

Monopoles and Dipoles

- Monopoles and dipoles are widely used antennas in wireless communications systems.
- Monopoles are particularly popular for portable units and on automobiles and other vehicles.
- In practice, wide use is made of the *quarter-wavelength monopole*.

Monopoles and Dipoles

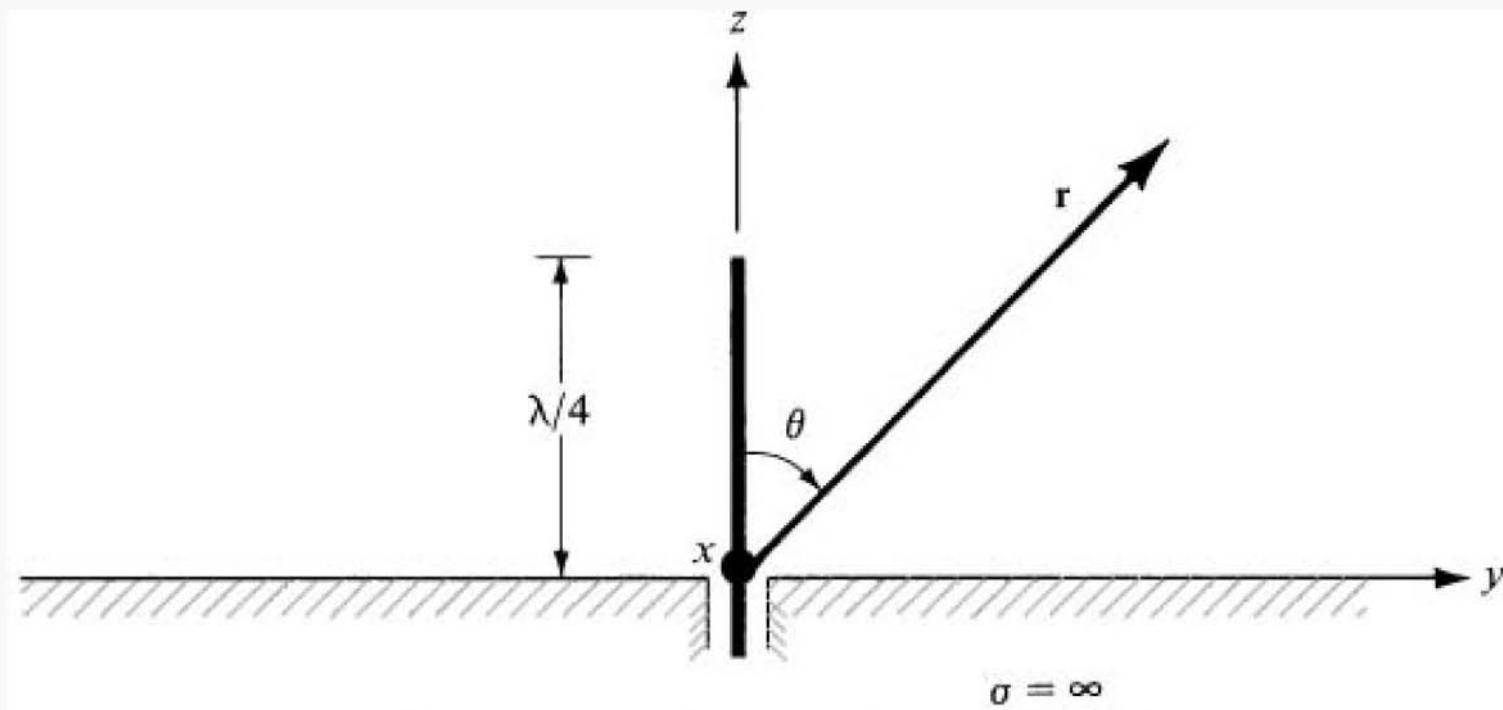


Fig. 4.19(a)

Equivalent of a $\lambda/4$ Monopole on a PEC

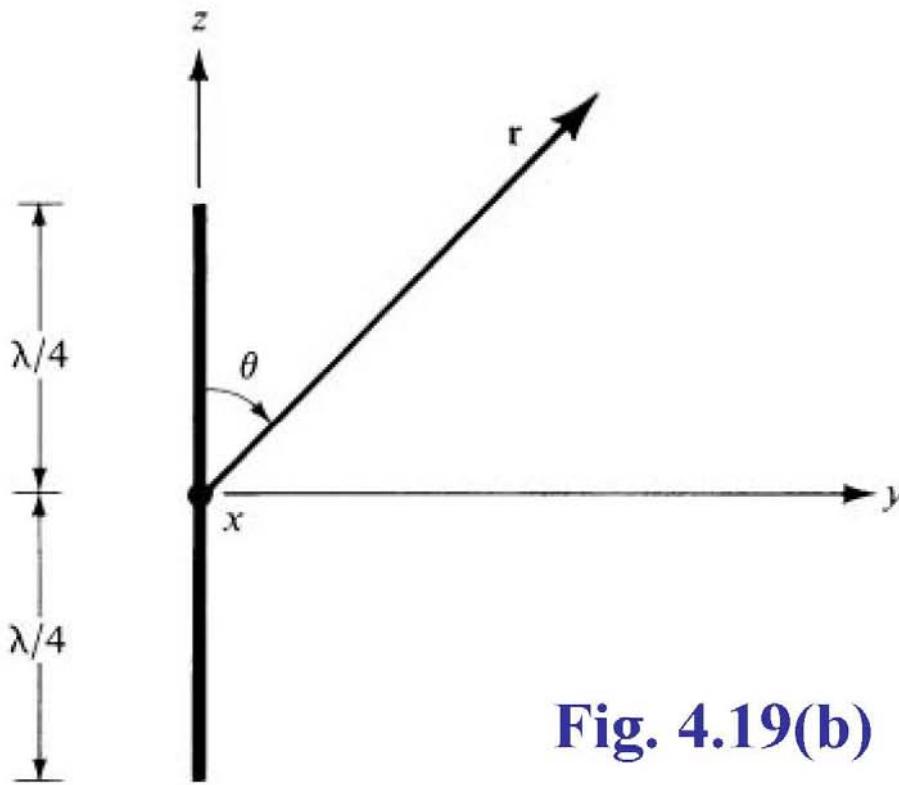


Fig. 4.19(b)

Half-Wavelength Dipole ($l = \lambda/2$)

$$E_\theta \simeq j\eta \frac{I_0 e^{-jkr}}{2\pi r} \left[\frac{\cos\left(\frac{\pi}{2}\cos\theta\right)}{\sin\theta} \right] \quad (4-84)$$

$$H_\phi \simeq j \frac{I_0 e^{-jkr}}{2\pi r} \left[\frac{\cos\left(\frac{\pi}{2}\cos\theta\right)}{\sin\theta} \right] = \frac{E_\theta}{\eta} \quad (4-85)$$

Directivity?

- Dipole in free space, and a monopole of half the length above a perfect ground plane will have the same radiation intensity in the top-half plane (since fields are identical).
- If the dipole emits power P , then the monopole emits power $P/2$, since the fields are zero in bottom hemisphere.
- Thus, $D_d = \frac{4\pi U_m}{P}$, whereas for the monopole,
$$D_m = \frac{4\pi U_m}{\frac{P}{2}} = 2D_d$$

Radiation resistance?

- If the dipole emits power P , then the monopole emits power $P/2$, since the fields are zero in bottom hemisphere.
- Thus, $R_{rd} = 2P/I_0^2$, whereas for the monopole, $R_{rm} = 2(\frac{P}{2})/I_0^2 = R_{rd}/2$

Monopoles and Dipoles

$$Z_{in} \text{ (monopole)} = \frac{1}{2} Z_{in} \text{ (dipole)} \quad (4-106)$$

$$D_0 \text{ (monopole)} = 2D_0 \text{ (dipole)}$$

Use Of Linear Monopole

Linear monopoles, especially $\lambda/4$, are used as transmitting/receiving elements for wireless mobile/cellular telephones.

Examples:

- A. Civilian Band (CB) Radio
- B. Cellular Telephone
- C. Rooftop Automobile Antenna
- D. Amateur Radio Antenna

Examples of Antennas on Cellular and Cordless Telephones, Walkie-Talkies, and CB Radios



Fig. 4.22

Copyright©2005 by Constantine A. Balanis
All rights reserved

Chapter 4
Linear Wire Antennas

Triangular Array Of Linear Dipoles For Wireless Mobile Communication Base Stations

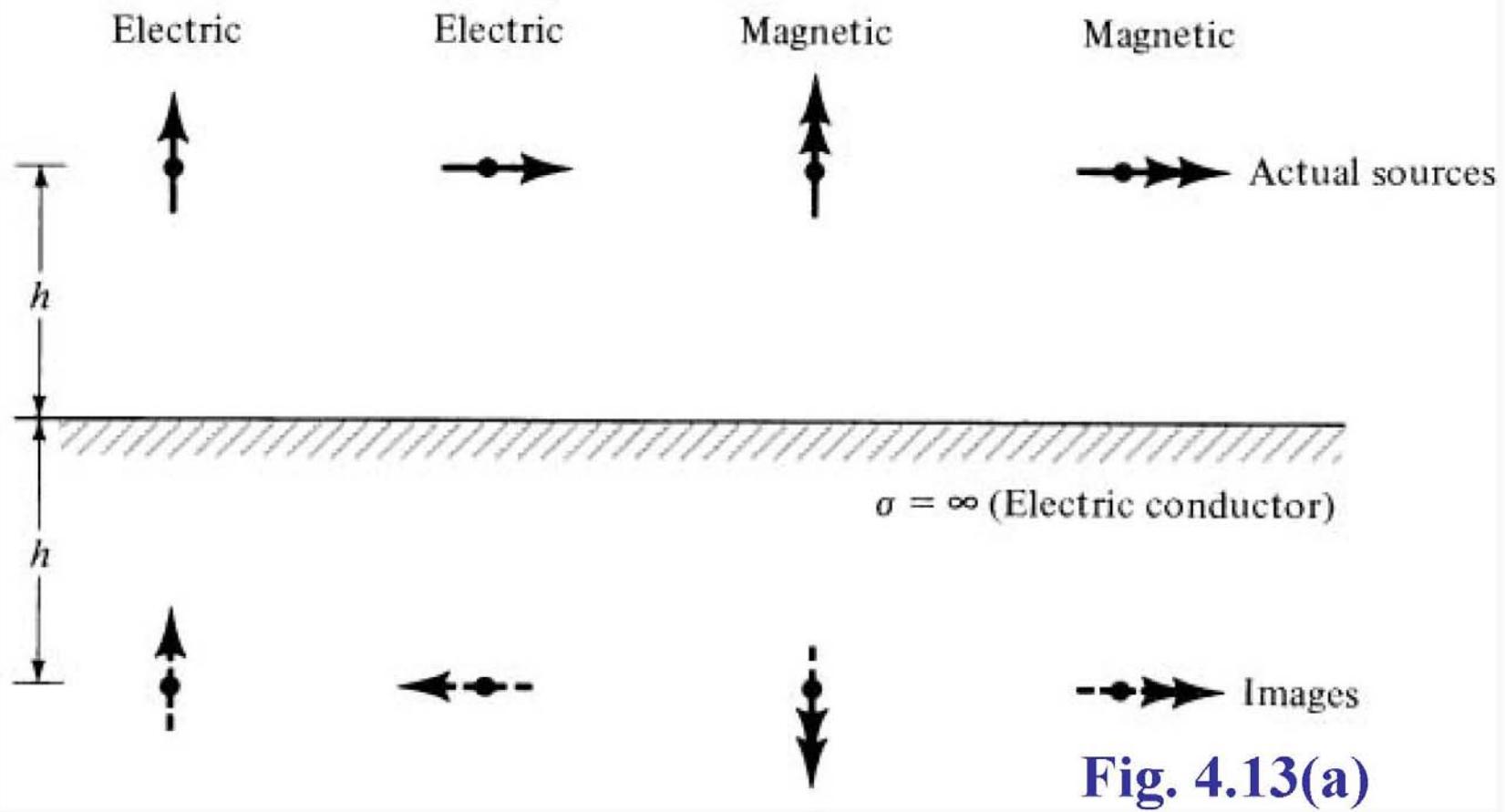


Fig. 4.23

Copyright©2005 by Constantine A. Balanis
All rights reserved

Chapter 4
Linear Wire Antennas

Electric Conductor



Horizontal Electric Dipole Above an Infinite Perfect Electric Conductor

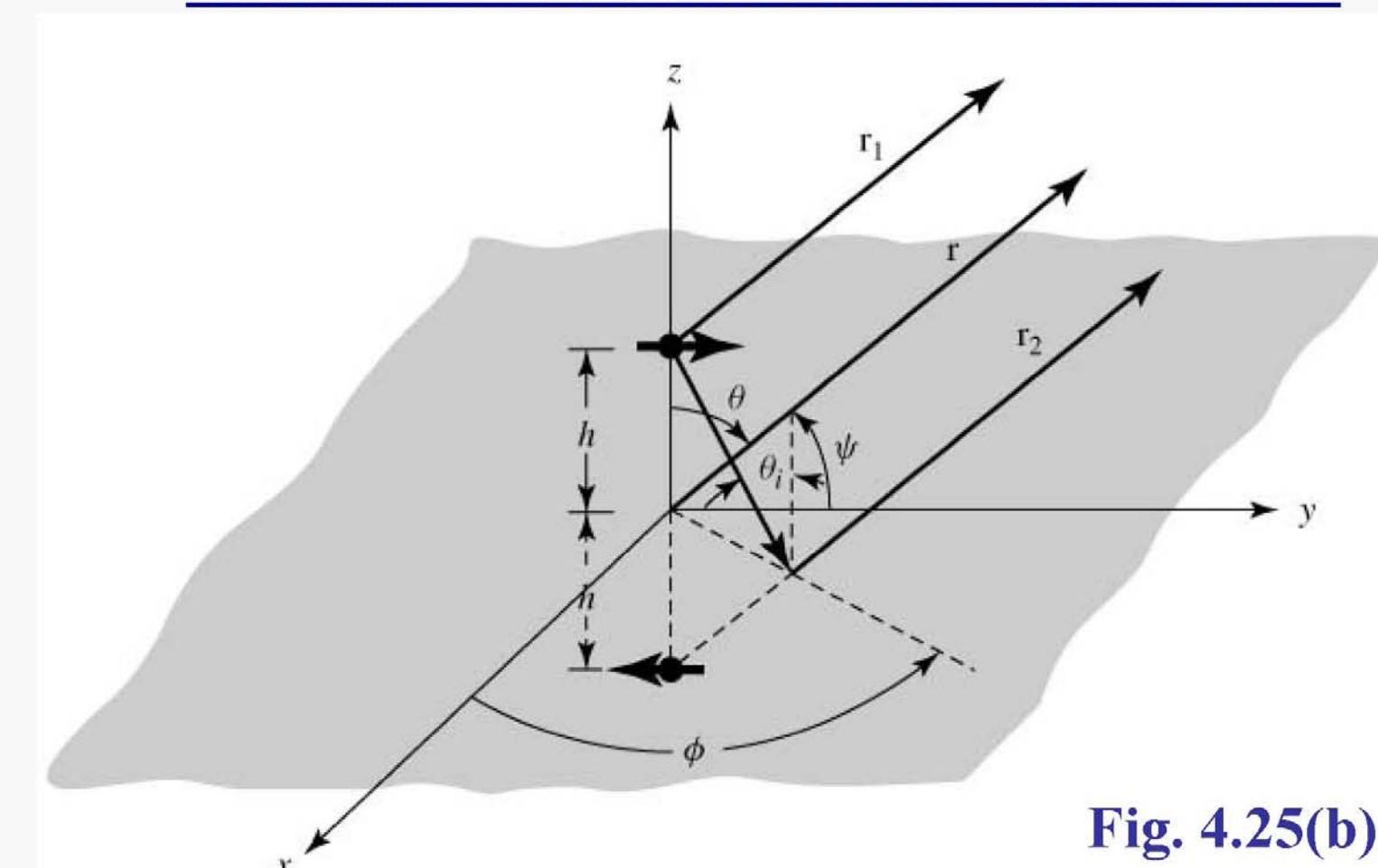


Fig. 4.25(b)

Copyright©2005 by Constantine A. Balanis
All rights reserved

Chapter 4
Linear Wire Antennas

$$E_{\psi}^d = j\eta \frac{kI_o \ell e^{-jkr_1}}{4\pi r_1} \sin \psi \quad (4-111)$$

$$E_{\psi}^r = jR_h \eta \frac{kI_o \ell e^{-jkr_2}}{4\pi r_2} \sin \psi \quad (4-112)$$

$$= -j\eta \frac{kI_o \ell e^{-jkr_2}}{4\pi r_2} \sin \psi \quad (4-112a)$$

Elevation Plane ($\phi = 90^\circ$) Amplitude Patterns

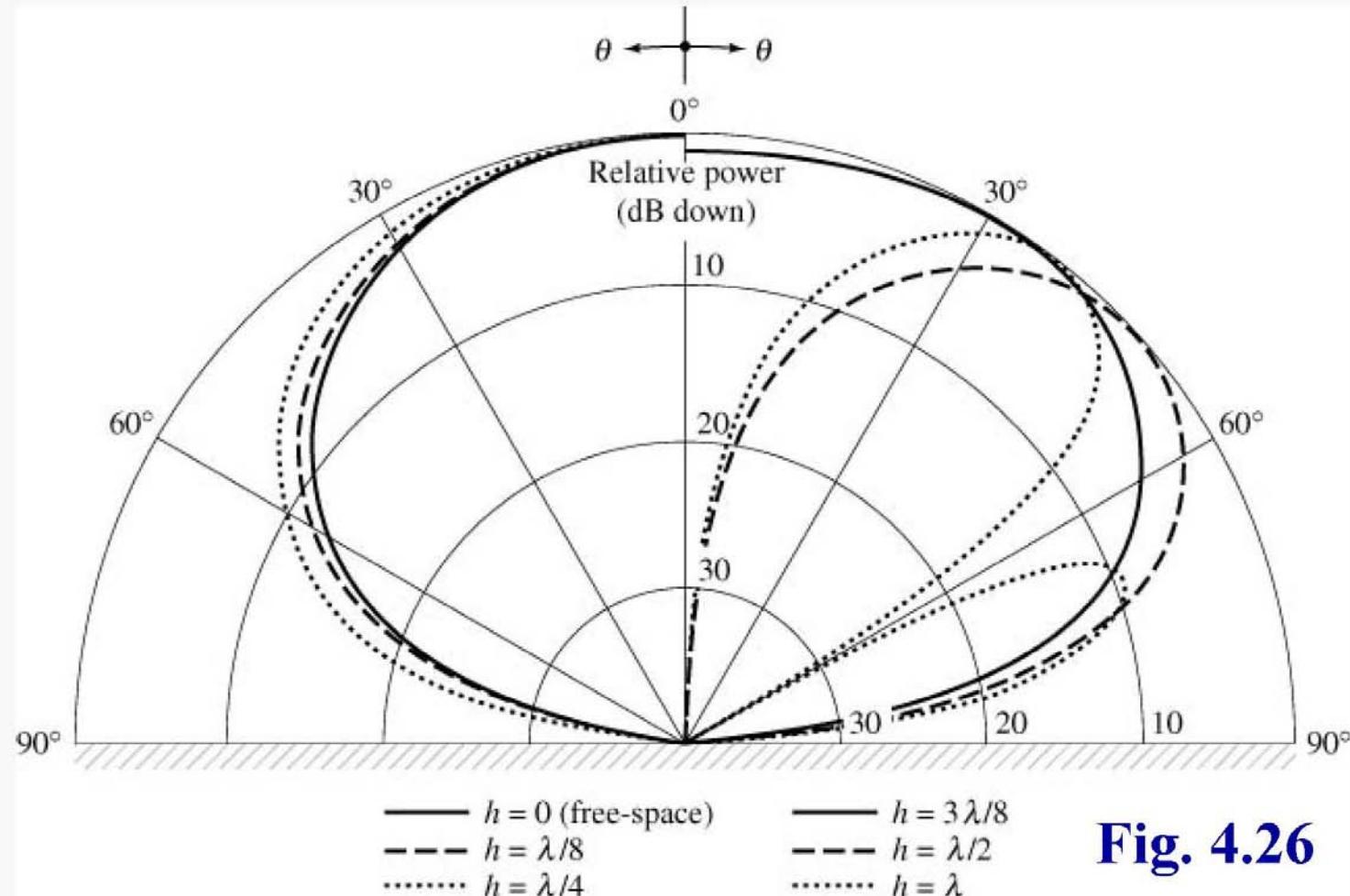


Fig. 4.26

3-D Amplitude Pattern of a Horizontal Dipole

$$h = \lambda$$

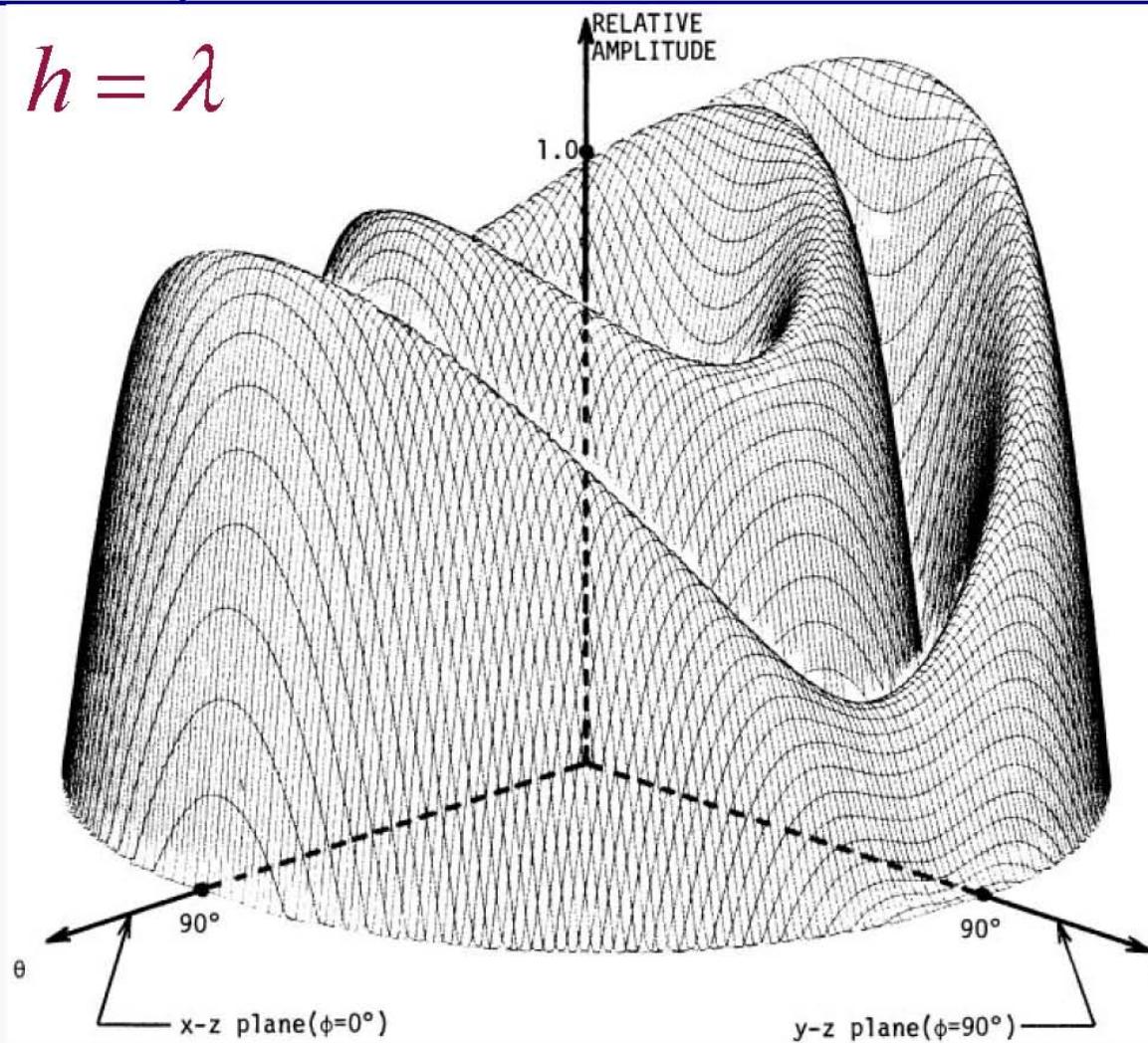
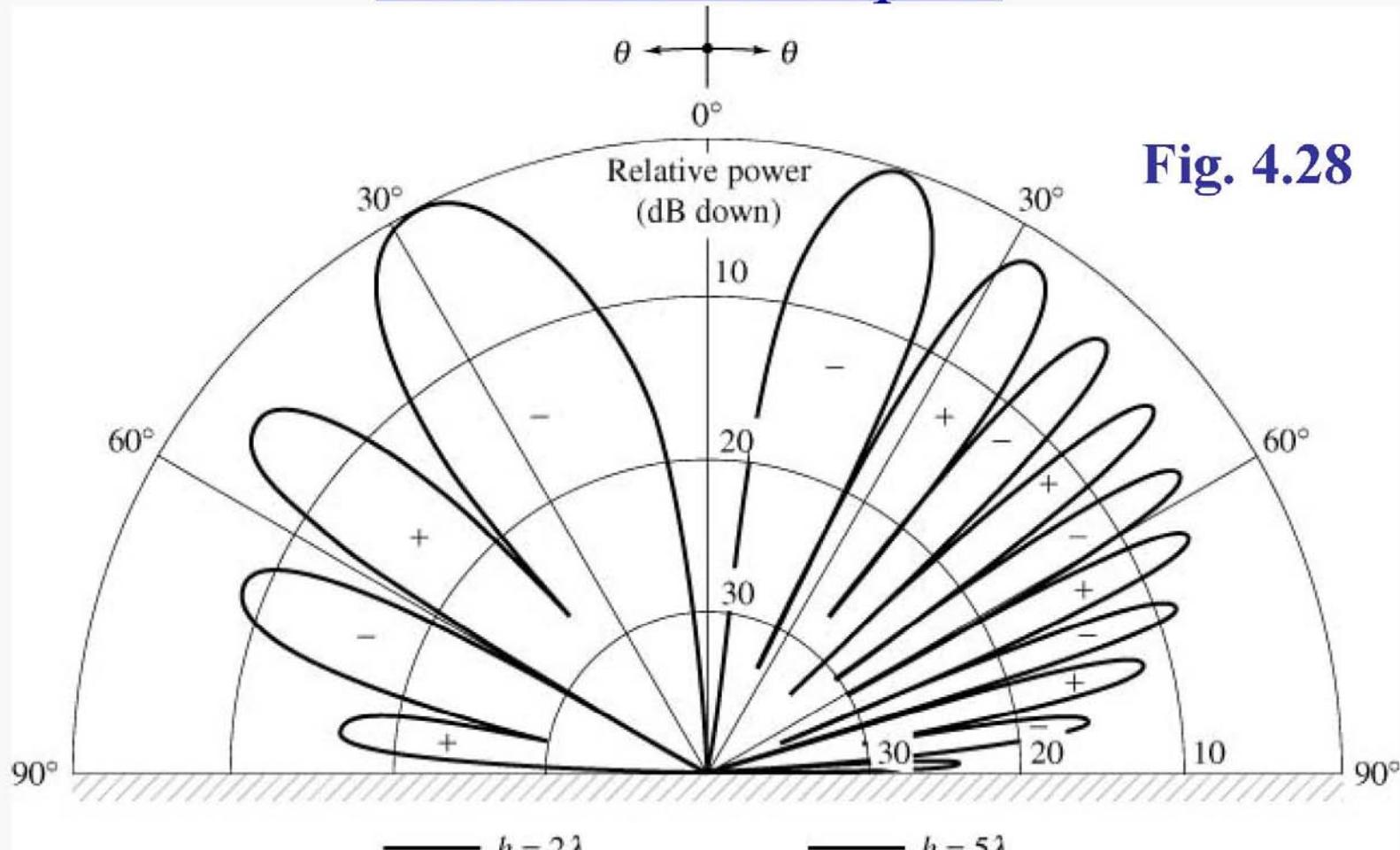


Fig. 4.27

Copyright©2005 by Constantine A. Balanis
All rights reserved

Chapter 4
Linear Wire Antennas

Scalloping of Amplitude Pattern of Horizontal Dipole



Horizontal Dipole

$$\text{Number of Lobes} \simeq 2 \left(\frac{h}{\lambda} \right)$$

(4-117)

$$h \gg \lambda$$

Loss-y Earth

- For lower frequencies, (<3 MHz), PEC is not a good approximation.
- As engineering design, to improve radiation efficiency often metal plates are placed below antennas to simulate PEC planes.

Constitutive Parameters of Ground

$$\epsilon_0, \mu_0, \sigma = 0$$



$$\epsilon_1, \mu_1, \sigma_1$$

Constitutive Parameters of Ground

$$\epsilon_1, \mu_1, \sigma_1$$

or

$$\dot{\epsilon}_1, \mu_1$$

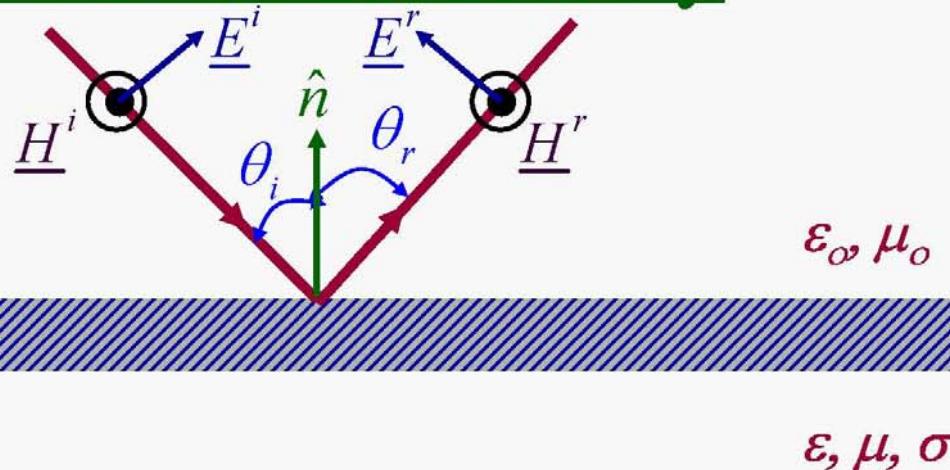
Could also include
magnetic conductivity,
if necessary.

where

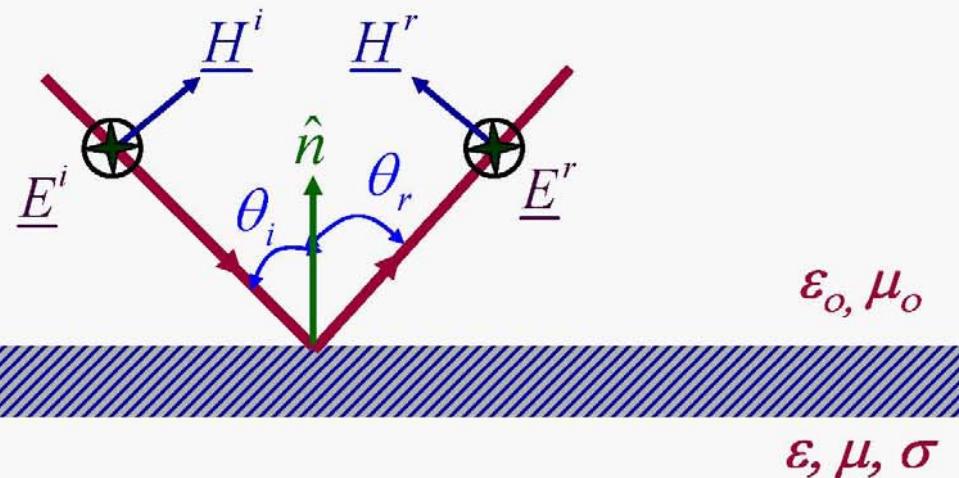
$$\dot{\epsilon}_1 = \epsilon_1' - j\epsilon_1'' = \epsilon_1 - j \frac{\sigma_1}{\omega}$$

Interface Geometry

Vertical
(Parallel)



Horizontal
(Perpendicular)



Vertical Polarization

$$E_\theta = j\eta \frac{kI_o \ell e^{-jkr}}{4\pi r} \sin \theta \left[e^{jkh \cos \theta} + R_v e^{-jkh \cos \theta} \right]$$

$$R_v = \frac{\eta_0 \cos \theta_i - \eta_1 \cos \theta_t}{\eta_0 \cos \theta_i + \eta_1 \cos \theta_t} = -R_{\parallel} \quad (4-125)$$

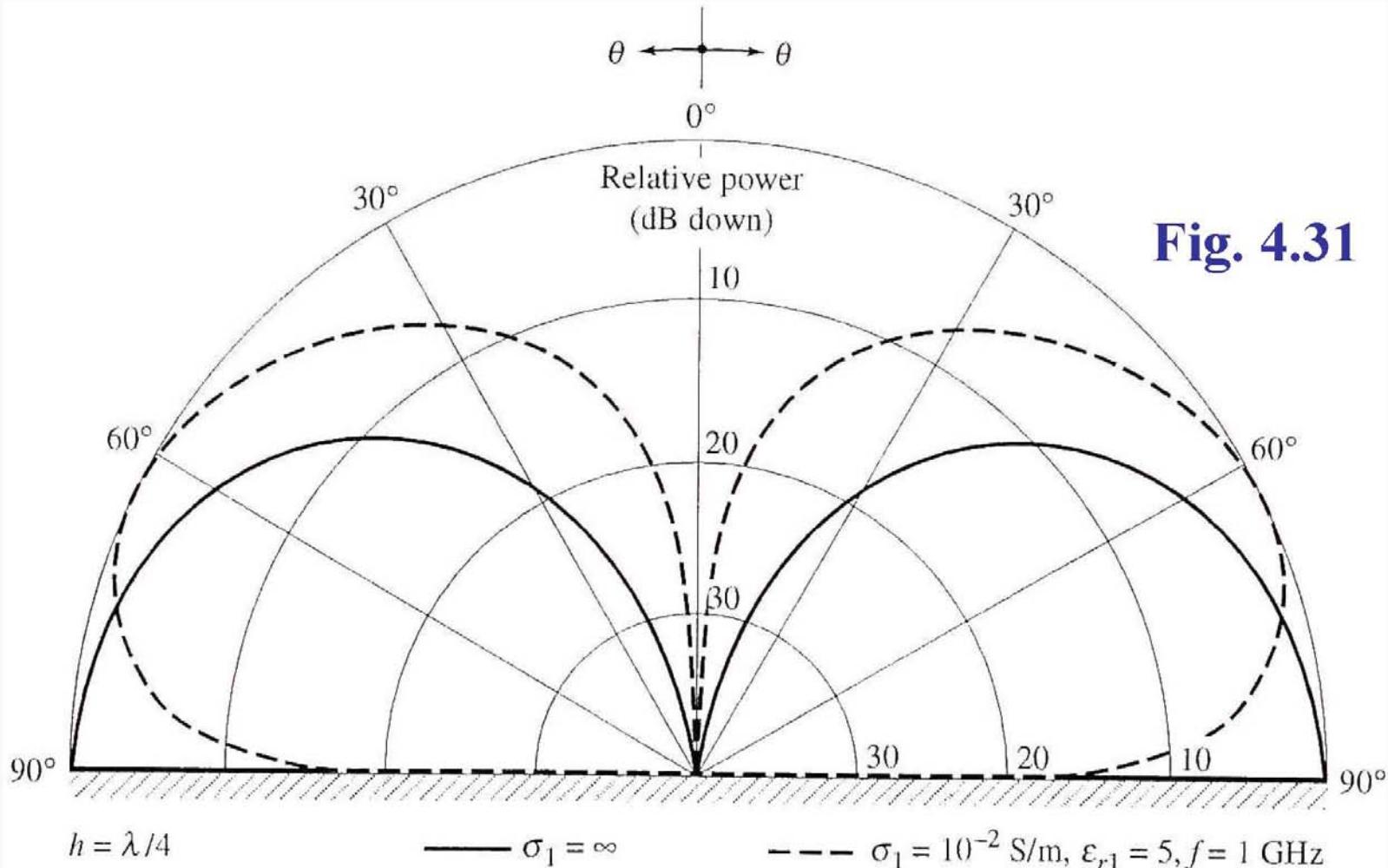
$$\eta_1 = \sqrt{\frac{j\omega\mu_1}{\sigma_1 + j\omega\varepsilon_1}}, \quad \eta_0 = \sqrt{\frac{\mu_o}{\varepsilon_o}}$$

$$\gamma_0 \sin \theta_i = \gamma_1 \sin \theta_t \quad (4-126)$$

$$\gamma_0 = j\beta_0$$

$$\gamma_1 = \sqrt{j\omega\mu_1(\sigma_1 + j\omega\varepsilon_1)} = \alpha_1 + j\beta_1$$

Vertical Polarization



Copyright©2005 by Constantine A. Balanis
All rights reserved

Chapter 4
Linear Wire Antennas

Horizontal Polarization

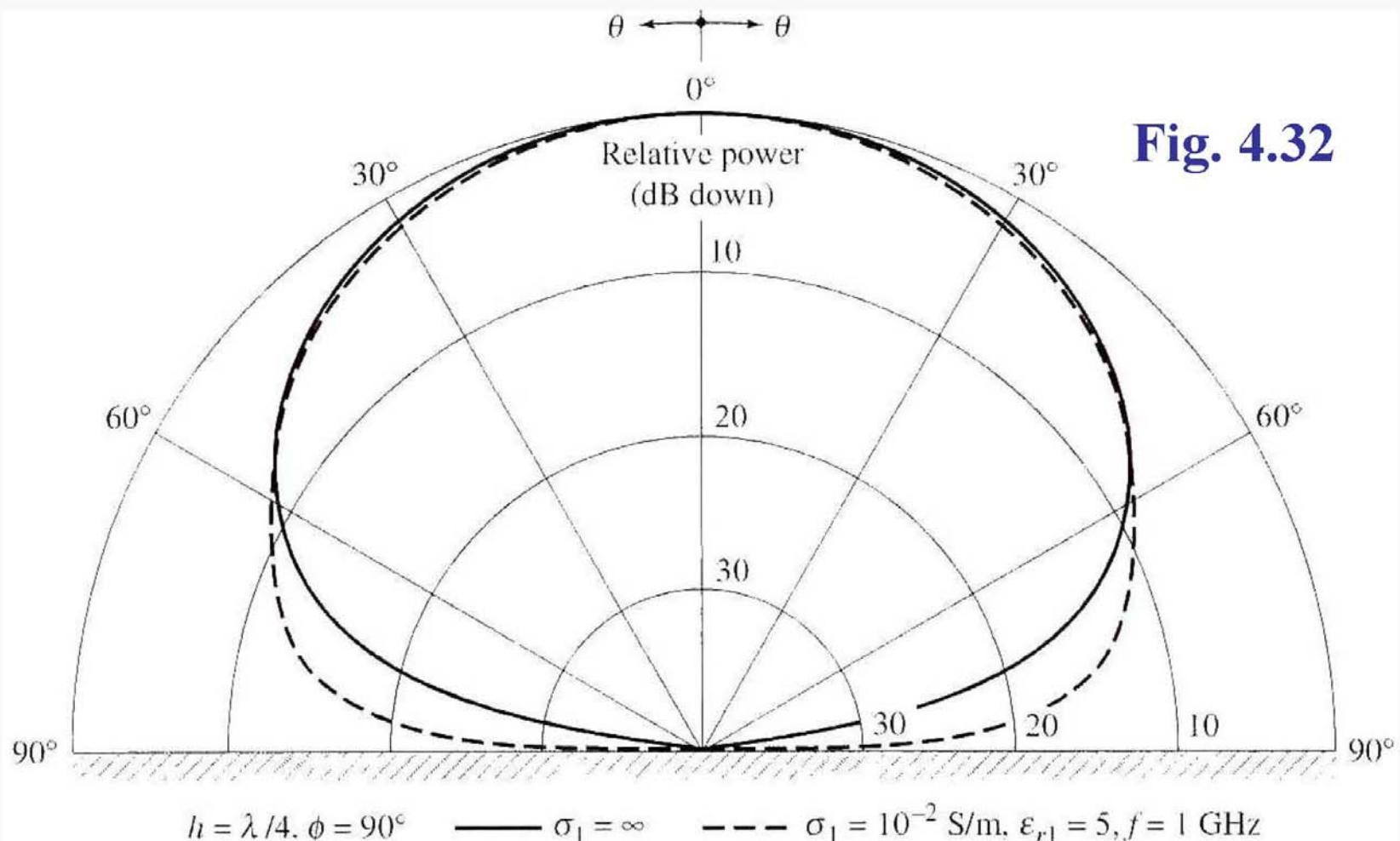


Fig. 4.32