

*Spur Reduction in Wideband PLLs by Random
Positioning of Chargepump Current Pulses*
2010 International Symposium on Circuits and Systems, Paris

Chembiyan Thambidurai
Nagendra Krishnapura

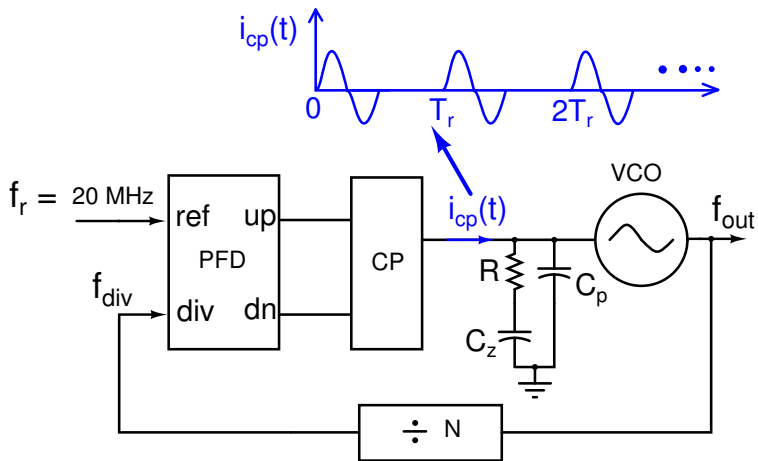
Department of Electrical Engineering
Indian Institute of Technology, Madras
Chennai, 600036, India

2 June 2010

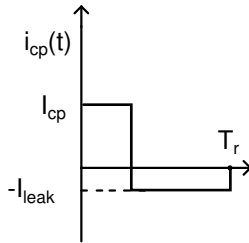
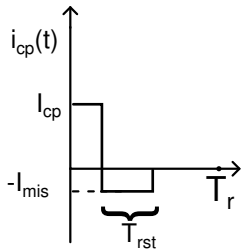
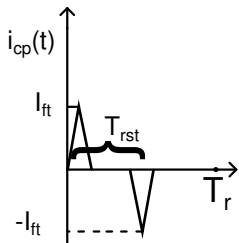
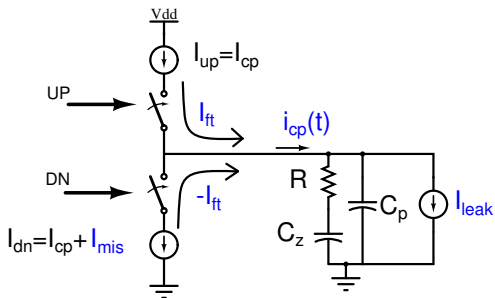
Outline

- Reference spur in chargepump PLLs
- Randomization of chargepump current pulses
- Implementation details
- Spectrum after randomization
- Effect of non-idealities
- Simulation results
- Conclusions

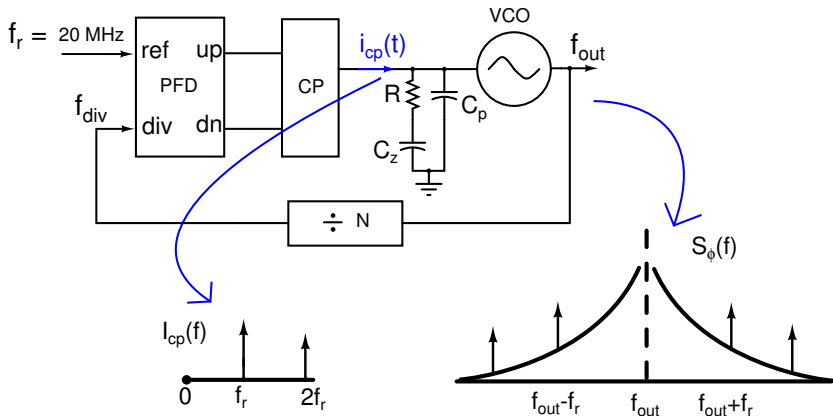
Reference spurs



Chargepump non-idealities



Reference spurs



Spur vs bandwidth tradeoff

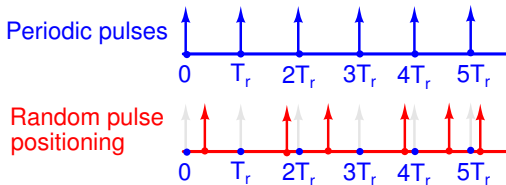
- The magnitude of the spur at a frequency offset f_r (dBc)

$$S_{\phi}(f_r) = 20 \log \left(\frac{I_{cp}(f_r) |Z_{lp}(f_r)| K_{vco}}{2f_r} \right)$$

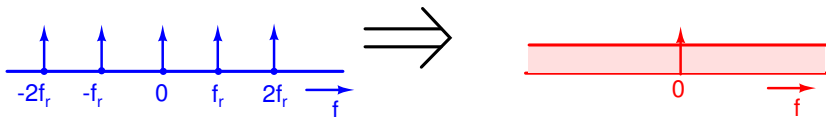
- Low spur level \Rightarrow low bandwidth (large settling time)
(Loop filter with one pole and one zero assumed here)

Random pulse position modulation

Time Domain

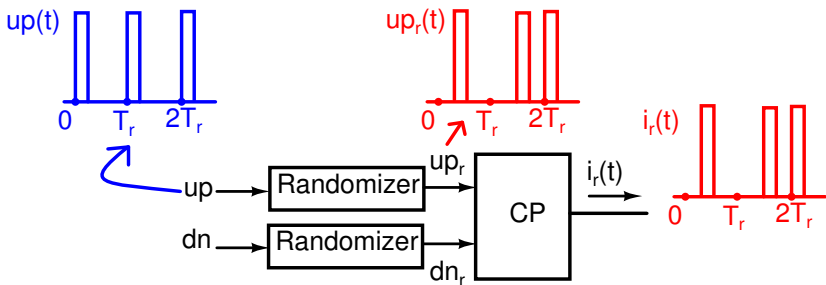


Frequency Domain



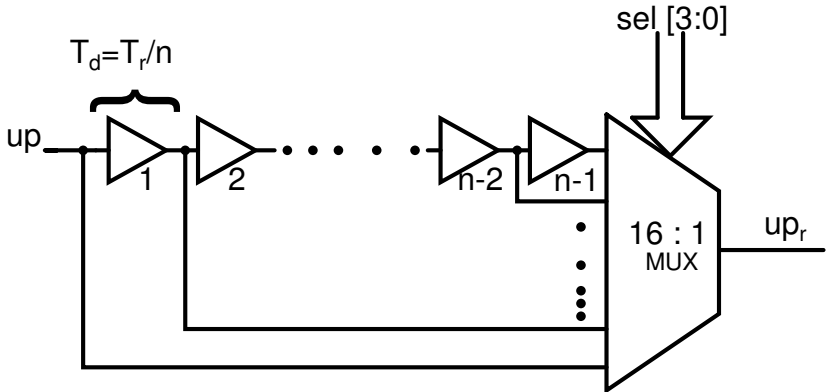
- Redistribute the spur energy to all frequencies.

Implementation



- Chargepump current pulse position has to be randomized.
- Accomplished by randomizing up/dn pulses.

Randomizer

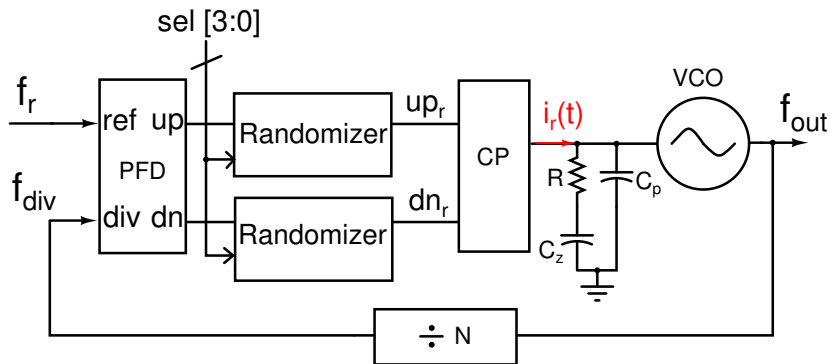


- Randomly choose 1 of n delayed pulses

Random number generator

- The randomizing sequence sel [3 : 0] should have a uniform distribution.
- Generated using PRBS(Pseudo Random Bit Sequence) generator.
- A PRBS of longer length
 - produces low in-band noise.
 - guarantees near uniform distribution.
- Length of PRBS chosen based on tolerable in-band noise.

PLL with random pulse positioning



- Control voltage not periodic

Mathematical analysis

- The periodic impulse train

$$x(t) = \sum_{k=-\infty}^{\infty} \delta(t - kT_r)$$

- The randomized impulse train

$$r(t) = \sum_{k=-\infty}^{\infty} \delta(t - kT_r - \frac{a_k T_r}{n})$$

(n : Number of possible pulse positions in a period)

Spectrum before and after randomization

- Power spectrum of a periodic impulse train

$$S_x(f) = \frac{1}{T_r^2} \sum_{k=-\infty}^{\infty} \delta\left(f - \frac{k}{T_r}\right)$$

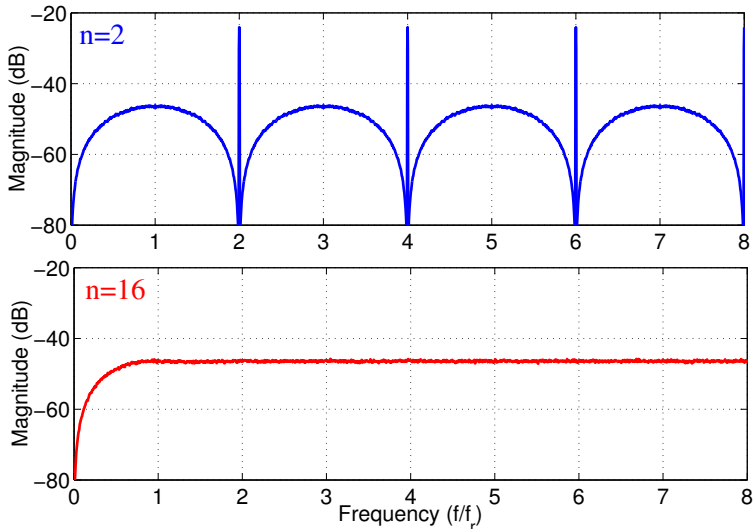
- Power spectrum of the randomized signal

$$S_r(f) = S_{rd}(f) + \frac{1}{T_r^2} \sum_{k=-\infty}^{\infty} \delta\left(f - k\frac{n}{T_r}\right)$$

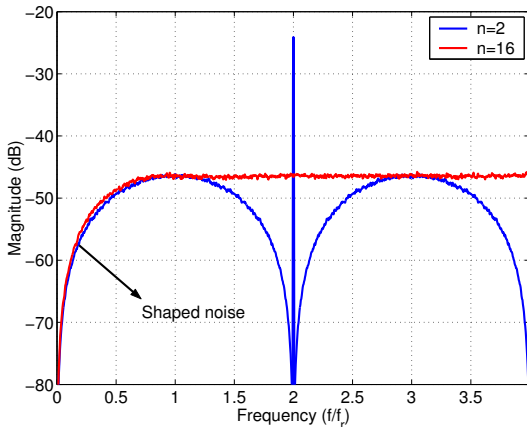
- $S_{rd}(f)$ is the “redistributed noise”

$$S_{rd}(f) = \frac{1}{nT_r} \left[(n-1) - \frac{2}{n} \sum_{k=1}^{n-1} (n-k) \cos\left(\frac{2\pi kfT_r}{n}\right) \right]$$

Simulated spectrum after randomization



Noise shaping in the redistributed noise



- The 'redistributed noise' is not white.
- For $n=2$ we can see that

$$S_{rd}(f) = \frac{1}{T_r} \sin^2\left(\frac{\pi f T_r}{2}\right)$$

- Close-in phase noise remains unaffected.

Delay sensitivity

- Delays prone to process variations ($T_d \neq T_r/n$).
- Delay line may span more or less than a reference period
- The current after randomization ($i_r(t)$) on an average can be expressed as

$$i_r(t) = \frac{1}{n} [i_{cp}(t) + i_{cp}(t - T_d) + \dots + i_{cp}(t - (n - 1)T_d)]$$

$$|I_r(f)| = \frac{\sin(n\pi f T_d)}{\sin(\pi f T_d)} |I_{cp}(f)|$$

Delay sensitivity

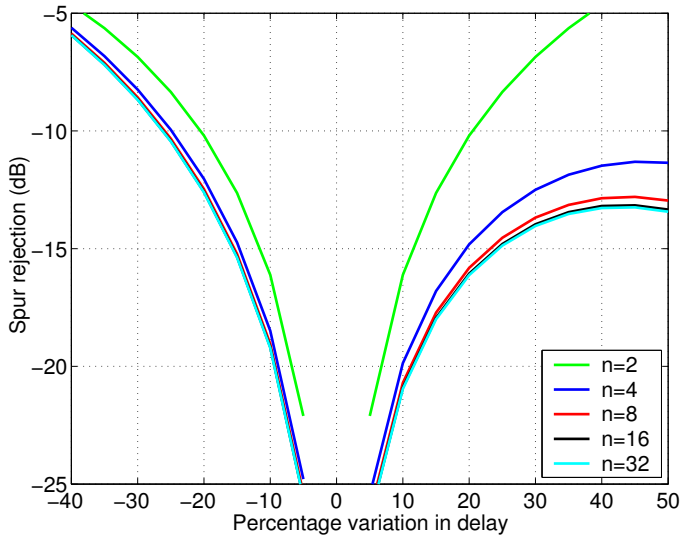
- Thus the randomization behaves as a moving average filter with frequency nulls at

$$f_z = \frac{k}{nT_d}$$

$$k \in [1, (n - 1)]$$

- If $T_d = \frac{T_r}{n}$; nulls occur at reference harmonics.
- If $T_d \neq \frac{T_r}{n}$; nulls do not occur at reference harmonics and spurs appear at PLL output

Sensitivity to delay variations

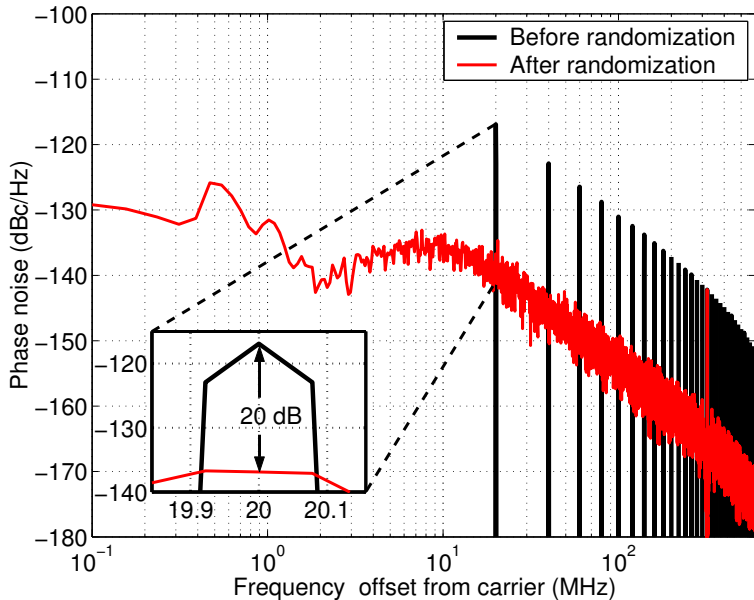


Simulated PLL parameters

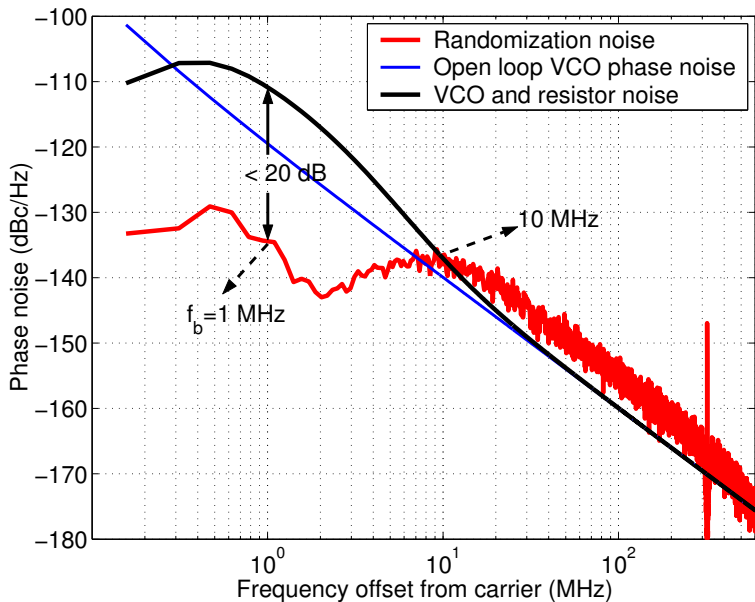
f_{ref}	20 MHz
f_{out}	1 GHz
f_{BW}	1 MHz
<hr/>	
PFD	Tri-state PFD
Charge-pump	$I_{cp} = 50 \mu\text{A}$
Loop-filter	$R = 21.7 \text{ k}\Omega, C_z = 37.25 \text{ pF}, C_p = 1.99 \text{ pF}$
VCO	$f_{vco} = 1 \text{ GHz}, K_{vco} = 200 \text{ MHz/V}$
Divider	$N=50$

- 3-dB bandwidth of the PLL is $\approx 1 \text{ MHz}$.
- Charge pump current mismatch 10 %
- Charge pump and PFD: transistor level
- Other components: ideal

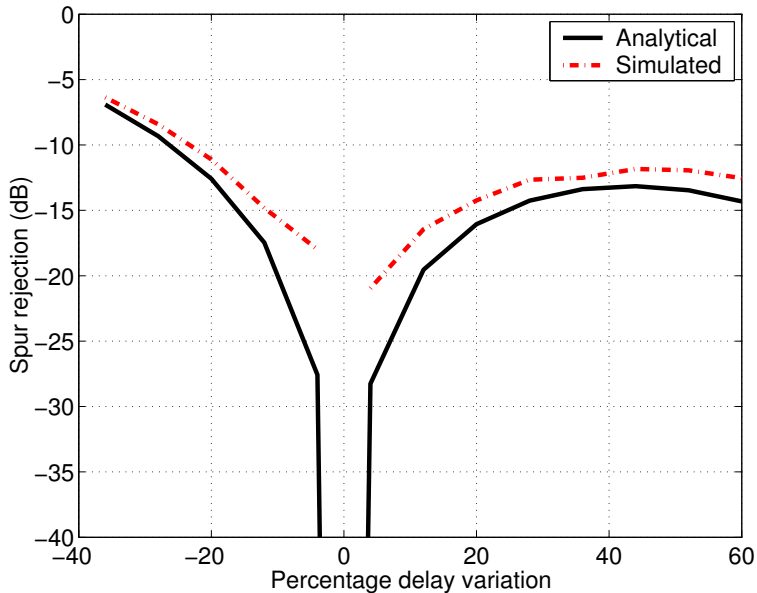
Simulation results



Effect of randomization at high frequencies



Simulated sensitivity to delay variations



Conclusions

- Pulse position randomization eliminates reference spur.
- Resulting spectrum shaped to high frequencies.
- Close-in phase noise remains unaffected.
- > 11.5 dB spur rejection for $\pm 20\%$ delay variation.
- Simple implementation.

References



Cicero.S.Vaucher, "An adaptive PLL tuning system architecture combining high spectral purity and fast settling time." *IEEE Journal of Solid State Circuits*, pp. 2131-2137, vol. 35, issue 4, April. 2000.



Che-Fu Liang et al., "Spur suppression techniques for frequency synthesizers," *IEEE Transactions on Circuits and Systems-II:Express Briefs*, pp. 653-657, vol. 54, issue 8, Aug. 2007.



Che-Fu Liang et al., "A digital calibration technique for charge pumps in phase-locked systems," *IEEE Journal of Solid State Circuits*, pp. 390-398, vol. 38, issue 2, Feb. 2008.



T. C. Lee, W. L. Lee, "A spur suppression technique for phase Locked frequency synthesizers.," *International Solid State Circuits Conference*, ISSCC 2006, pp.592-593.

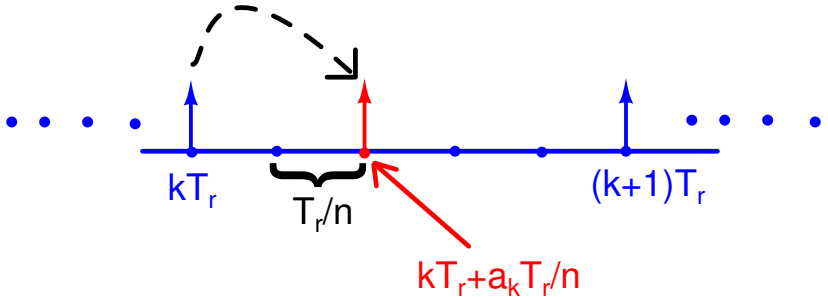


Cameron T. Charles, David J Allstot, "A Calibrated Phase/Frequency Detector for Reference Spur Reduction in Charge-Pump PLLs," *IEEE Transactions on Circuits and Systems-II:Express Briefs*, vol. 53, issue 9, Sep. 2006.



B. P. Lathi, *Modern Digital and Analog Communication Systems.*, Third edition, New York:Oxford University Press., 1998.

Mathematical representation



- The reference period (T_r) is divided into equal time intervals of T_r/n .
- The k^{th} current pulse will appear at $kT_r + a_k T_r/n$ instead of kT_r .
- a_k is a uniform random integer $\in [0, n - 1]$

Random pulse positioning illustrated for $n=4$

