

## Frequency Response of Systems with Rational Transfer Function:

Frequency selective filtering is very important in many practical applications. We can obtain the frequency response by

$$H(e^{j\omega}) = H(z) \Big|_{z=e^{j\omega}}$$

provided the **unit circle is part of the RoC**, i.e.,  $e^{j\omega} \in \text{RoC}$

If  $e^{j\omega} \in \text{RoC}$ , the system is also BIBO stable.

In practice, we will concern ourselves with **causal and stable** systems. In particular, we will restrict ourselves to the class of

LTI systems characterized by LCCDE.

Some important frequency responses are: LPF, HPF, BPF, BSF, differentiator, and Hilbert transformer.

If the system is to be causal, then ideal, brickwall filters **cannot be realized**, since they violate the **Paley-Wiener theorem**.

We will approximate the ideal responses using rational transfer functions, i.e., by systems that are **realizable**.

Consider  $y[n] = - \sum_{k=1}^N a_k y[n-k] + \sum_{l=0}^M b_l x[n-l]$

Taking z-transforms and simplifying,

$$\frac{Y(z)}{X(z)} = H(z) = \frac{\sum_{l=0}^M b_l z^{-l}}{1 + \sum_{k=1}^N a_k z^{-k}} = \frac{B(z)}{A(z)}$$

In product form,

$$H(z) = b_0 \frac{\prod_{l=1}^M (1 - z_l z^{-1})}{\prod_{k=1}^N (1 - p_k z^{-1})} = b_0 z^{\overbrace{N-M}^{N-M}} \frac{\prod_{l=1}^M (z - z_l)}{\prod_{k=1}^N (z - p_k)}$$

*N-M order trivial pole or zero*

Since the system is stable,  $e^{j\omega} \in \text{ROC}$ . Hence,

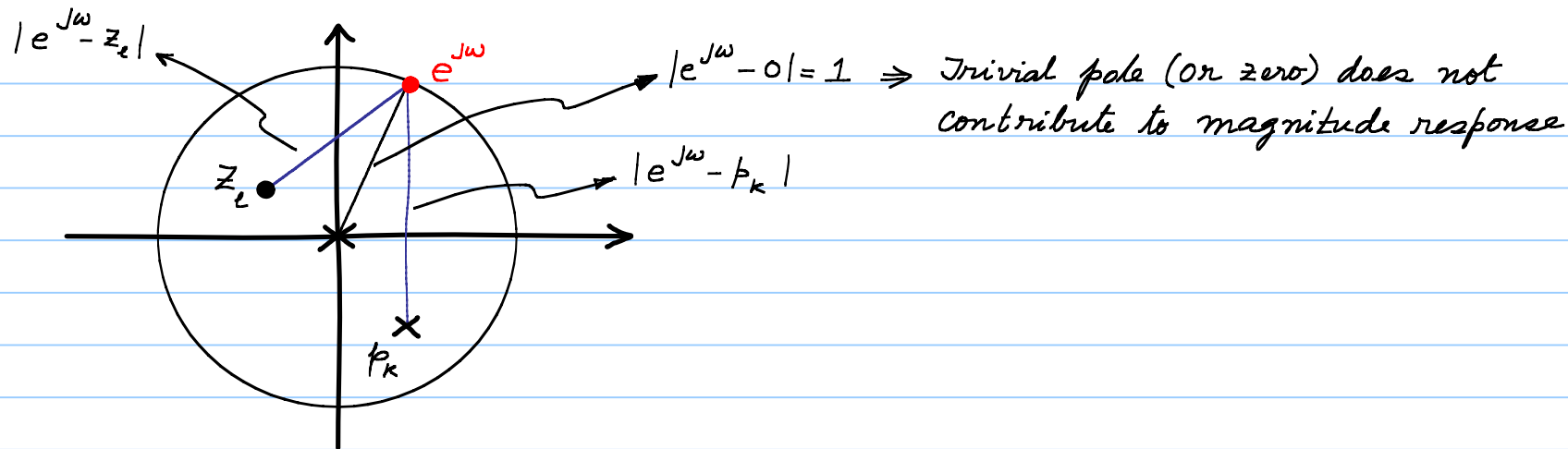
$$H(e^{j\omega}) = b_0 e^{j\omega(N-M)} \frac{\prod_{l=1}^M (e^{j\omega} - z_l)}{\prod_{k=1}^N (e^{j\omega} - p_k)} = \underbrace{|H(e^{j\omega})|}_{\text{magnitude response}} e^{j\angle H(e^{j\omega})} \quad \text{phase response}$$

$$|H(e^{j\omega})| = |b_0| \overbrace{|e^{j\omega(N-M)}|}^1 \frac{\prod_{l=1}^M |e^{j\omega} - z_l|}{\prod_{k=1}^N |e^{j\omega} - p_k|}$$

Because a pole or zero at  $z=0$  does not contribute to the magnitude frequency response, they are called TRIVIAL pole/zero

Trivial poles and zeros contribute to the phase response.

Consider  $|e^{j\omega} - z_e|$ . Geometrically, this denotes the distance from  $e^{j\omega}$  (point on the unit circle) to  $z_e$  (zero at  $z = z_e$ ). Thus, the numerator term is the product of all the distances from  $e^{j\omega}$  to all the zeros. Similarly, the denominator is the product of all the distances from  $e^{j\omega}$  to all the poles. Finally,  $|H(e^{j\omega})|$  is the ratio of these two product of distances, multiplied by the gain term  $|b_0|$ .  $|H(e^{j\omega})|$  changes as ' $\omega$ ' changes.



Because  $|H(e^{j\omega})|$  spans a large range, we plot the magnitude on a **log scale**. In particular, we plot  $20 \log_{10} |H(e^{j\omega})|$  (or, equivalently,  $10 \log_{10} |H(e^{j\omega})|^2$ ). The gain term  $|b_0|$  merely shifts the curve up or down in the log scale.

The same geometric interpretation holds good in the  $s$ -plane also, when interpreting the magnitude of  $H(s) \Big|_{s=j\Omega}$ . For rational  $H(s)$ ,

$$|H(j\Omega)| = |b_0| \frac{\prod_{e=1}^M |j\Omega - z_e|}{\prod_{k=1}^N |j\Omega - p_k|}$$

$|H(j\Omega)|$  is the ratio of the product of all the distances from  $j\Omega$  to all the zeros to product of all the distances from  $j\Omega$  to all the poles, multiplied by  $|b_0|$ .

The above geometric interpretation reveals that there is no point in the  $s$ -plane that is at a constant distance as we move along the  $j\Omega$  axis. Hence there is no concept of trivial pole in the  $s$ -plane (unlike in the  $z$ -plane, where the origin is at a constant distance as we move along the unit circle).