left[\frac{\sqrt{3}}{2} - \frac{i}{2} \right].$$

Hence,

$$\vec{E}_{\text{refl}} = \Gamma E_0 e^{ik_c z} \hat{y}$$

$$\vec{E}_{\text{tran}} = \tau E_0 e^{i k_0 \sqrt{3} z} e^{-k_0 z} \hat{y} \quad (k_0 = \frac{\omega}{c})$$

Imposing continuity of parallel \vec{E} at $z=0$,

$$1 + \Gamma = \tau \quad \text{--- (1)}$$

Now, compute magnetic fields:

$$\vec{H}_{\text{inc}} = \frac{k_0 E_0}{\omega \mu_0} e^{ik_c z} \hat{y} \quad \vec{H}_{\text{refl}} = -\frac{k_0 E_0 \Gamma}{\omega \mu_0} e^{-ik_c z} \hat{y}$$

$$\vec{H}_{\text{tran}} = \frac{(k_0 \sqrt{3} - ik_0)}{\omega \mu_0} E_0 \tau e^{-ik_0 \sqrt{3} z} e^{-k_0 z} \hat{y}$$

Imposing contⁿ of parallel \vec{H} at $z=0$,

$$\frac{k_0 \epsilon_0}{\omega \mu_0} - \frac{k_0 \epsilon_0 \Gamma}{\omega \mu_0} = \frac{k_0 \epsilon_0}{\omega \mu_0} \tau (\sqrt{3} - i).$$

$$\Rightarrow 1 - \Gamma = \tau (\sqrt{3} - i) \quad \text{--- (2)}$$

Solve (1) and (2) to obtain Γ and τ .

$$\tau = \frac{2}{(1 + \sqrt{3} - i)} \approx 0.687 \angle 20.1^\circ$$

$$\Gamma = \frac{(1 + i - \sqrt{3})}{(1 + \sqrt{3} - i)} \approx 0.426 \angle 14.6^\circ$$

Thus real reflected field:

$$\vec{E}_{\text{refl}} = 0.687 E_0 \cos(\omega t + k_0 z + 20.1^\circ) \hat{y}$$

real transmitted field

$$\vec{E}_{\text{tran}} = 0.426 E_0 \cos(\omega t - k_0 \sqrt{3} z + 14.6^\circ) \cdot e^{-k_0 z} \hat{y}$$

6) a) clearly, field in II would be 0 since there is metal in that region. In region III, the field would also be 0 since the EM wave could not propagate through metal. We explicitly compute field in region I - the same procedure can be followed to rigorously show that the field in region III is 0. Again, we work with complex fields.

$$\vec{E}_{\text{inc}} = E_0 (8\hat{x} + 6\hat{y} + 5\hat{z}) \sin \left[\omega t - \frac{\omega}{5c} (3x - 4y) \right]$$

$$\Rightarrow \tilde{E}_{\text{inc}} = -i E_0 (8\hat{x} + 6\hat{y} + 5\hat{z}) e^{-i \frac{\omega}{5c} (3x - 4y)}$$

reflected wave would again be a plane wave. let

us assume

$$\tilde{E}_{\text{refl}} = E_0 (a_x \hat{x} + a_y \hat{y} + a_z \hat{z}) e^{i(k_x x + k_y y)}$$

Since reflected wave should propagate away from the interface at $x=0$, $k_x > 0$. Also, $k_x = \sqrt{k_0^2 - k_y^2}$.

At $x=0$, parallel components of \vec{E} vanish. Thus

$$\hat{z} \cdot (\vec{E}_{inc} + \vec{E}_{refl}) \Big|_{x=0} = 0 \quad \text{--- (1)}$$

$$\hat{y} \cdot (\vec{E}_{inc} + \vec{E}_{refl}) \Big|_{x=0} = 0 \quad \text{--- (2)}$$

From (1),

$$\left[-i5 e^{i \frac{4\omega y}{5c}} + a_z e^{ik_y y} \right] = 0$$

$$\Rightarrow a_z = 5i, \quad k_y = \frac{4\omega}{5c}$$

From (2)

$$\left[-i6 e^{i \frac{4\omega y}{5c}} + a_y e^{ik_y y} \right] = 0$$

$$\Rightarrow a_y = 6i, \quad k_y = \frac{4\omega}{5c}$$

To calculate a_x , we use the fact that $\nabla \cdot \vec{E}_{refl} = 0$

$$\Rightarrow \frac{\partial(\vec{E}_{refl} \cdot \hat{x})}{\partial x} + \frac{\partial(\vec{E}_{refl} \cdot \hat{y})}{\partial y} + \frac{\partial(\vec{E}_{refl} \cdot \hat{z})}{\partial z} = 0$$

$$\Rightarrow ik_x a_x + ik_y a_y = 0$$

$$\Rightarrow a_x = -\frac{k_y}{k_x} a_y = -\frac{k_y}{[k_0^2 - k_y^2]^{1/2}} a_y$$

$$= -\frac{4\omega/5c}{\left[\frac{\omega^2}{c^2} - \frac{16\omega^2}{25c^2} \right]^{1/2}} (6i) = -8i$$

Thus

$$\vec{E}_{refl} = i \left[-8\hat{x} + 6\hat{y} + 5\hat{z} \right] E_0 e^{i \frac{\omega}{5c} (3x + 4y)}$$

$$\Rightarrow \vec{E}_{refl} = -E_0 \left[-8\hat{x} + 6\hat{y} + 5\hat{z} \right] \sin \left(\omega t + \frac{3\omega x}{5c} + \frac{4\omega y}{5c} \right)$$

Hence, total field in region I-

$$\vec{E} = \vec{E}_{inc} + \vec{E}_{refl.}$$

$$= 8\hat{x} E_0 \left\{ \sin\left(\omega t - \frac{3\omega x}{5c} + \frac{4\omega y}{5c}\right) + \sin\left(\omega t + \frac{3\omega x}{5c} + \frac{4\omega y}{5c}\right) \right\} + (6\hat{y} + 5\hat{z}) \cdot E_0 \left\{ \sin\left(\omega t - \frac{3\omega x}{5c} + \frac{4\omega y}{5c}\right) - \sin\left(\omega t + \frac{3\omega x}{5c} + \frac{4\omega y}{5c}\right) \right\}$$

$$\vec{E} = 16\hat{x} E_0 \sin\left(\omega t + \frac{4\omega y}{5c}\right) \cos\left(\frac{3\omega x}{5c}\right) - (12\hat{y} + 10\hat{z}) E_0 \sin\left(\frac{3\omega x}{5c}\right) \cos\left(\omega t + \frac{4\omega y}{5c}\right)$$

Note that this resembles a standing wave in x - a consequence of the metal being perfect and hence reflectivity being 1.

b) For a near perfect conductors, fields would exponentially decay inside instead of exactly zero. In

this case

$$k_c^2 = \frac{\omega^2}{c^2} \left[\epsilon_r - \frac{i\sigma}{\omega\epsilon_0} \right]$$

$$= \frac{\omega^2}{c^2} \cdot [1 - 2i]$$

$$= \frac{\omega^2}{c^2} \sqrt{5} \cdot e^{-i63.4^\circ}$$

$$\Rightarrow k_c = \frac{\omega}{c} \cdot 5^{1/4} e^{-i31.7^\circ}$$

$$= \frac{\omega}{c} (1.27 - i0.79)$$

Thus, field magnitude varies as $\sim \exp\left(-\frac{0.79\omega x}{c}\right)$ from conductor surface.

If d is large enough to ensure

$$\exp\left(-\frac{0.79 \omega d}{c}\right) \approx \exp(-5) \approx 0$$

no significant fields would be detected in region III.

$$\Rightarrow d \sim \left[\frac{5 \cdot c}{0.79 \omega} \right] \approx \lambda_0$$

where

$$\lambda_0 = \frac{2\pi c}{\omega} \text{ is the free space wavelength}$$

