## DIFFERENTIAL AMPLIFIERS USING TRANSISTOR LOADS.

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## DIFFERENTIAL AMPLIFIER USING NMOS LOAD.

The advantage over resistive load is that gain is a ratio of like components, so the variations are less.

• The gain is  $\frac{g_{m1}}{g_{m3}+g_{mbs3}}$ .

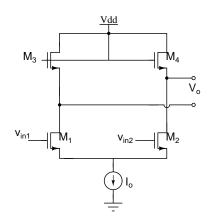


Figure 1: DIFFERENTIAL AMPLIFIER USING NMOS TRANSISTOR LOAD.

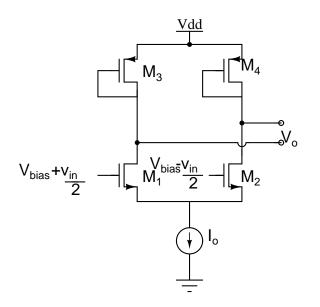


Figure 2: DIFFERENTIAL AMPLIFIER USING PMOS TRANSISTOR LOAD.

 $\checkmark$  To avoid the body effect we can use PMOS transistors. The gain is then  $\frac{g_{m1}}{g_{m3}}$ 

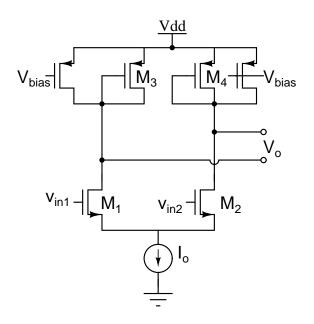


Figure 3: DIFFERENTIAL AMPLIFIER USING PMOS TRANSISTOR AND A PMOS CURRENT SOURCE AS LOAD.

• We can increase gain by reducing  $g_{m3}$ . This can be done by reducing the current through  $M_3$ , so we connect a current source in parallel.

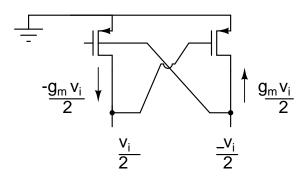


Figure 4: NEGATIVE RESISTANCE

 Another option to increase gain is by connecting negative resistance in parallel across the load.

Negative small signal resistance =  $\frac{-2}{g_m}$ 

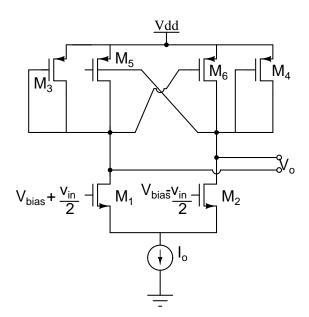


Figure 5: DIFFERENTIAL AMPLIFIER WITH NEGATIVE RESISTANCE IN PARALLEL AS LOAD

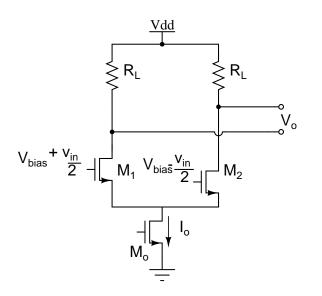


Figure 6: DIFFERENTIAL AMPLIFIER WITH RESISTANCE AS LOAD

• For a differential amplifier using  $R_L$  as load,

$$V_{bias} > V_T + \sqrt{\frac{2\frac{I_o}{2}}{\mu_n C_{ox} \frac{W}{L}}} + \sqrt{\frac{2I_o}{\mu_n C_{ox} \frac{W}{L}}}$$
(1)

Also,

$$V_{bias} + \frac{v_{in}}{2} - v_{th} < V_{DD} - \frac{I_o R_L}{2} - \frac{g_m v_{in} R_L}{2}$$
(2)

$$V_{bias} < V_{DD} - \frac{I_o R_L}{2} - (1 + g_m R_L) \frac{v_{in}}{2} + v_{th}$$
 (3)

- $\diamond V_{bias}$  should be such that the transistors  $M_0$  and  $M_1$  are kept in saturation.
- $\diamond$  To maximise signal swing  $V_{bias}$  must be at the lowest possible value.
- $\diamond$  With  $V_{bias}$  at the minimum value

$$V_{DD} > V_{DSAT1} + V_{DSAT0} + \frac{I_o R_L}{2} + (g_m R_L + 1)\frac{v_{in}}{2}$$

For a differential pair using current sources as load the lower constraint is the same but the upper constraint is given by the sum of overdrive of  $M_3$  and  $v_{th}$ .

$$V_{bias} < V_{DD} - \left(\sqrt{\frac{2\frac{I_o}{2}}{\mu_n C_{ox} \frac{W}{L}}} + v_{th3}\right) + v_{th1}$$
(4)