

EE539: Analog Integrated Circuit Design;

Nagendra Krishnapura (nagendra@iitm.ac.in)

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1 FREQUENCY RESPONSE OF TWO STAGE OPAMP

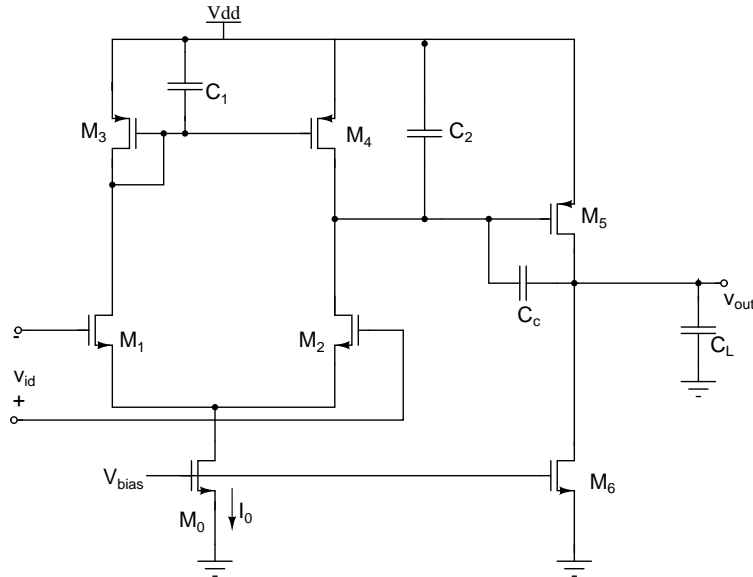


Figure 1: Two stage opamp

$$A_{dc} = \frac{g_{m1}}{g_{ds1} + g_{ds3}} \cdot \frac{g_{m5}}{g_{ds5} + g_{ds6} + G_L} = \frac{g_{m1}}{G_1} \cdot \frac{g_{m5}}{G_L}$$

$$P_1 = -\frac{G_1}{C_2 + (1 + \frac{g_{m5}}{G_L})C_c}$$

$$P_2 = -\frac{g_{m5} \cdot \frac{C_c}{C_c + C_2}}{C_L + \frac{C_c \cdot C_2}{C_c + C_2}} \approx \frac{g_{m5}}{C_L}$$

$$Z_1 = \frac{g_{m5}}{C_c}$$

$$Z_2 = -\frac{2g_{m3}}{C_1}$$

$$P_3 = -\frac{gm_3}{C_1}$$

$$w_u = -\frac{gm_1}{C_c}$$

1.1 DESIGN OF TWO STAGE OPAMP

Given G_L, A_{dc}, C_L, w_u

- Choose $gm_5, I_5, C_c : \frac{gm_5}{C_L} > w_u$
 - Choose gm_1 : small I_0 and, large W_1 but considering phase margin(PM) requirements.
- Due to this Z_2, P_3 moves to lower frequencies.
- To improve phase margin(PM), introduce compensation resistor R_c as shown in fig(1).

Now

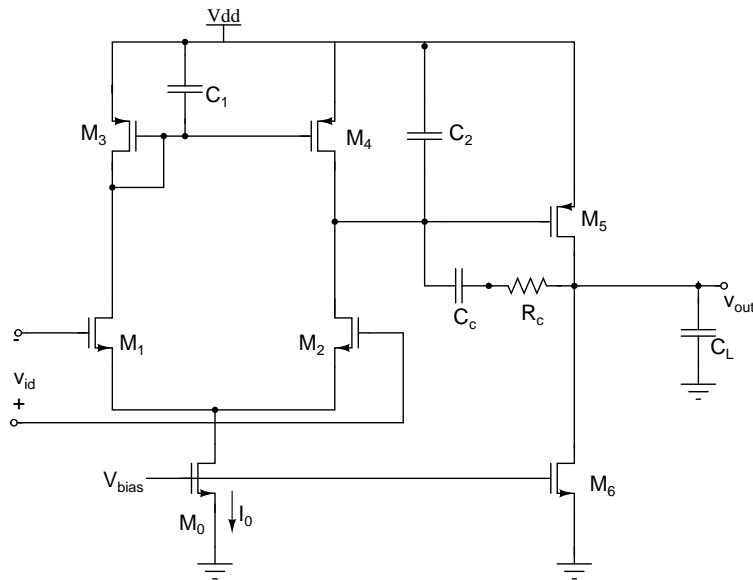


Figure 2: Two stage opamp

$$Z'_1 = \frac{gm_5}{C_c(1 - gm_5 R_c)} = -\frac{1}{C_c(\frac{1}{gm_5} - R_c)}$$

- If $R_c = \frac{1}{gm_5}$, then Z'_1 moves to ∞ , and improves PM.
 - If $R_c > \frac{1}{gm_5}$, further improvement in PM, since zero moves left half plane and cancels left half plane pole.
- But the problem here is R_c must be able to track gm_5

2 SLEW RATE OF TWO STAGE OPAMP

2.1 Positive slew rate

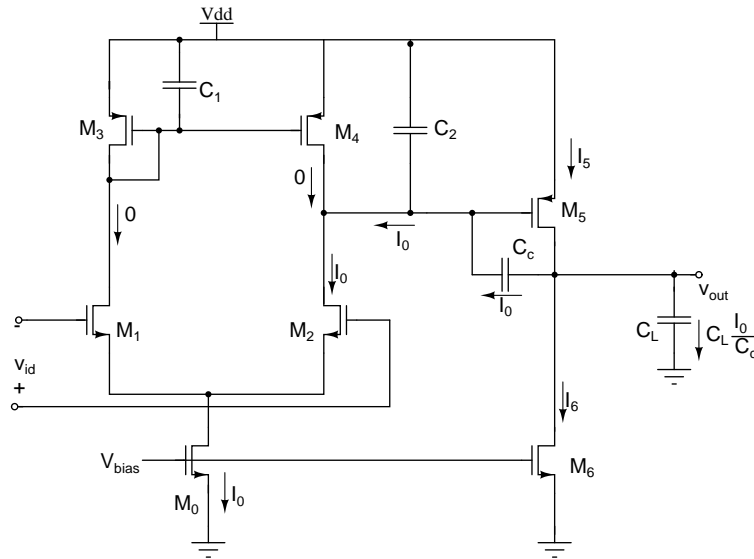


Figure 3: Two stage opamp

If we apply large positive voltage at input as shown in figure(3),then

$$SR_+ = \frac{I_0}{C_c}$$

This is correct if we assume that gate of M_5 can go low enough to support a current $I_0(1 + C_L C_c) + I_6$

2.2 Negative slew rate

If we apply large negative voltage at input as shown in figure(4),then

•

$$SR_- = \frac{I_0}{C_c}$$

This is correct if we assume that $I_5 > I_0(1 + C_L C_c)$

•

$$SR_- = \frac{I_0}{C_c + C_L}$$

This is correct if we assume that $I_5 < I_0(1 + C_L C_c)$

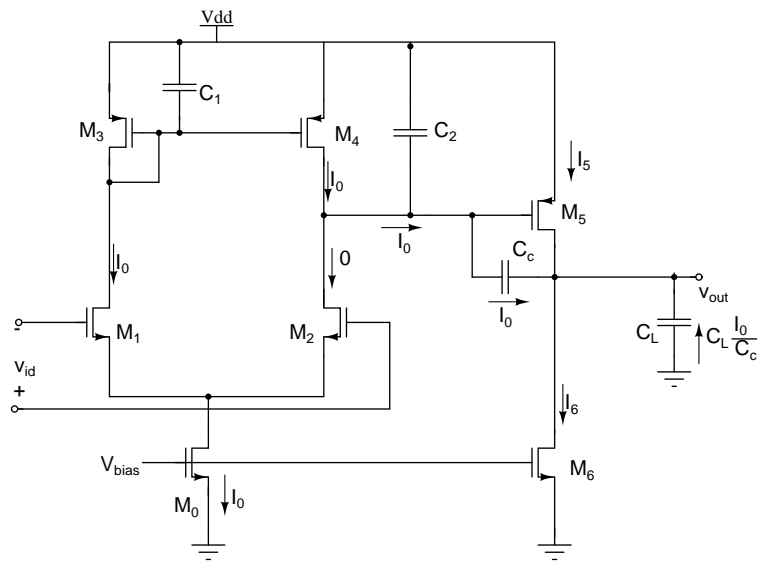


Figure 4: Two stage opamp