

EE 5140 Digital Modulation & Coding

Prereq: Probability

Contents : Complex baseband Representation

Digital Modulation

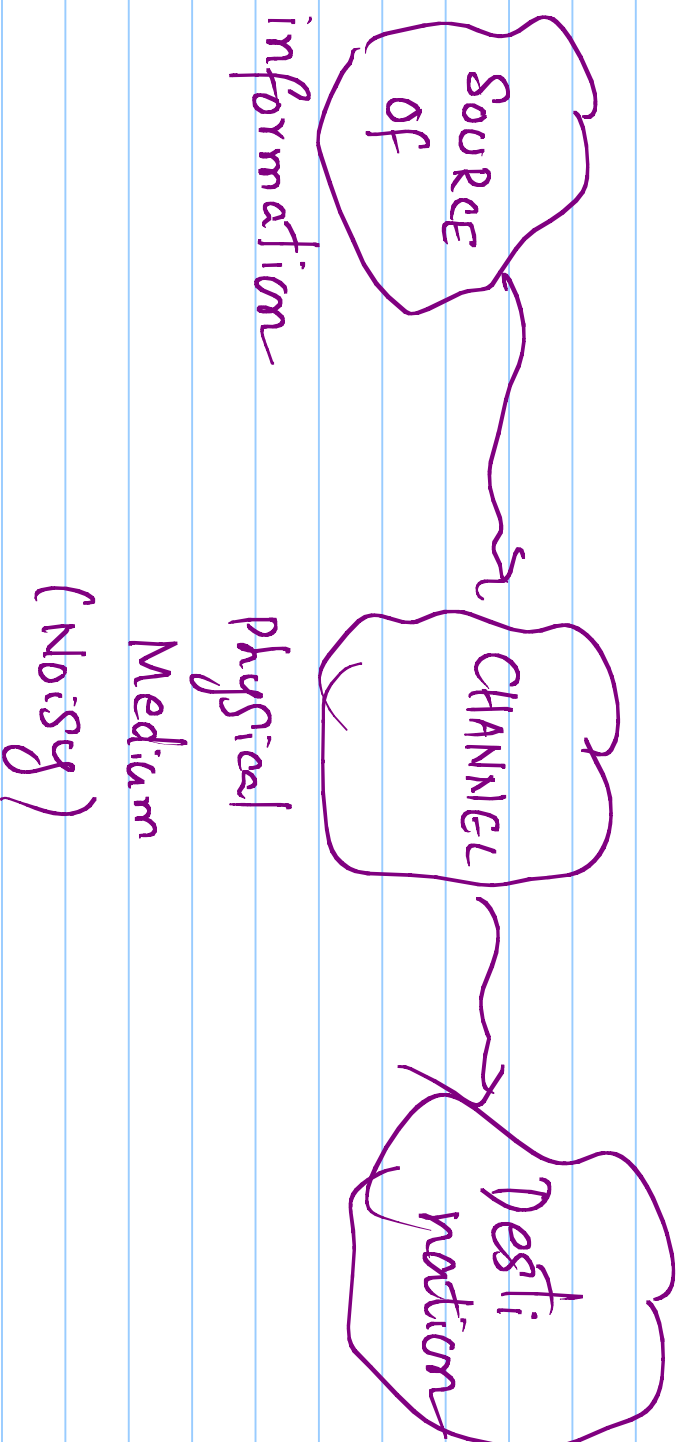
Demodulation

ISI channels & Equalization

Evaluation : Quiz 1 & 2 : 25 % each

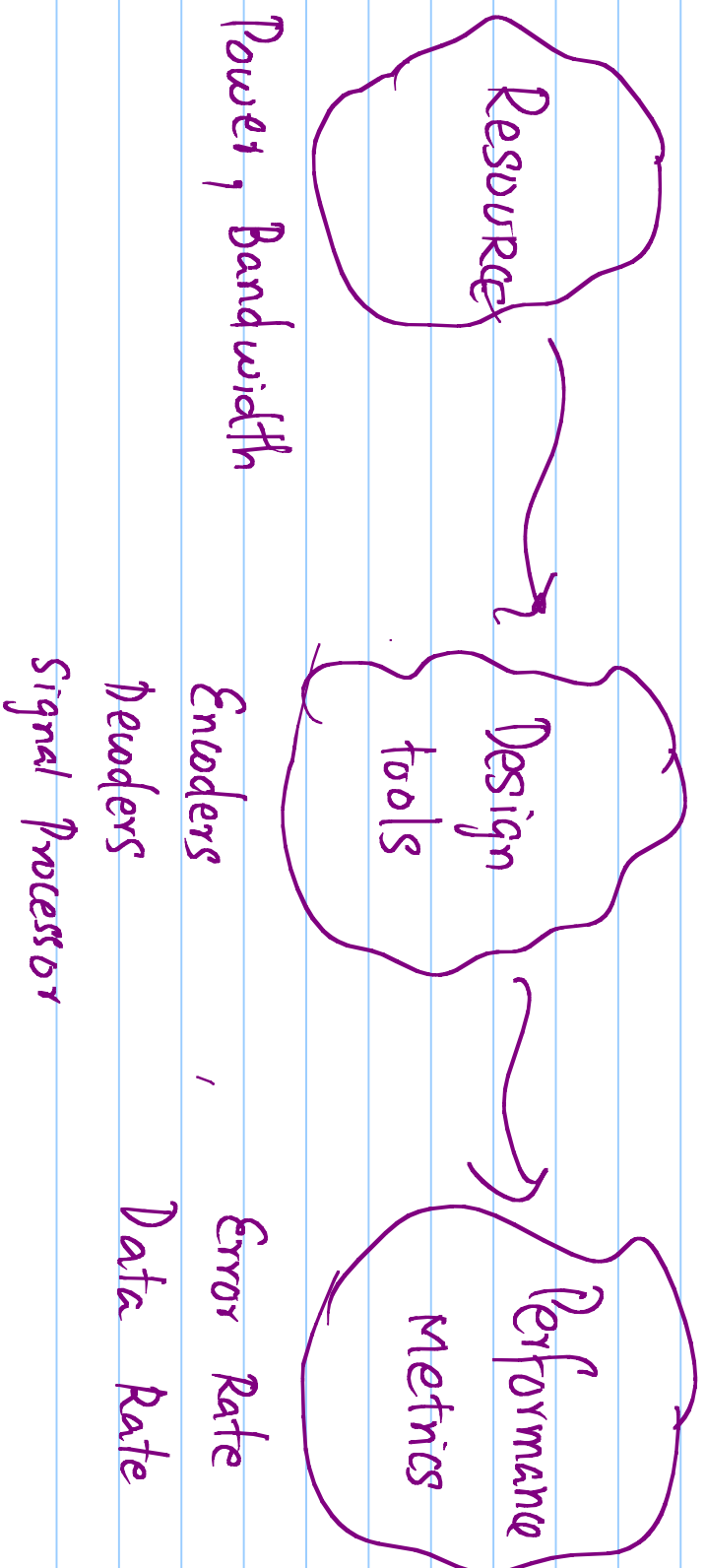
End Sem : 50 %

Comm. System

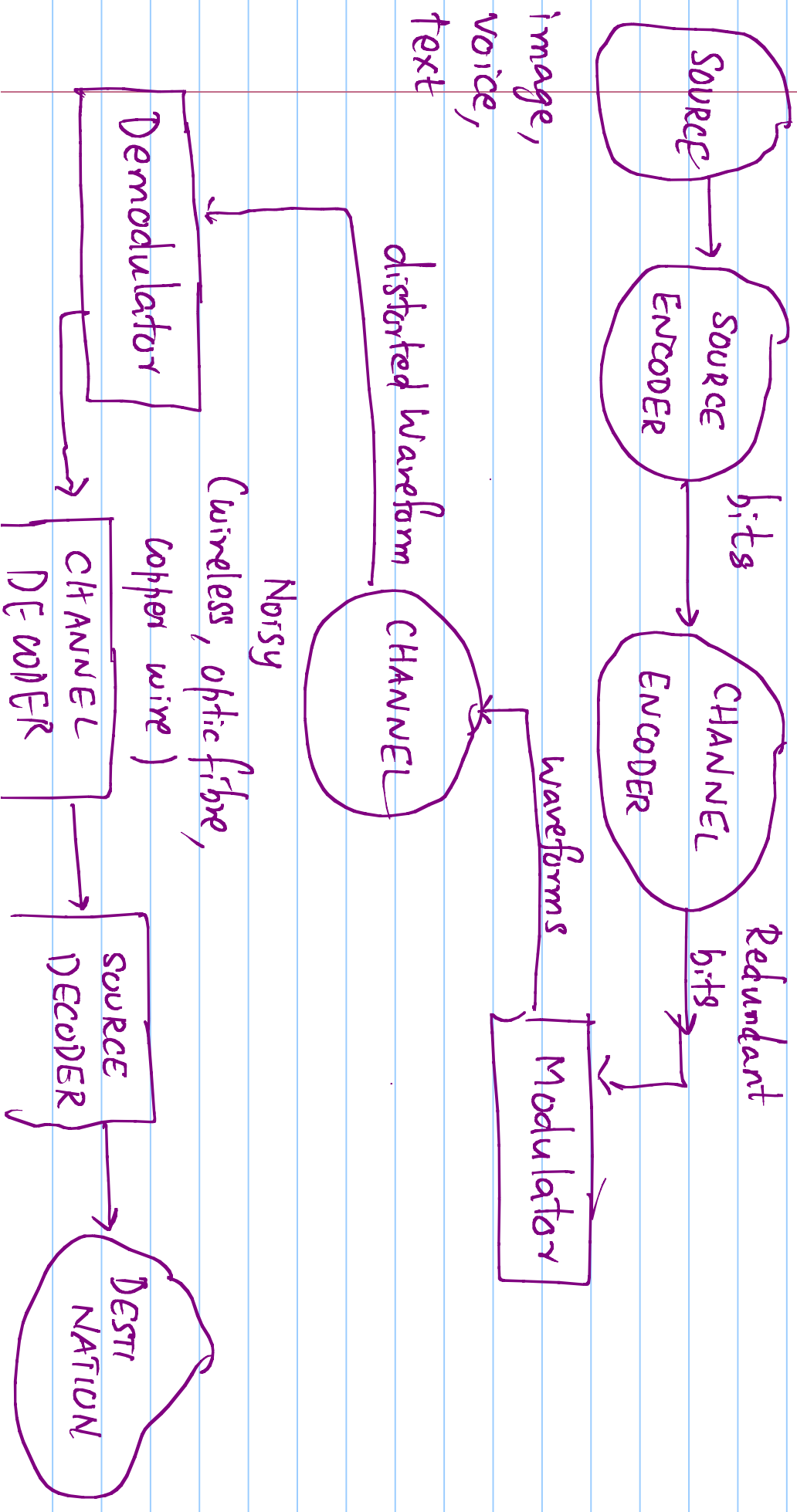


- * Info has to go from source to destination via noisy medium
- * Want reliable communication

Comm. System Design Principle



Components of Digital Comm. System



Reasons for using digital communication systems are from Shannon's theorems in information theory

① Channel Coding Theorem

We can build (almost) error-free digital communication systems across noisy medium with finite power & finite bandwidth

② Source - Channel Separation Theorem

Source coding & channel coding can be done separately,

Chapter 1:

Complex Baseband

Representation

a) Signals

→ Power, Energy, bandwidth

b) Baseband & Passband Signals (Fourier Transform)

c) Complex baseband Representation

Textbook:

Digital

Comm.

by Madhow

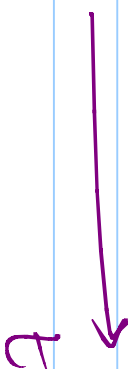
Signals

Signal $s(t)$ is a function of time t

t is continuous



$s(t)$



t

1) Energy of signal $s(t)$

$$E_s = \int_{-\infty}^{\infty} |s(t)|^2 dt$$

2) Power of signal $s(t)$

$$P_s = \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T |s(t)|^2 dt$$

Note:

If P_s is finite

then $E_s = \infty$

If E_s is finite,

$P_s = 0$

DC Value of signal

$$\overline{s(t)} = \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T s(t) dt$$

1) Real Sinusoid $s(t) = A \sin(2\pi f_0 t + \theta)$

Amplitude \downarrow Frequency \downarrow Phase \swarrow

2) Complex exponential $s(t) = A e^{j(2\pi f_0 t + \theta)}$

$$= A \left[\cos(2\pi f_0 t + \theta) + j \sin(2\pi f_0 t + \theta) \right]$$
$$= A e^{j\theta} \left[e^{j2\pi f_0 t} \right]$$

$$\text{Energy } E_s = \int_{-\infty}^{\infty} |A e^{j\theta} e^{j2\pi f_0 t}|^2 dt$$

$$= \int_{-\infty}^{\infty} A^2 dt$$

$$= \infty$$

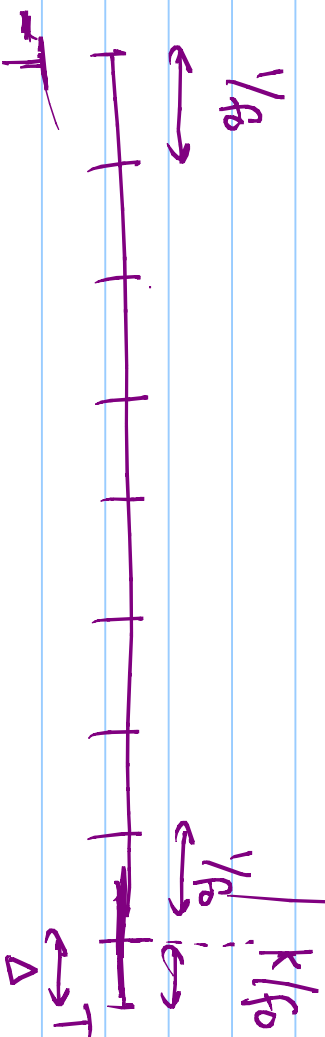
$$\text{Power } P_s = A^2 \quad \text{Since } |s(t)|^2 = A^2 \text{ for all } t$$

$$\text{Dc value of } A e^{j\theta} e^{j2\pi f_0 t} = ?$$

Need to find

$$\int_{-T}^T A e^{j\omega} e^{j2\pi f_0 t} dt$$

Time period is $\frac{1}{f_0}$



$$\int_{-T}^T A e^{j\omega} e^{j2\pi f_0 t} dt =$$

$$\int_{-T+k/f_0}^{-T+k/f_0+T} A e^{j\omega} e^{j2\pi f_0 t} dt + \int_{-T+2k/f_0}^{-T+2k/f_0+T} A e^{j\omega} e^{j2\pi f_0 t} dt + \dots$$

$$= \int_{-T+k/f_0}^T A e^{j\omega} e^{j2\pi f_0 t} dt$$

$$\leq \int_{-T}^T |A e^{j\omega} e^{j2\pi f_0 t}| dt$$

$$\leq \frac{-T+k}{f_0}$$

$$\leq \int_{-T}^T |A| dt$$

$$\leq \frac{-T+k}{f_0}$$

$$\Delta \leq \frac{1}{f_0}$$

$$\leq |A| \cdot \Delta$$

$$\leq \frac{|A|}{f_0}$$

Similarly we can show this integral $\geq \frac{-|A|}{f_0}$

$$S_0 = \int_{-T}^T A e^{j\theta} e^{j2\pi f_0 t} dt \leq \frac{|A|}{f_0} \text{ for any } T$$

dc value

$$\lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T A e^{j\theta} e^{j2\pi f_0 t} dt \leq \lim_{T \rightarrow \infty} \frac{1}{2T} \frac{|A|}{f_0} = 0$$

Example: Real Sinusoid

$$s(t) = A \sin(2\pi f_0 t + \theta) = \text{Imag} \left\{ A e^{j\theta} e^{j2\pi f_0 t} \right\}$$

So dc value of $s(t) = 0$, $E_s = \frac{\infty}{2}$ (Verify)
 $P_s = |A|^2/2$

Inner Product between two signals $s(t)$ & $r(t)$ is defined as

$$\langle s(t), r(t) \rangle = \int_{-\infty}^{\infty} s(t) r^*(t) dt$$

* \rightarrow denotes conjugation

Two signals are called orthogonal if their inner product is zero

Bandwidth of a Signal

We need to know frequency components in a signal to understand bandwidth

FOURIER TRANSFORM

Let $x(t)$ be a finite Energy Signal

FOURIER TRANSFORM (FT) of signal $x(t)$

defined as

$$X(f) = \int_{-\infty}^{\infty} x(t) e^{-j2\pi f t} dt$$

→ function of f

$X(f)$ is called Spectrum of $x(t)$; $f \in (-\infty, \infty)$

$X(f)$ is in general Complex Valued

(even if $x(t)$ is real)

$|X(f)| \rightarrow$ Magnitude Spectrum

$\angle X(f) \rightarrow$ Phase Spectrum

From $X(f)$, we get $x(t)$ as

$$x(t) = \int_{-\infty}^{\infty} X(f) e^{j2\pi f t} df$$

We have both +ve & -ve frequencies in spectrum

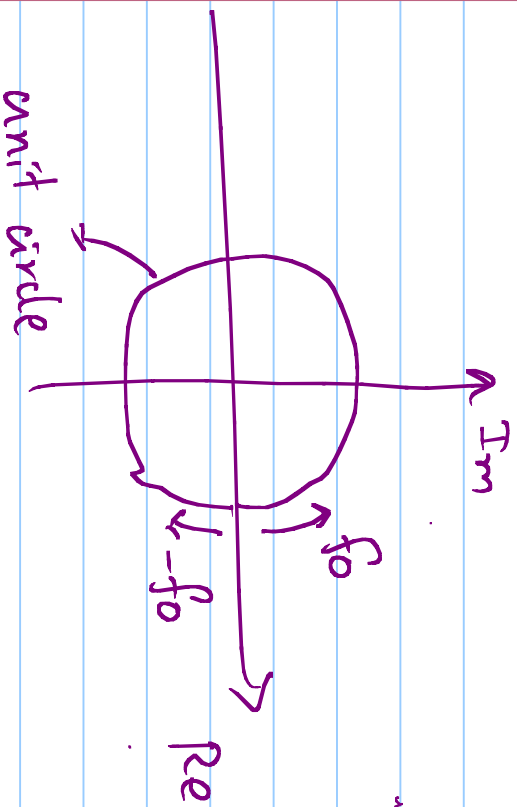
Complex exponentials

$$e^{j2\pi f_0 t} \quad \& \quad e^{-j2\pi f_0 t}$$

(+ve) (-ve)

are different

$$\begin{aligned} & \cos(2\pi(-f_0)t) \\ &= \cos(2\pi f_0 t) \\ & \sin(2\pi(-f_0)t) \\ &= -\sin(2\pi f_0 t) \end{aligned}$$

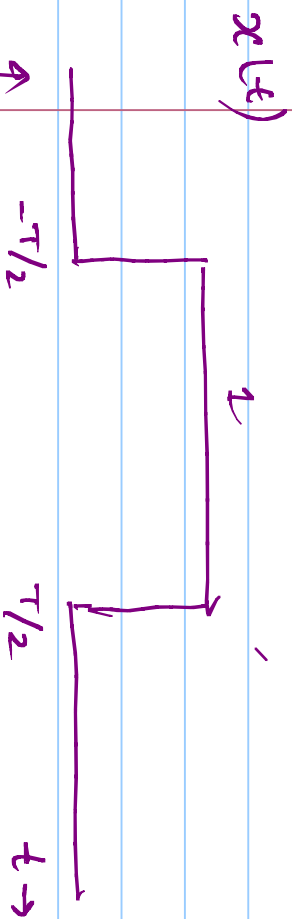


Phasors $e^{j2\pi f_0 t}$ & $e^{-j2\pi f_0 t}$ rotate in opposite directions

Example

Notation $x(t) \xleftrightarrow{F} X(f)$

$$x(t) = \begin{cases} 1 & \text{if } |t| \leq T/2 \\ 0 & \text{else} \end{cases}$$

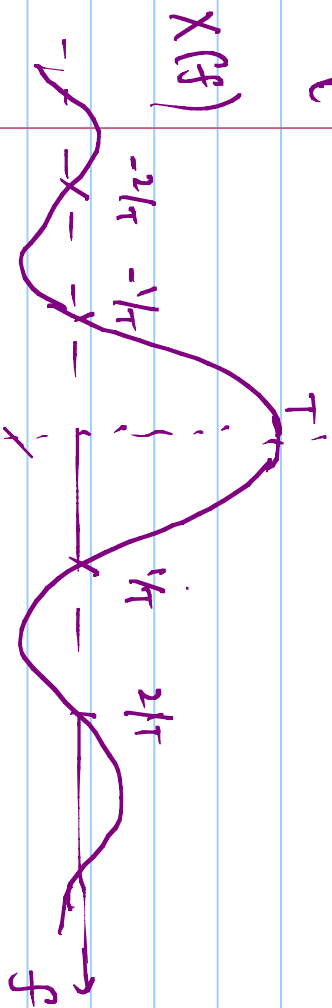


$$X(f) = \int_{-T/2}^{T/2} e^{-j2\pi ft} dt$$

$$= \left. \frac{e^{-j2\pi ft}}{-j2\pi f} \right|_{-T/2}^{T/2}$$

$$= \frac{\sin(\pi f T)}{\pi f}$$

$$= T \operatorname{Sinc}(fT)$$



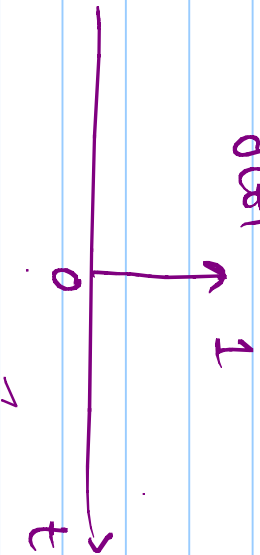
$$\text{Sinc}(x) = \frac{\text{Sin } \pi x}{\pi x}$$

Extension of FOURIER TRANSFORM to

Signals with infinite energy using impulse function.

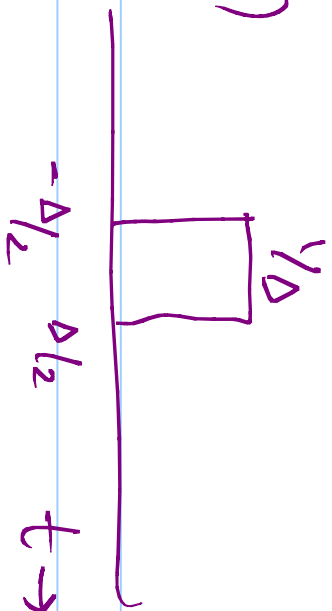
Delta function $\delta(t)$ denotes impulse function ✓

$$\int_{-\infty}^{\infty} \delta(t) dt = 1$$



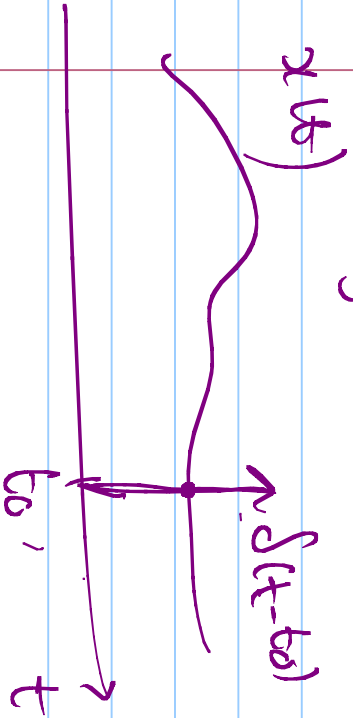
$$f(t) = \lim_{\Delta \rightarrow 0} f_{\Delta}(t)$$

$f_{\Delta}(t)$



Sifting Property:

Say $x(t)$ is a continuous function



$$x(t_0) = \int_{-\infty}^{\infty} x(t) \delta(t-t_0) dt$$

$$1) \delta(t) \xleftrightarrow{\mathcal{F}} 1 \quad (\text{Constant for all } f)$$

$$2) Ae^{j\theta} e^{j2\pi f_0 t} \xleftrightarrow{\mathcal{F}} Ae^{j\theta} \delta(f - f_0)$$

3) Linearity

$$\alpha x(t) + \beta y(t) \xleftrightarrow{\mathcal{F}} \alpha X(f) + \beta Y(f)$$

$$A(e^{j2\pi f_0 t + \theta} - e^{-j(2\pi f_0 t + \theta)}) \xleftrightarrow{\mathcal{F}} A \sin(2\pi f_0 t + \theta) \xleftrightarrow{\mathcal{F}} \frac{A}{2j} e^{j\theta} \delta(f - f_0) - \frac{A}{2j} e^{-j\theta} \delta(f + f_0)$$

Real Sinusoid

4) Time delay \Leftrightarrow linear phase shift
in frequency domain

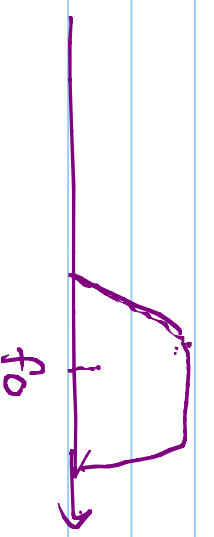
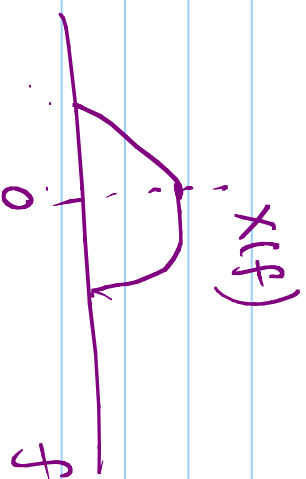
$$x(t) \xleftrightarrow{F} X(f)$$

$$x(t-t_0) \xleftrightarrow{F} X(f) e^{-j2\pi f t_0}$$

$$x(t) \xleftrightarrow{F} X(f)$$

5) Modulation Property

$$x(t) e^{j2\pi f_0 t} \xleftrightarrow{F} X(f-f_0)$$



6) Parseval's Theorem

$$\int_{-\infty}^{\infty} |x(t)|^2 dt = \int_{-\infty}^{\infty} |X(f)|^2 df$$

Energy in time domain = Energy in frequency domain

7) Suppose $x(t)$ is Real valued Signal

$$x(t) \xrightarrow{F} X(f)$$

Then

$$X(f) = X^*(-f)$$

that is

$$\text{Real part } \operatorname{Re} \{ X(f) \} = \operatorname{Re} \{ X(-f) \}$$

$$\text{imag. part } \operatorname{Im} \{ X(f) \} = - \operatorname{Im} \{ X(-f) \}$$

For real signals, Spectrum on positive frequencies alone is sufficient to reconstruct the signal

8) Differentiation

$$x(t) \longrightarrow X(f)$$

$$\frac{d}{dt} x(t) \longrightarrow j2\pi f X(f)$$

↓

linear gain with frequency

Higher gain for high frequency

(High Pass filter)

9) Integration

$$x(t) \xrightarrow{F} X(f)$$

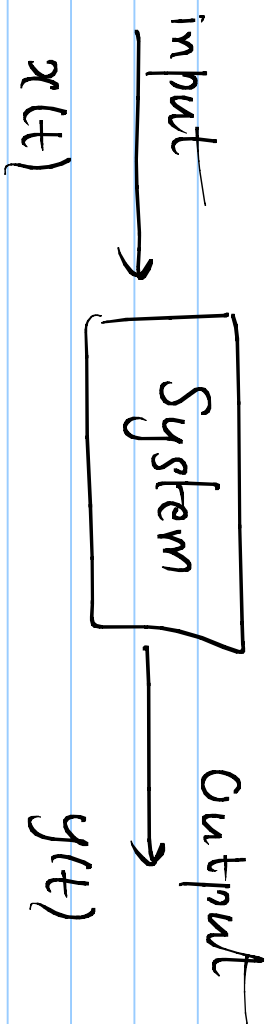
$$y(t) = \int_{-\infty}^t x(\tau) d\tau$$

$$Y(f) = \frac{X(f)}{\int 2\pi f} + \bar{x} \delta(f)$$

$$\bar{x} = \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T x(\tau) d\tau$$

low pass filter

LTI Systems



$$x(t) \rightarrow y(t) \quad (\text{shorthand notation})$$

1) Linearity

Suppose

$$\left\{ \begin{array}{l} x_1(t) \rightarrow y_1(t) \\ x_2(t) \rightarrow y_2(t) \end{array} \right.$$

if $\alpha x_1(t) + \beta x_2(t) \rightarrow \alpha y_1(t) + \beta y_2(t)$

then, system is linear

2) time invariance

if $x(t) \rightarrow y(t)$

then $x(t-t_0) \rightarrow y(t-t_0)$

System is time invariant

LTI is both linear & time invariant

System

Properties of LTI System



$h(t) \rightarrow$ impulse response of system

$h(t)$ Completely characterizes the system

2) For input $x(t)$, output $y(t)$ is

given by

$$y(t) = \int_{-\infty}^{\infty} x(\tau) h(t-\tau) d\tau$$

Convolution

Proof: We know

$$\delta(t) \rightarrow h(t)$$

(Time
invariance,
 $\delta(t-\tau) \rightarrow h(t-\tau)$)

(linearity) $x(\tau) \delta(t-\tau) \rightarrow x(\tau) h(t-\tau)$

$$x(t) = \int_{-\infty}^{\infty} x(\tau) \delta(t-\tau) d\tau \rightarrow \int_{-\infty}^{\infty} x(\tau) h(t-\tau) d\tau$$

Sifting Property $y(t)$

$$y(t) = x(t) * h(t)$$

↓

convolution

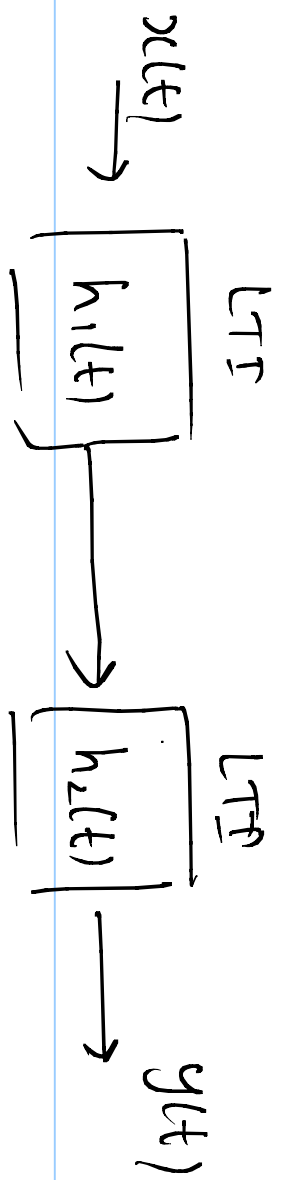
Properties of convolution

Commutative 1) $x(t) * h(t) = h(t) * x(t)$

Distributive 2) $x(t) * (h_1(t) + h_2(t))$

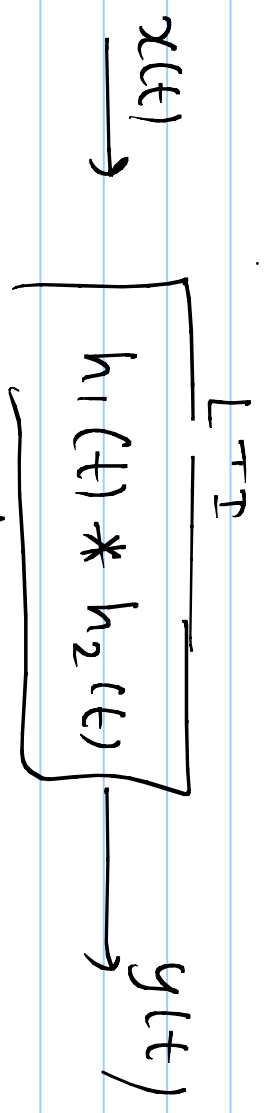
$$= x(t) * h_1(t) + x(t) * h_2(t)$$

Associative 3) $x(t) * (h_1(t) * h_2(t)) = (x(t) * h_1(t)) * h_2(t)$

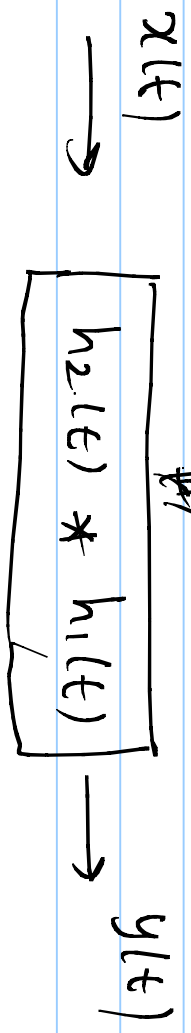


Equivalent \Downarrow

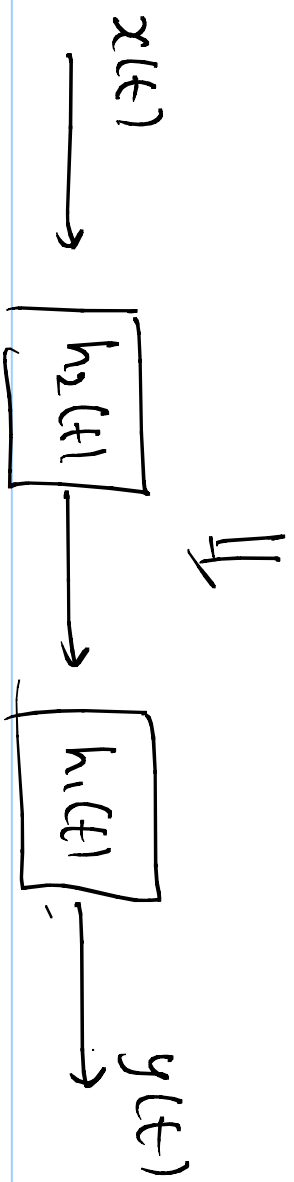
$$y(t) = (x(t) * h_1(t)) * h_2(t)$$



\Downarrow Commutative



\Downarrow Associativity



Fourier Transforms & LTI Systems

$$x(t) \rightarrow X(f)$$

$$h(t) \rightarrow H(f)$$

$$x(t) * h(t) \rightarrow Y(f) = X(f)H(f)$$

Convolution in time domain \Leftrightarrow Multiplication in frequency domain

$$x(t) \cdot h(t)$$

\Rightarrow

$$X(f) * H(f)$$

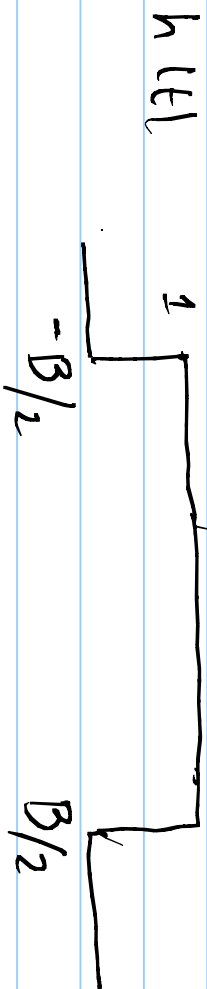
Multiplication
in time

convolution in
frequency domain

Example (convolution)

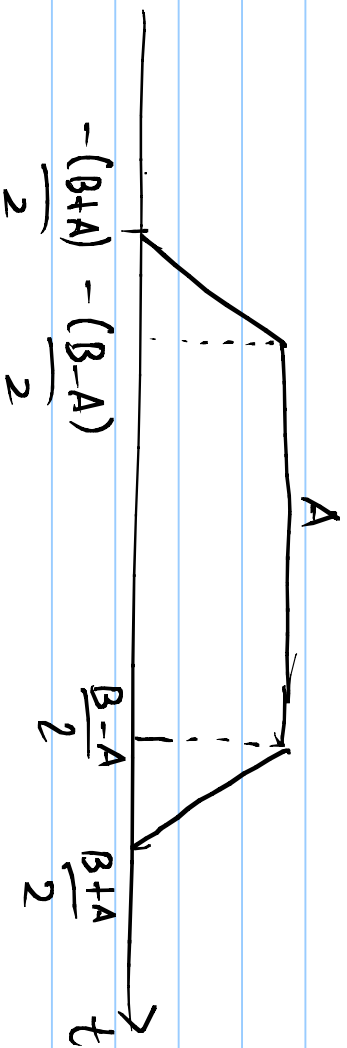


$$B \geq A$$



$$y(t) = x(t) * h(t)$$

$y(t)$



Bandwidth of Signals

$$x(t) \xleftrightarrow{F} X(f)$$

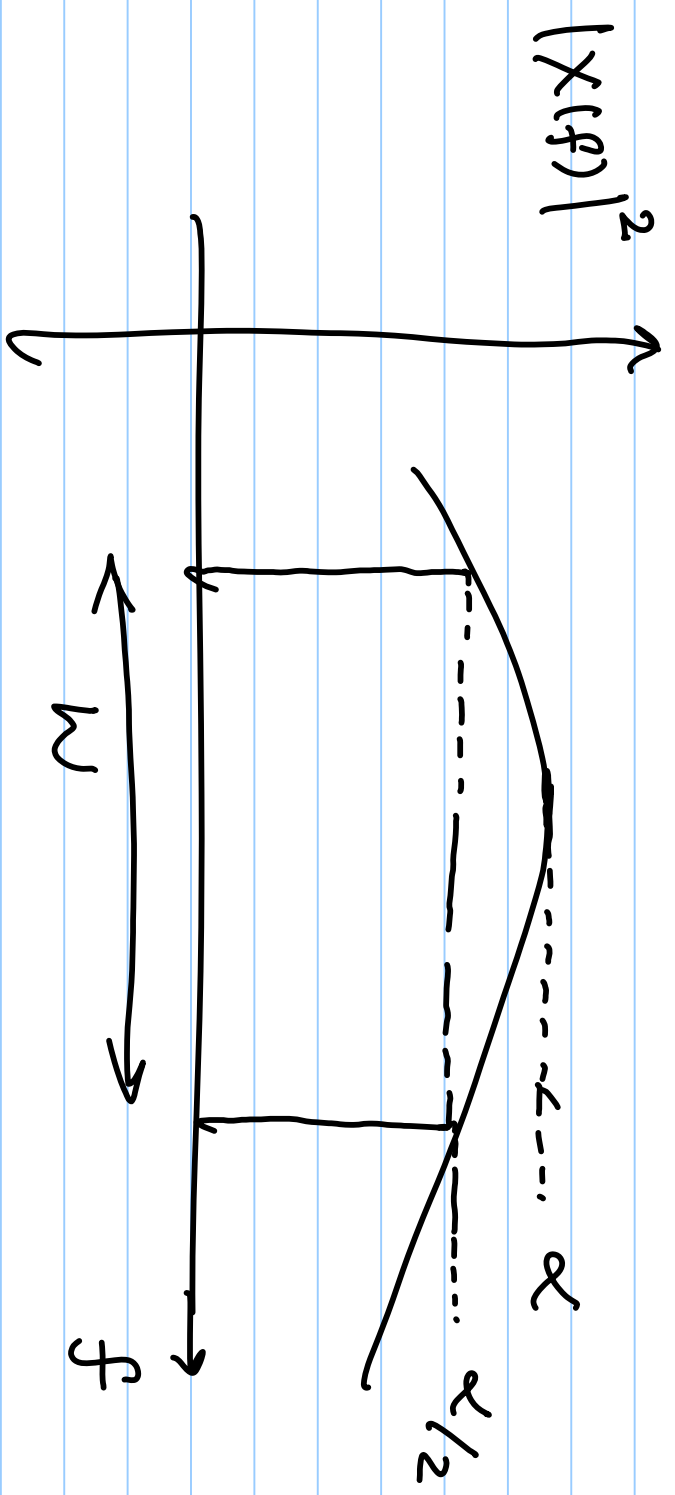
Spectrum $X(f)$ gives frequency components present in $x(t)$

Signals are rarely bandlimited

Spectrum $X(f)$ is non-zero from $-\infty$ to ∞

Two Notions of Bandwidth

① 3 dB Bandwidth



3 dB Bandwidth = W

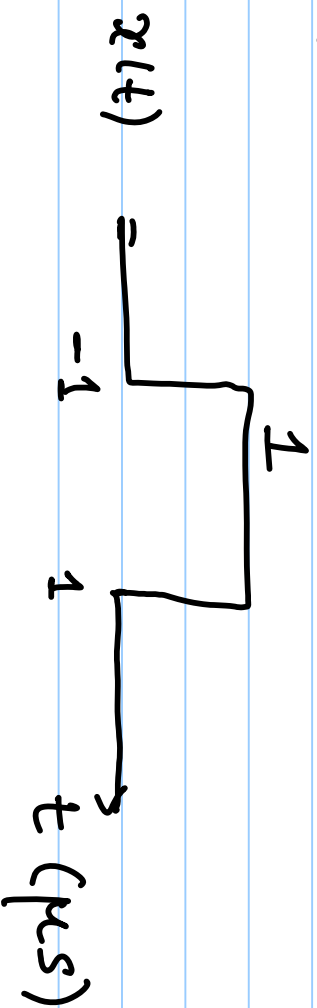
② α - fraction bandwidth

Width of Band of frequencies (continuous)

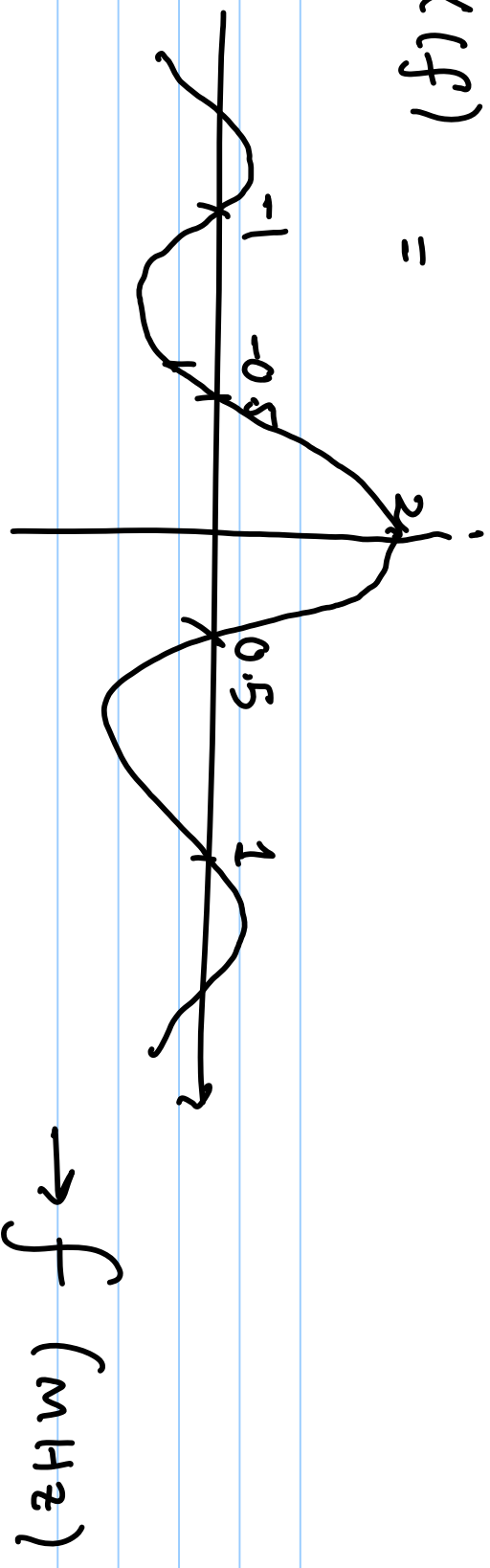
which contain α -1. of total energy

of signal

Example:



$$X(f) =$$



$$X(f) = \frac{\sin 2\pi f}{\pi f} \quad (\text{unit is MHz})$$

of f

Find Bandwidth which contains 99% of total energy.

Find ω such that

$$\omega \int_{-\omega}^{\omega} |x(f)|^2 df = 0.99 \underbrace{\int_{-\infty}^{\infty} |x(t)|^2 dt}_{2}$$

$$= 1.98$$

$$\omega \int_{-\omega}^{\omega} \frac{\sin^2 2\pi f}{(\pi f)^2} df = 1.98$$

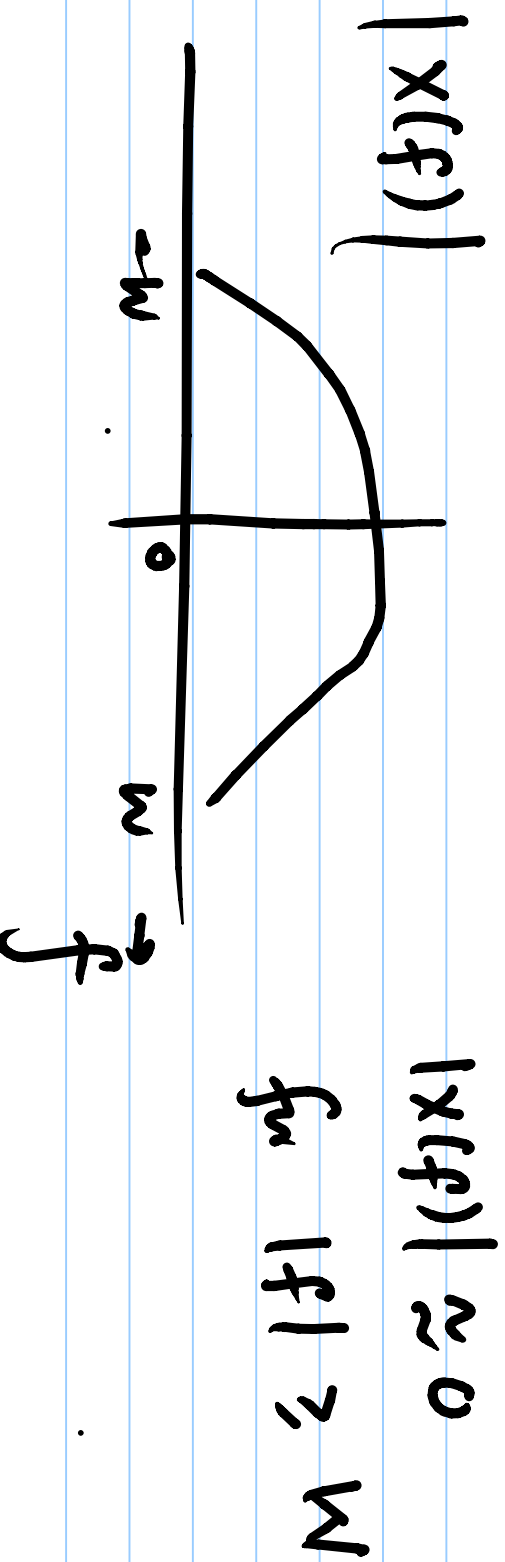
Numerically find $\omega \approx 5.1 \text{ MHz}$

Baseband and Passband Signals

Signal $x(t)$ is called baseband

Signal if its energy is

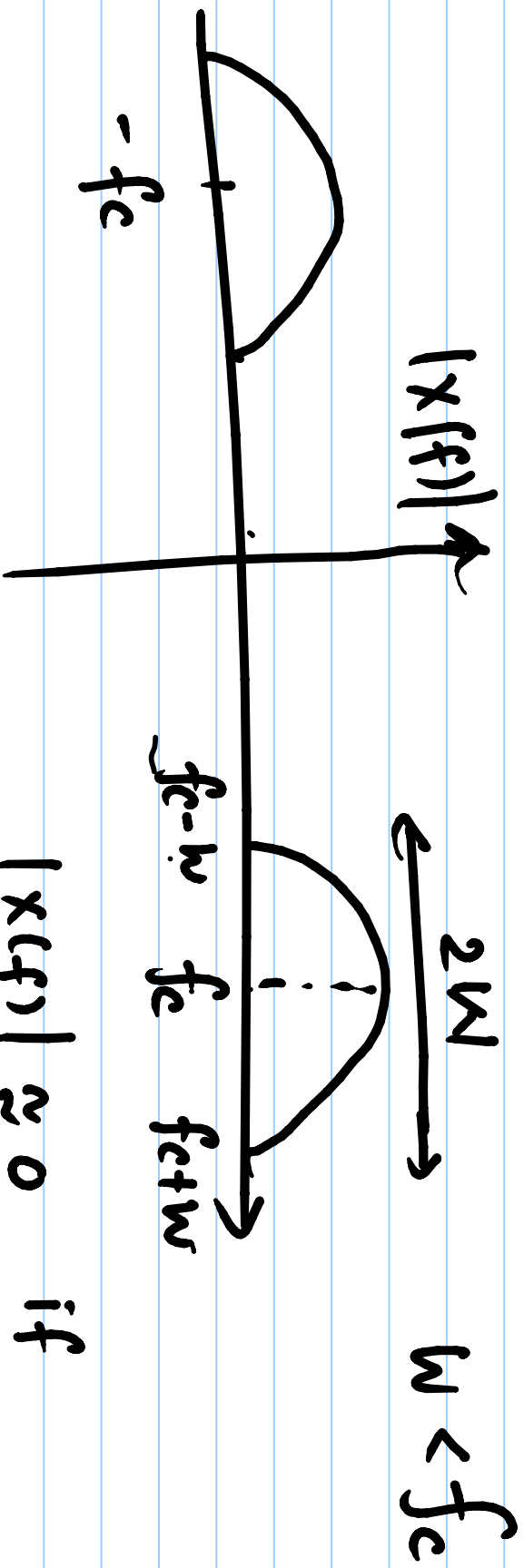
concentrated around DC (zero frequency)



Passband Signal

Energy is concentrated around

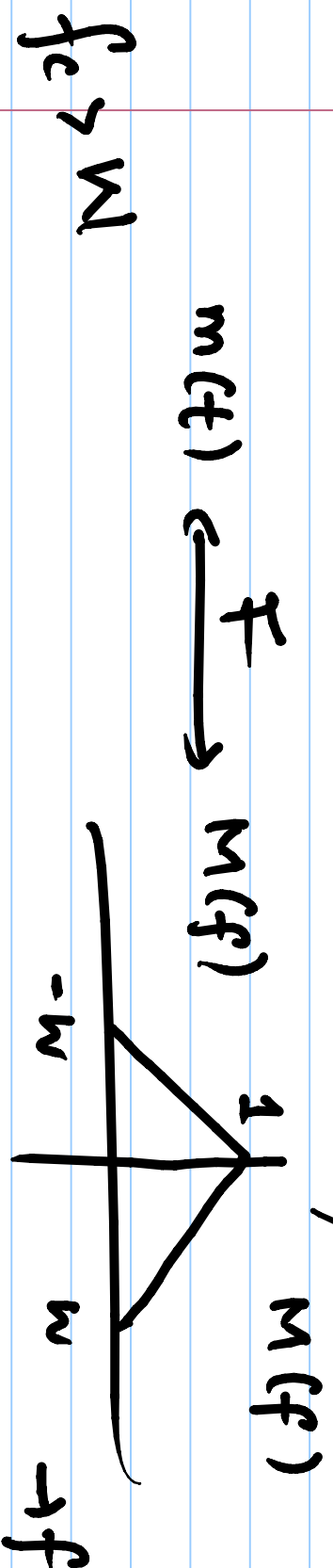
a band away from zero



Connection between baseband & Passband Signals

Say we have message signal $m(t)$
(real valued)

(base band)



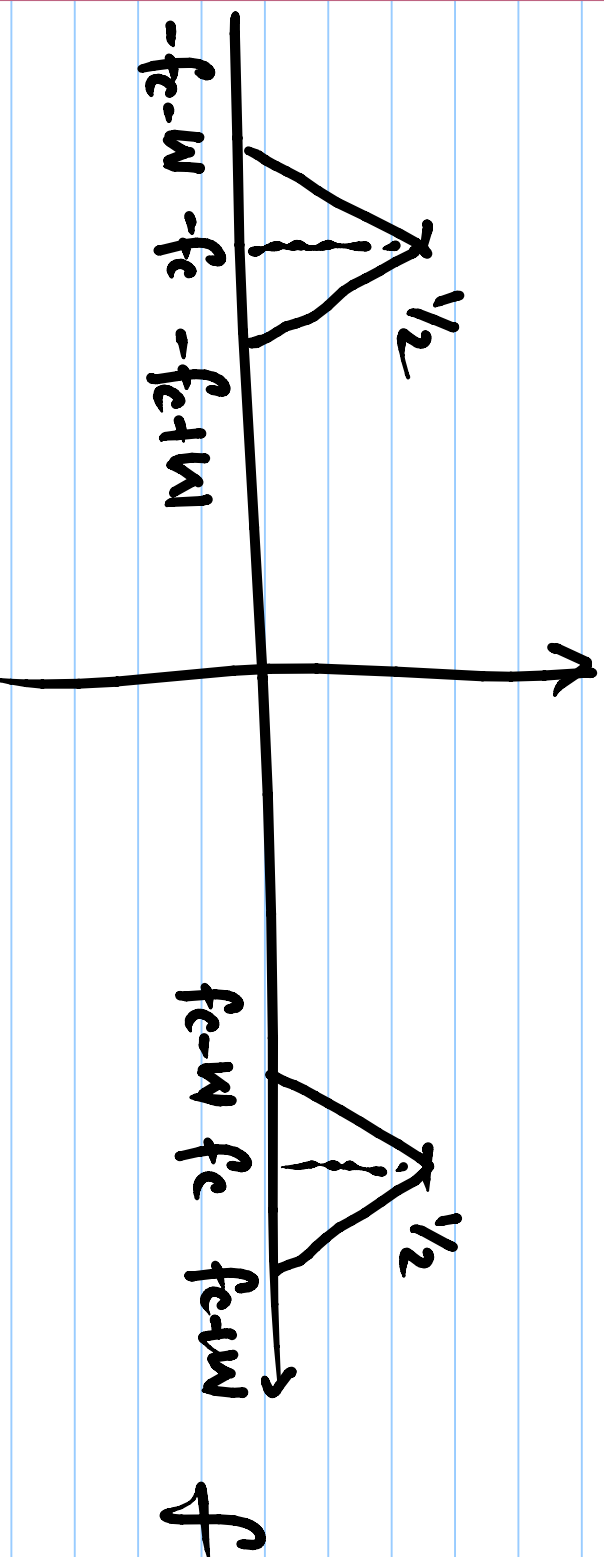
Suppose we want to send this message
Via carrier frequency f_c

$$\text{Let } m_p(t) = m(t) \cos(2\pi f_c t)$$

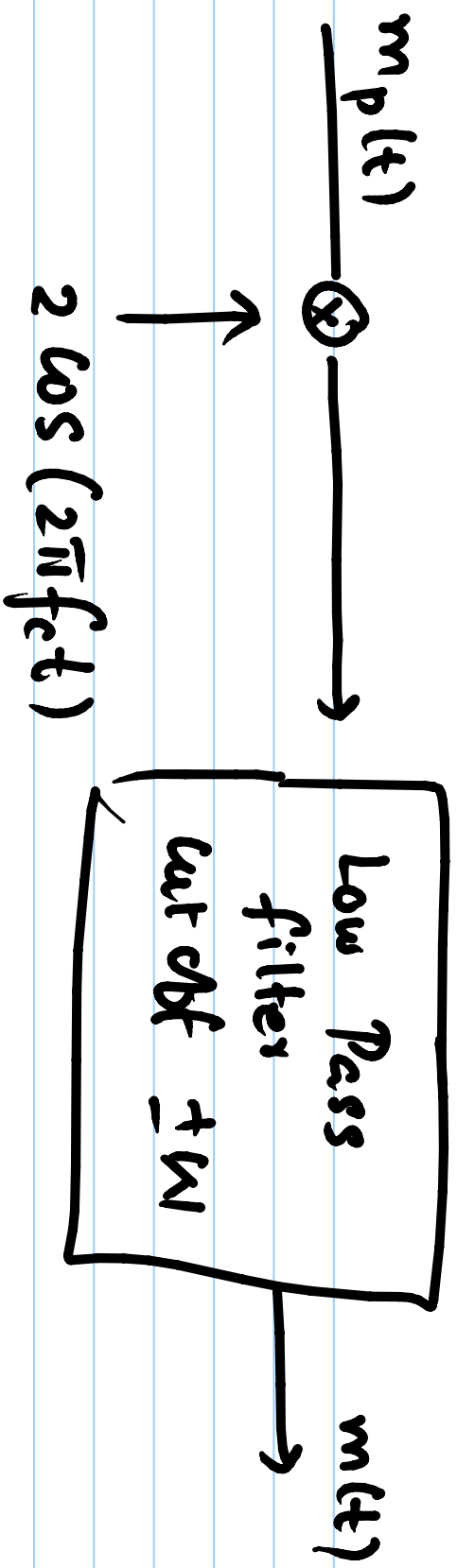
\downarrow
 \neq

$$\begin{aligned} \text{Spectrum } M_p(f) &= M(f) * \left(\frac{1}{2} \delta(f-f_c) \right. \\ &\quad \left. + \frac{1}{2} \delta(f+f_c) \right) \\ &= \frac{1}{2} M(f-f_c) + \frac{1}{2} M(f+f_c) \end{aligned}$$

$M_p(f)$



From $m_p(t)$ we can get original message $m(t)$
as follows



$$\begin{aligned}
 2 m_p(t) \cos(2\pi f_c t) &= m(t) 2 \cos^2(2\pi f_c t) \\
 &= m(t) [1 + \cos 4\pi f_c t]
 \end{aligned}$$

$$= m(t) + m(t) \cos 4\pi f_c t$$

Passband Signal

centered around

$$2f_c$$

base band
signal

frequencies

from $-W$ to W

eliminated by

LPF



IN-Phase & Quadrature Modulation

Let $x_c(t)$ & $x_s(t)$ be two

real different baseband signals

$$|X_c(f)| \approx 0 \quad \text{for } |f| > W$$

$$|X_s(f)| \approx 0 \quad \text{for } |f| > W$$

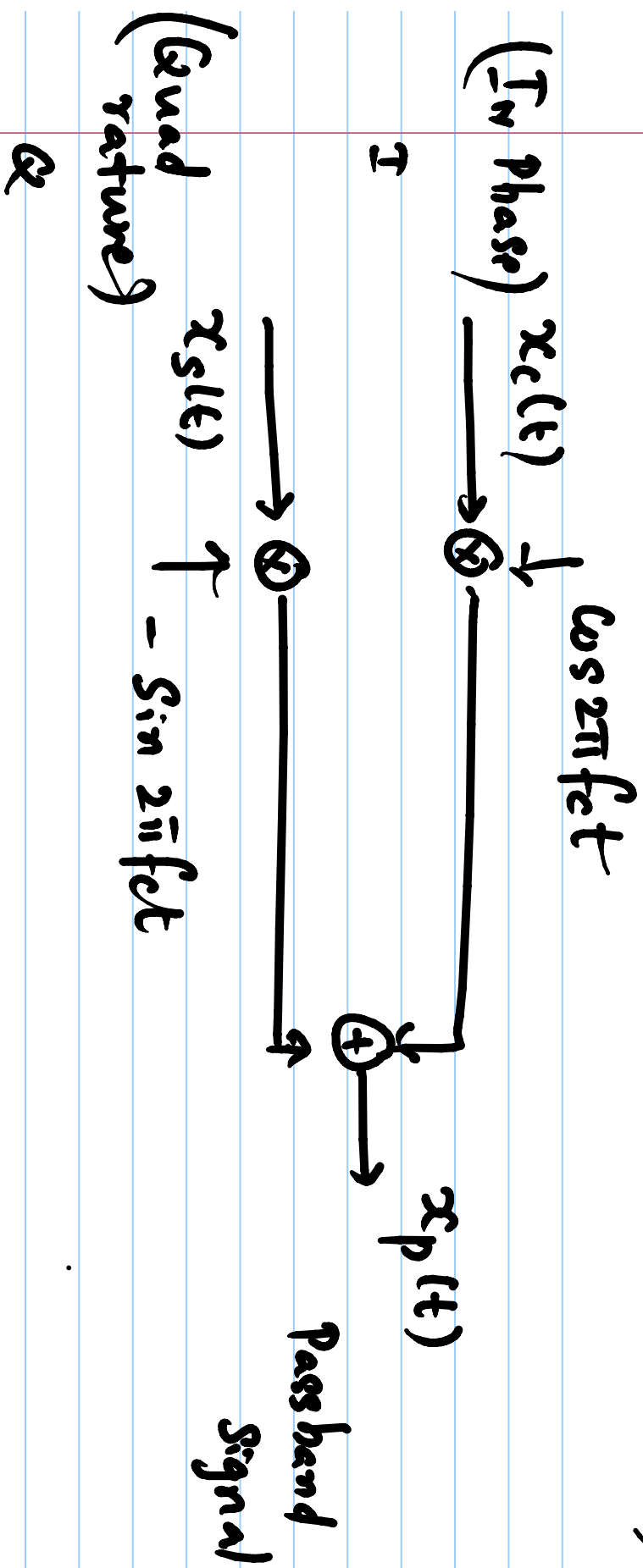
$$x_p(t) = x_c(t) \cos 2\pi f_c t - x_s(t) \sin 2\pi f_c t$$

Passband Signal

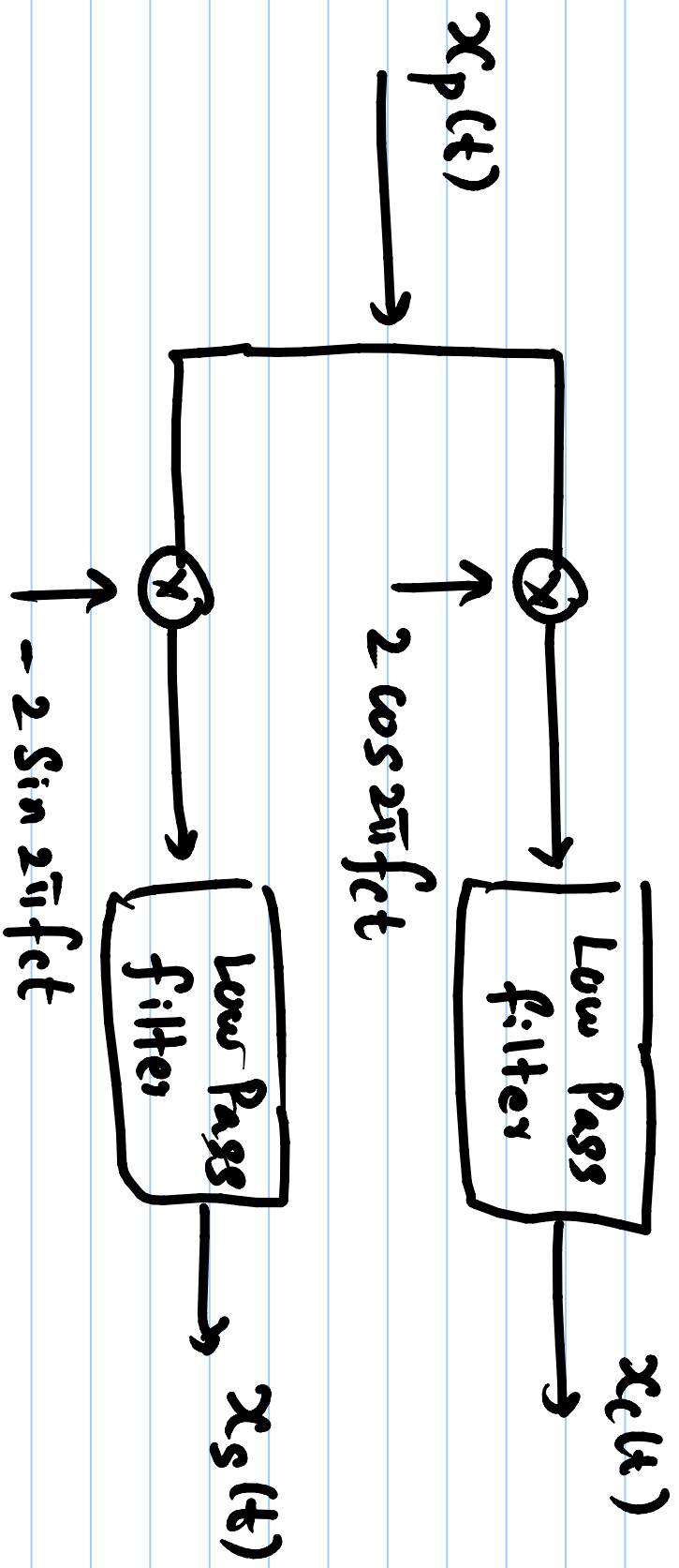
$$\text{Spectrum } |X_p(f)| \approx 0 \text{ if}$$

$$|f \pm f_c| > W$$

Upconversion (baseband to Passband)



Down Conversion (Passband to baseband)



$$x_p(t) = x_c(t) \cos 2\pi f_c t - x_s(t) \sin 2\pi f_c t$$

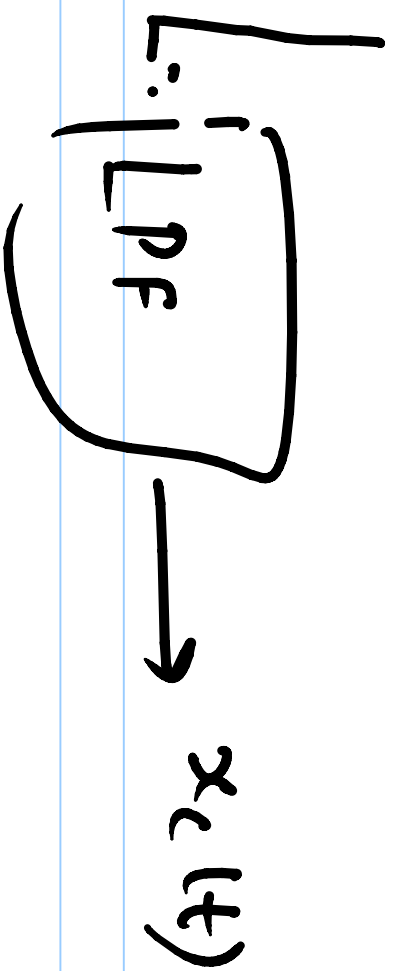
Top Branch of Down Conversion

$$x_p(t) \cos(2\pi f_c t)$$

$$= 2 x_c(t) \cos^2 2\pi f_c t - 2 x_s(t) \sin(2\pi f_c t) \cos(2\pi f_c t)$$

$$= x_c(t) [1 + \cos 4\pi f_c t] - x_s(t) \sin(4\pi f_c t)$$

↓
Centered $2f_c$ Pass band at $2f_c$



Verify yourself for quadrature component

Main Result: Two different baseband

Signals (In phase & Quadrature component)

are sent via \cos & \sin carriers

Orthogonality of I & Q components

$$x_p(t) = \underbrace{x_c(t) \cos 2\pi f_c t}_{\text{I}} - \underbrace{x_s(t) \sin 2\pi f_c t}_{\text{Q}}$$

$$a(t) = x_c(t) \cos 2\pi f_c t$$

$$b(t) = x_s(t) \sin 2\pi f_c t$$

Claim: $a(t)$ & $b(t)$ are orthogonal

$$\int_{-\infty}^{\infty} a(t) b(t) dt = 0$$

Proof:

$$\text{Let } c(t) = x_c(t) x_s(t)$$

$$\text{Spectrum } C(f) = X_c(f) * X_s(f)$$

$$\int \int \text{limited to}$$

$$-w \text{ to } w$$

limited to

$$-2w \text{ to } +2w$$

$c(t)$ is base band signal (Spectrum $-2w$ to $+2w$)

$$a(t)b(t) = x_c(t) x_s(t) \cos 2\pi f_c t \sin 2\pi f_c t$$

$$= c(t) \frac{\sin 4\pi f_c t}{2}$$



↓

Passband Signal centered $2f_c$

-

↓

Spectrum exists $2f_c - 2W$ to

$2f_c + 2W$

(on positive side)

(Conjugate Symmetry on
negative side)

Since $f_c > w$, we have $2f_c - 2w > 0$

Dc component in spectrum is

$a(t) \cdot b(t)$ is zero

$$\text{So } \int_{-\infty}^{\infty} a(t) b(t) dt = 0$$

Complex Envelope

$$(I) \quad (R)$$

Let $x(t) = x_c(t) + j x_s(t)$

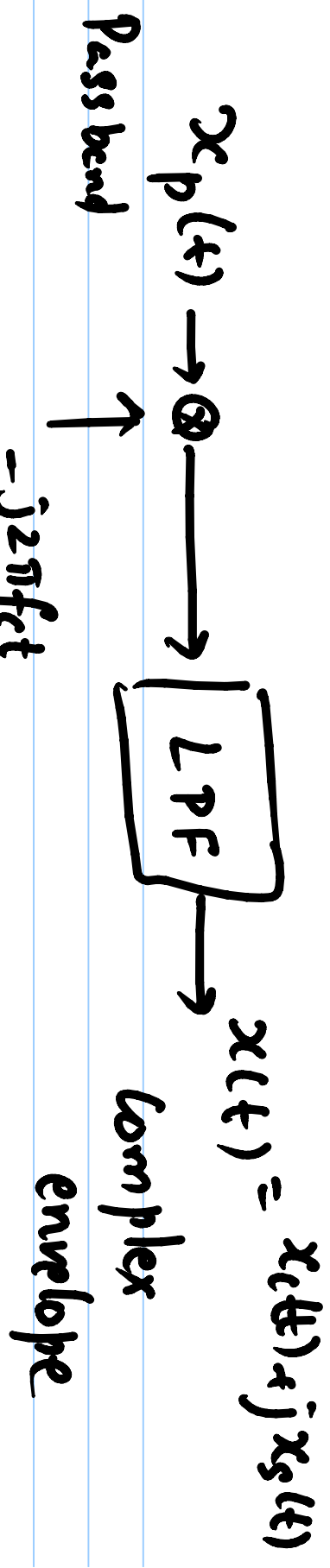
$x_c(t)$, $x_s(t)$ are

Complex envelope

real baseband signals

Passband Signal $x_p(t) = x_c(t) \cos 2\pi f_c t$

$$x_p(t) = \operatorname{Re} \left\{ x_c(t) e^{j2\pi f_c t} - x_s(t) \sin 2\pi f_c t \right\}$$



FREQUENCY DOMAIN RELATIONSHIP

between baseband & Passband

Signals

Let $x_c(t)$ & $x_s(t)$ be

real baseband signal

freq. components from $-W$ to $+W$

Complex envelope $x(t) = x_c(t) + j x_s(t)$

↳ freq. components $-W$ to W

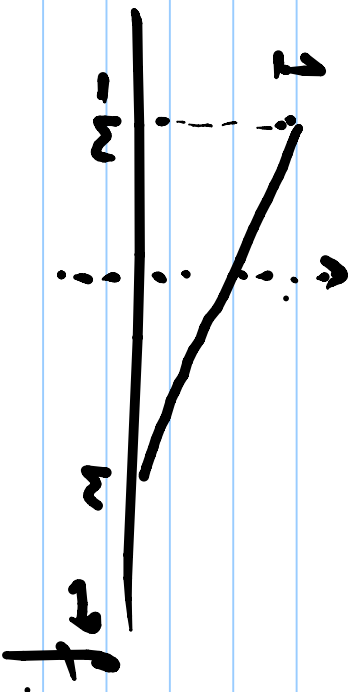
$$x_p(t) = \operatorname{Re} \{ x(t) e^{j2\pi f t} \}$$

$x(t)$ has all the information

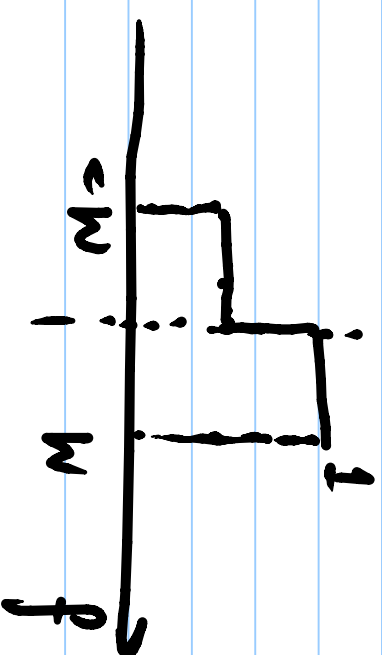
about $x_c(t)$, $x_s(t)$

Spectrum $x(t) \xleftrightarrow{F} X(f)$

Suppose $\operatorname{Re}\{X(f)\}$



$\operatorname{Im}\{X(f)\}$

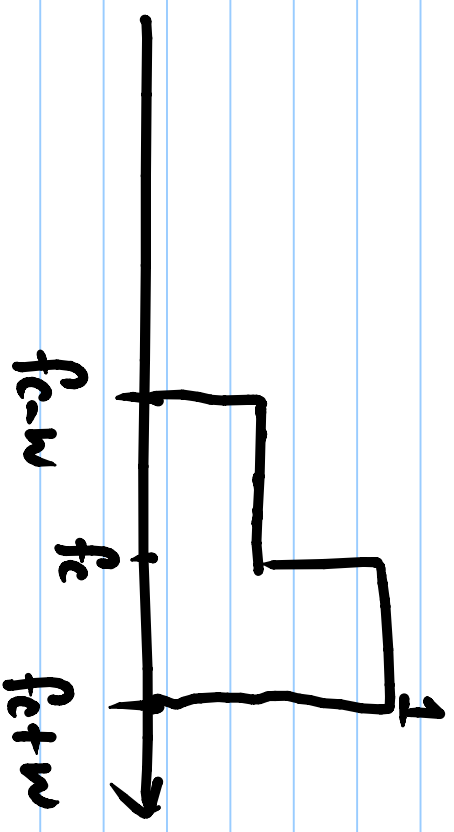
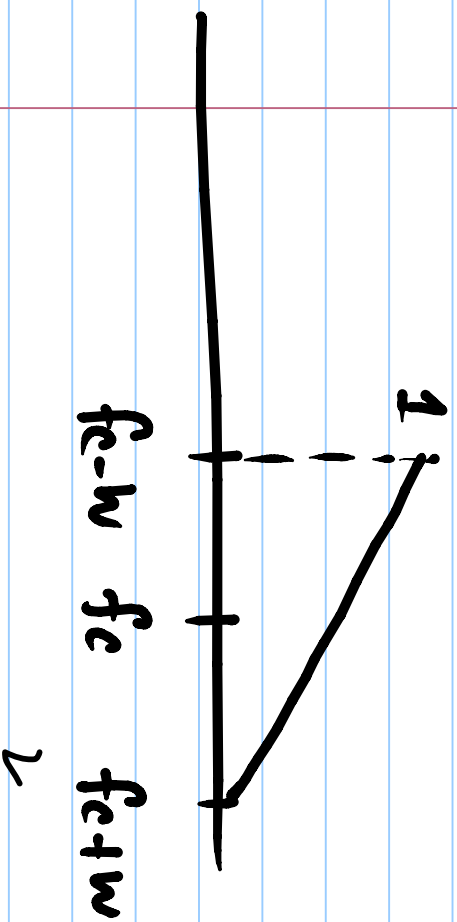


Define $C(f) = x(t) e^{j2\pi fct}$

We have $C(f) = X(f - f_c)$

Re $\{C(f)\}$

Im $\{C(f)\}$



$$x_p(t) = \operatorname{Re}\{c(t)\} \rightarrow \text{conjugation}$$

$$= \frac{c(t) + c^*(t)}{2}$$

$$c(t) \xrightarrow{f} c(f)$$

$$c^*(t) \leftrightarrow c^*(-f)$$

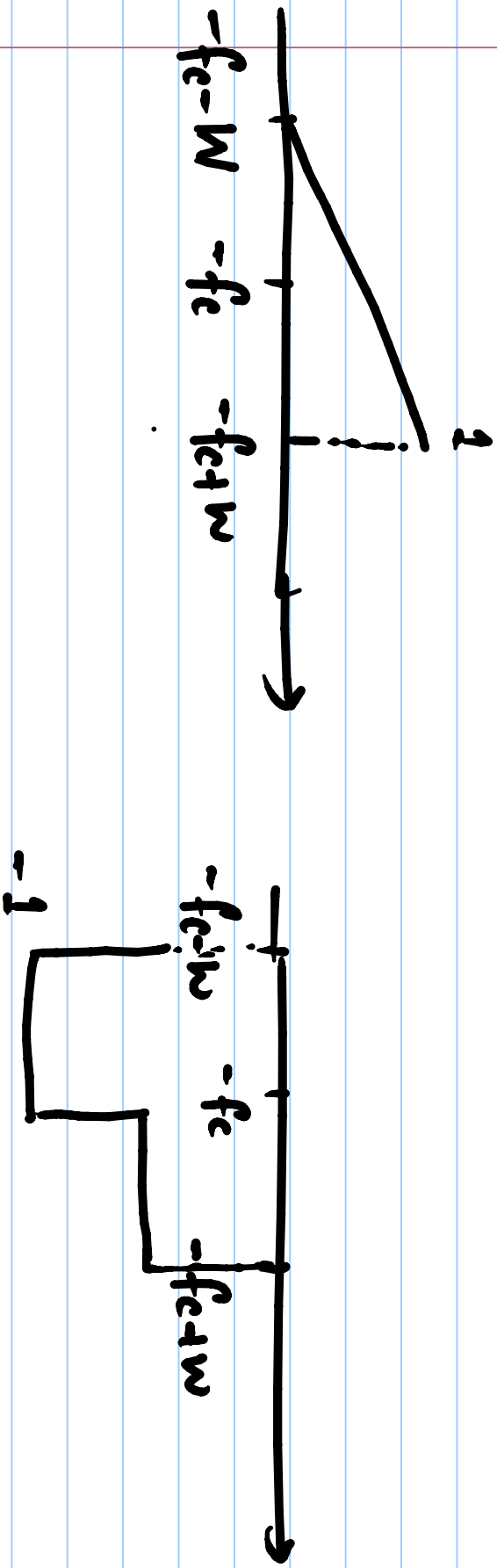
→ flipping and

$$\operatorname{Re}\{c^*(-f)\} = \operatorname{Re}\{c(f)\} \quad \text{conjugation}$$

$$\operatorname{Im}\{c^*(-f)\} = -\operatorname{Im}\{c(f)\}$$

Re $\{c^*(-f)\}$

Im $\{c^*(-f)\}$

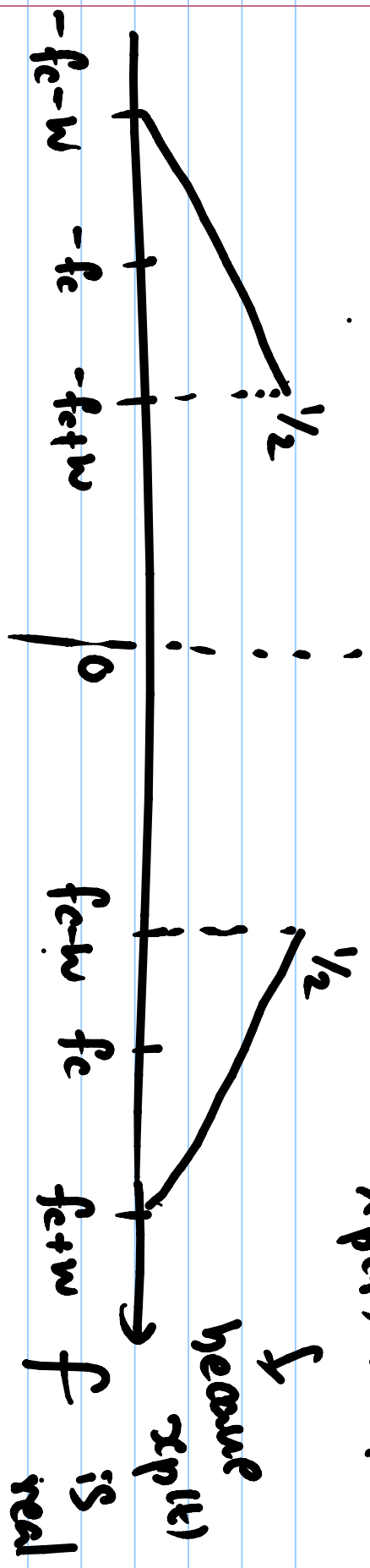


$$X_p(f) = \frac{C(f) + c^*(-f)}{2} \quad .1$$

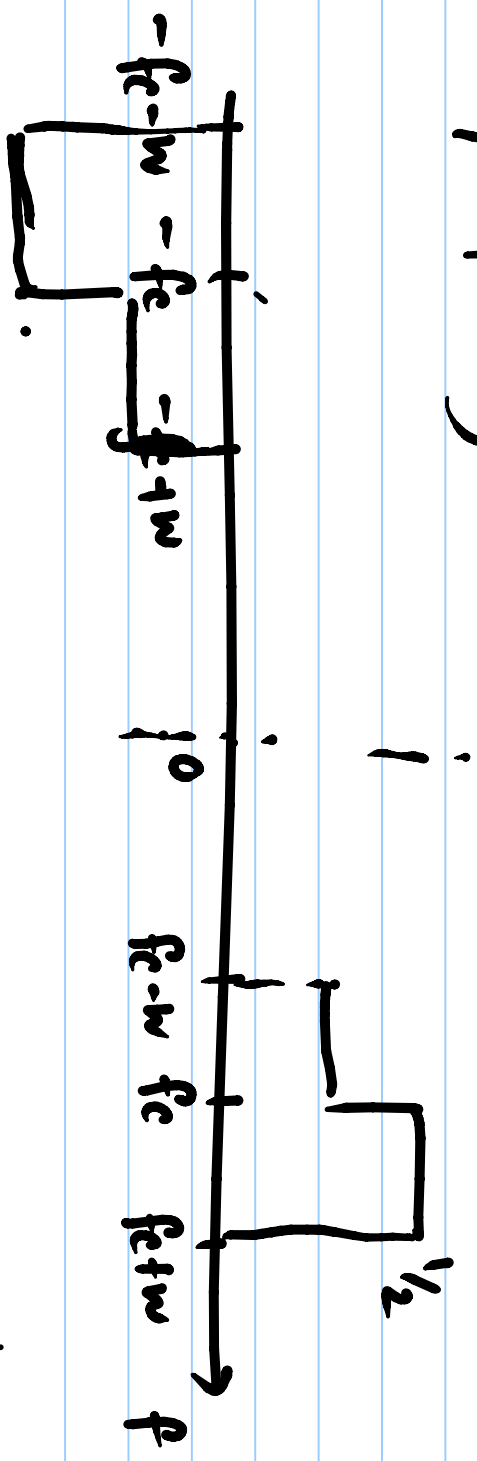
Re {Xp(f)}

Note

$$X_p(f) = X_p^*(-f)$$



Im {Xp(f)}



Notes:

① Shape of Spectrum $X(f)$

f Shape of $X_p(f)$ are same
(positive side)

② Complex base band signals, the
spectrum is not symmetric

Bandwidth = $2W$ (include both
positive and negative freq)

③ Real passband signal $x_p(t)$

has symmetric spectrum

Bandwidth (look at only positive freq)

$$\hat{=} 2W$$

$$\textcircled{4} X_p(f) = \frac{X(f-f_c)}{2} + \frac{X^*(-f-f_c)}{2}$$

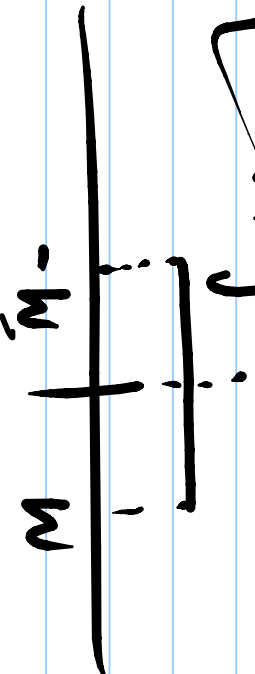
Find $X_c(f)$ & $X_s(f)$ from $X(t)$

$$x_c(t) = x_c(t) + j x_s(t)$$

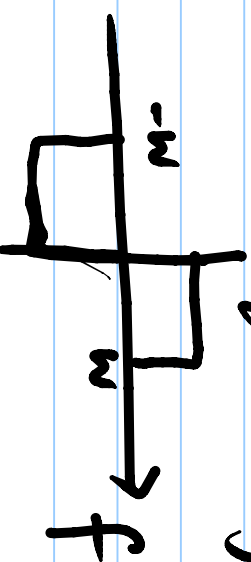
$$x_c(t) = \operatorname{Re}\{x_c(t)\} = \frac{x_c(t) + x_c^*(t)}{2}$$

$$X_c(f) = \frac{1}{2} [X(f) + X^*(-f)]$$

$\operatorname{Re}\{X_c(f)\}$



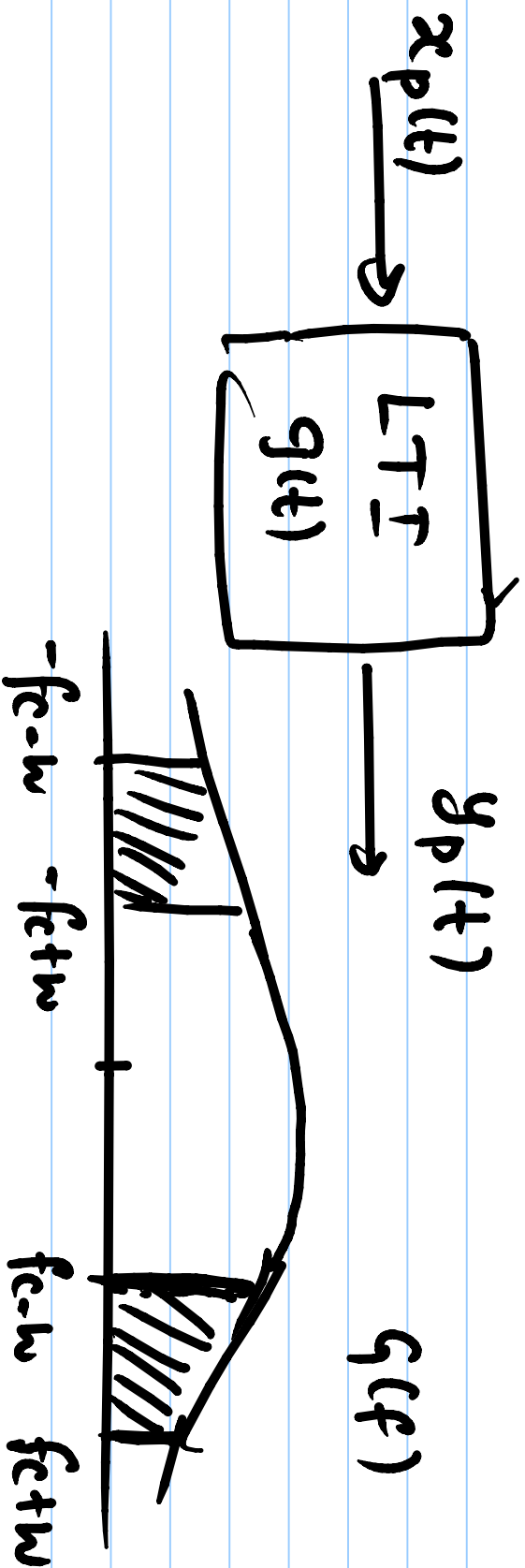
$\operatorname{Im}\{X_c(f)\}$



Similarly

$$X_S(f) = \frac{1}{2j} [X(f) - X^*(-f)]$$

∴



Restricting $G(f)$ to $f_{\pm w}$, $-f_{\pm w}$
bands

We get $H_p(f)$ (and impulse response $h_p(t)$)

Other Equivalences between baseband & Passband

Let $x(t) = x_c(t) + j x_s(t)$

↓
baseband complex envelope

$$x_p(t) = \text{Re} \left\{ x_c(t) e^{j\omega_c t} \right\}$$

$$\begin{aligned} \text{Energy of } x_p(t) &= \int_{-\infty}^{\infty} (x_p(t))^2 dt \\ &= \frac{1}{2} \int_{-\infty}^{\infty} |x_c(t)|^2 dt \end{aligned}$$

$$\text{Let } y_p(t) = \operatorname{Re} \{ y_c(t) e^{j2\pi f_c t} \}$$

$y_c(t) \rightarrow$ complex envelope in baseband

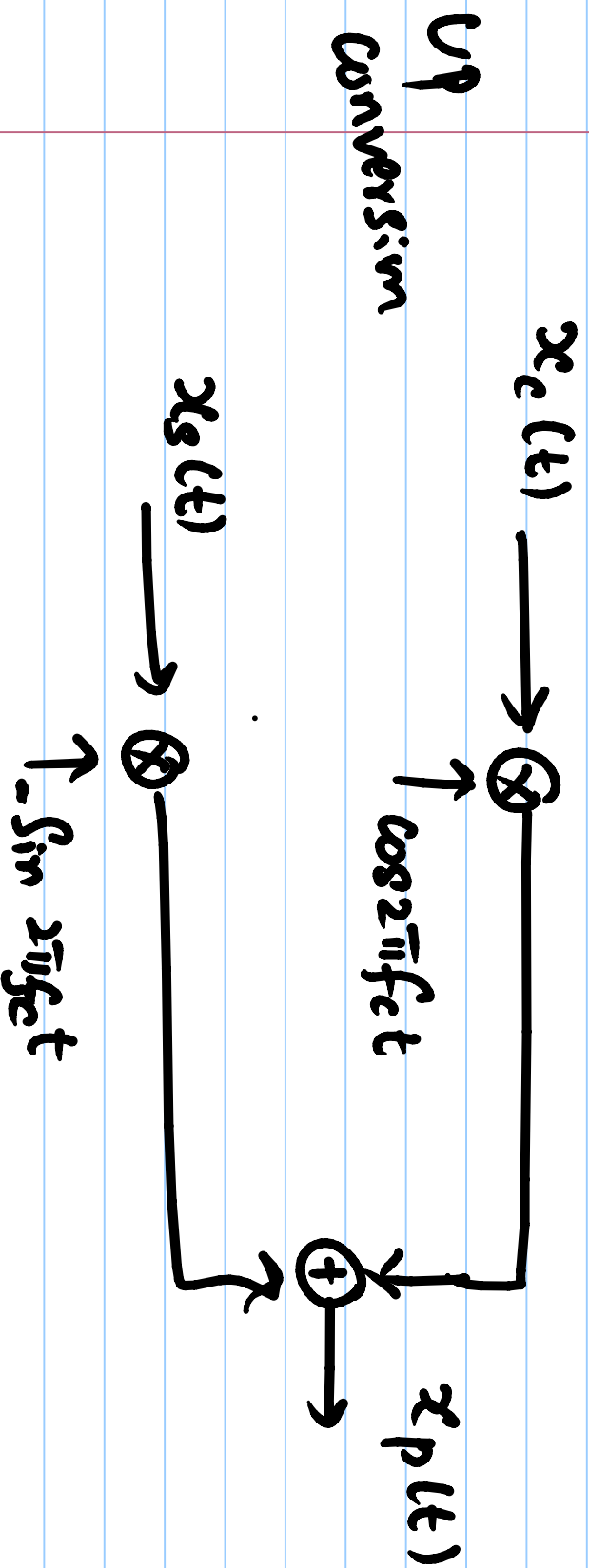
Inner product between $x_p(t)$ & $y_p(t)$

$$\langle x_p(t), y_p(t) \rangle = \int_{-\infty}^{\infty} x_p(t) y_p(t) dt$$

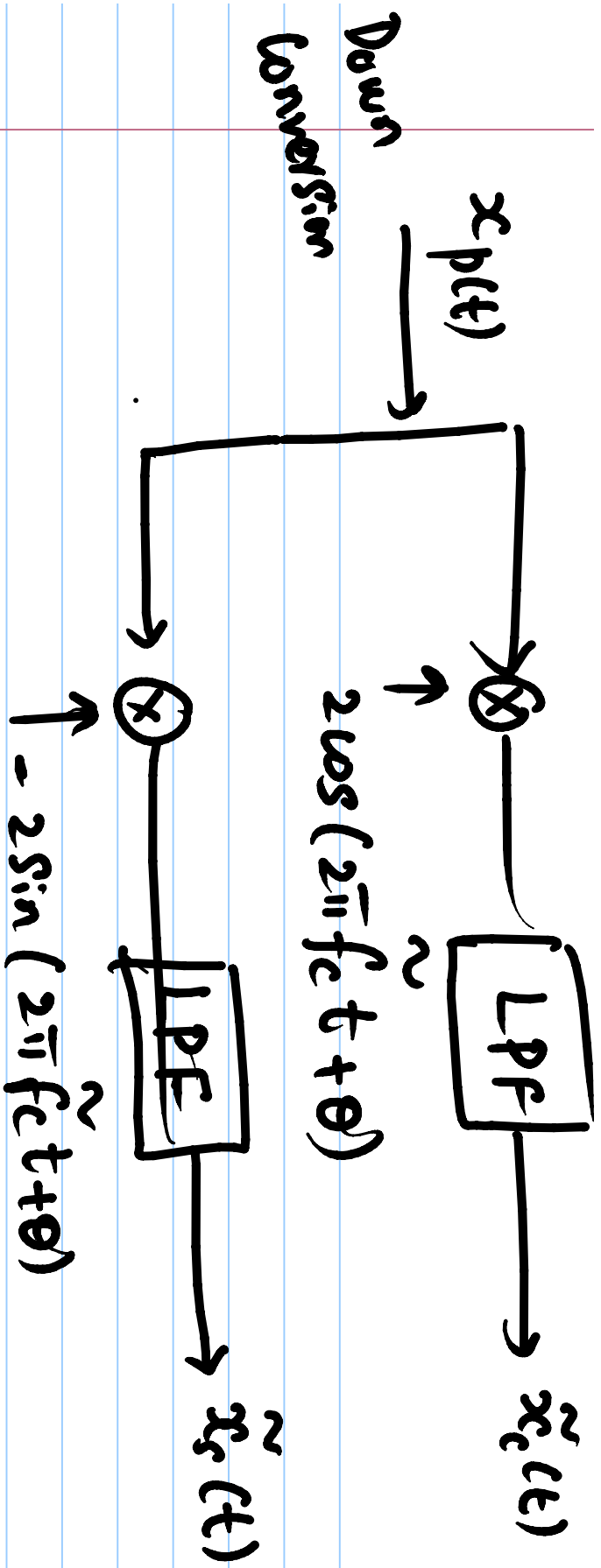
Verify \rightarrow

$$= \frac{1}{2} \operatorname{Re} \left\{ \int_{-\infty}^{\infty} x_c(t) \overset{*}{y_c(t)} dt \right\}$$

Mismatched Down Conversion



Down convert with mismatched
carrier freq f_c & phase θ



How is \tilde{x}_c & \tilde{x}_s related to

x_c & x_s ?

$$x(t) = x_c(t) + j x_s(t)$$

$$\tilde{x}(t) = \tilde{x}_c(t) + j \tilde{x}_s(t)$$

We know

$$x_p(t) = \operatorname{Re} \left\{ x(t) e^{j2\pi f_c t} \right\}$$

We also have

$$x_p(t) = \operatorname{Re} \left\{ \tilde{x}(t) e^{j(2\pi f_c t + \theta)} \right\}$$

It follows that

$$x(t) e^{j2\pi f_c t} = \tilde{x}(t) e^{j(2\pi \tilde{f}_c t + \theta)}$$

$$\tilde{x}(t) = x(t) e^{j(2\pi (f_c - \tilde{f}_c)t - \theta)}$$

$$\phi(t) = 2\pi (f_c - \tilde{f}_c)t - \theta$$

If $f_c = \tilde{f}_c$ then $\phi(t)$ is constant over time

$$\tilde{x}(t) = x(t) e^{j\phi(t)}$$

$$\tilde{x}_c(t) = x_c(t) \cos \phi(t) - x_s(t) \sin \phi(t)$$

$$\tilde{x}_s(t) = x_c(t) \sin \phi(t) + x_s(t) \cos \phi(t)$$

$\tilde{x}_c(t)$ has "interference" from $x_s(t)$

I & Q components interfere with each other due to carrier mismatch,

Our down conversion process
requires strict alignment of
(transmit & receive) carrier frequencies
and phase

This is called coherent down conversion