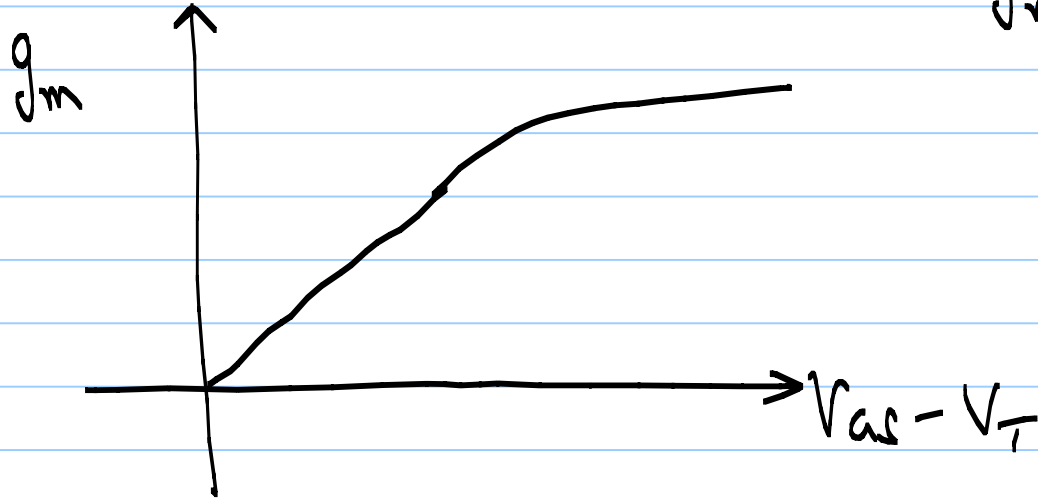


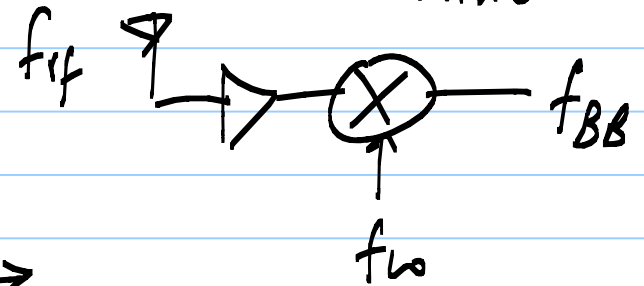
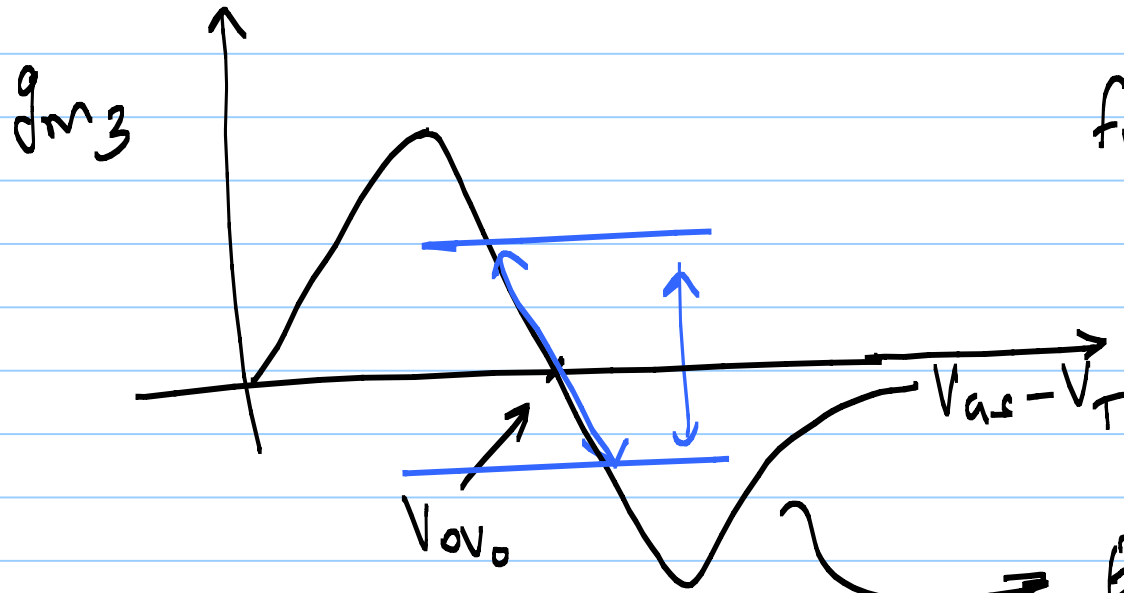
27/2/20

Lec 19

$$g_m = \mu_n C_{ox} \left(\frac{W}{L}\right) (V_{GS} - V_T)$$



Zero-IF
11P2: mixers
or
direct
conversion
mixers

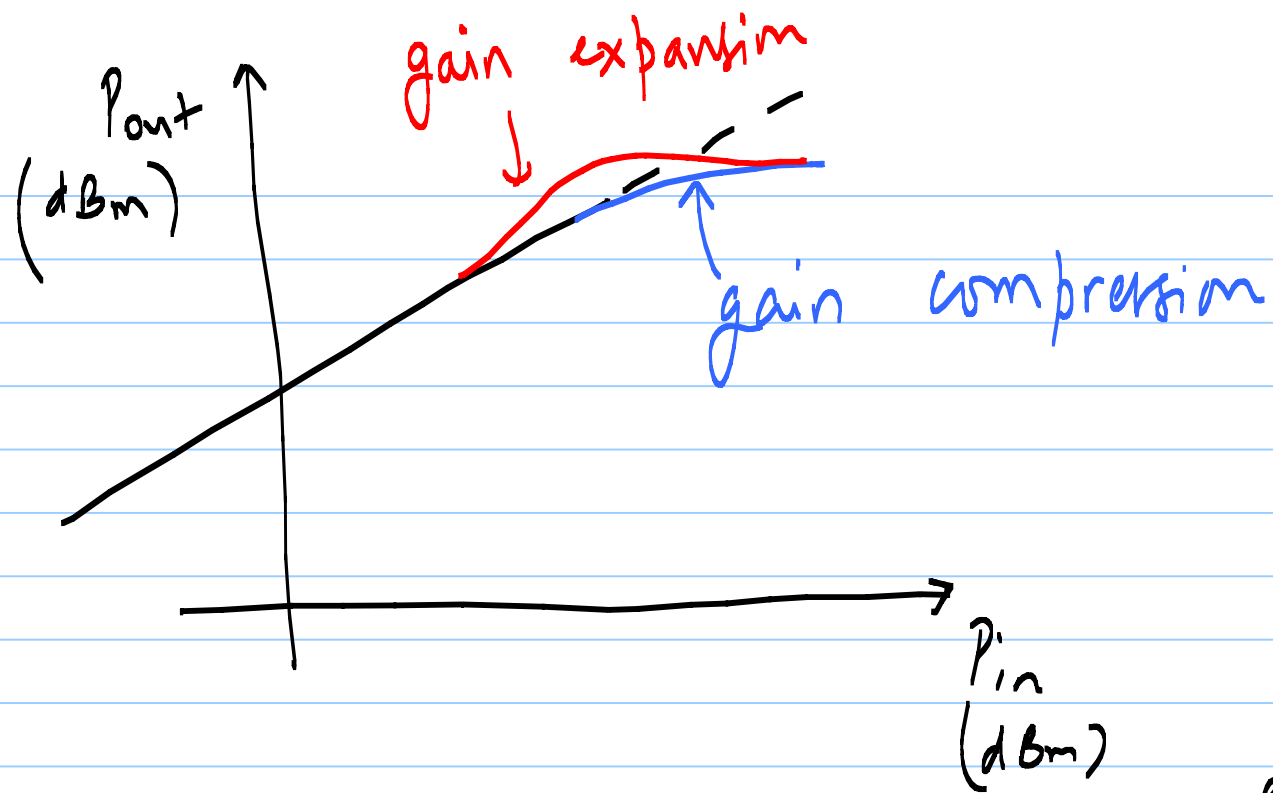


* If we design LNA so that the amplifying device has $(V_{as} - V_T) = V_{ov0}$ you will achieve very high $1/f_3$

* g_{m3} slope around V_{ov0} is high
 \Rightarrow ensure that $1/f_3$ is met over PVT variations

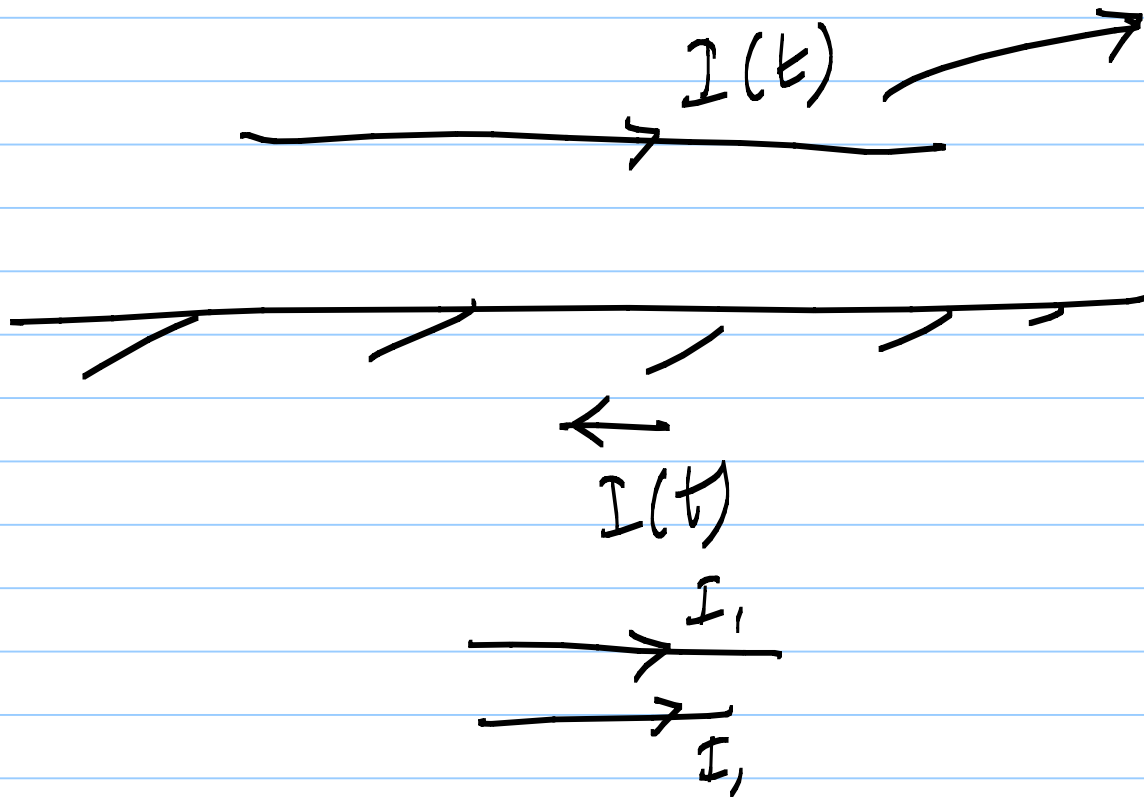
* Otherwise, operate at very high $V_{as} - V_T$ where $|g_{m3}|$ is low & has small slope

* g_{m3} has +ve or -ve signs depending on $(V_{as} - V_T) > V_{ov0}$ or $< V_{ov0}$
 \Rightarrow you can achieve gain expansion or gain compression

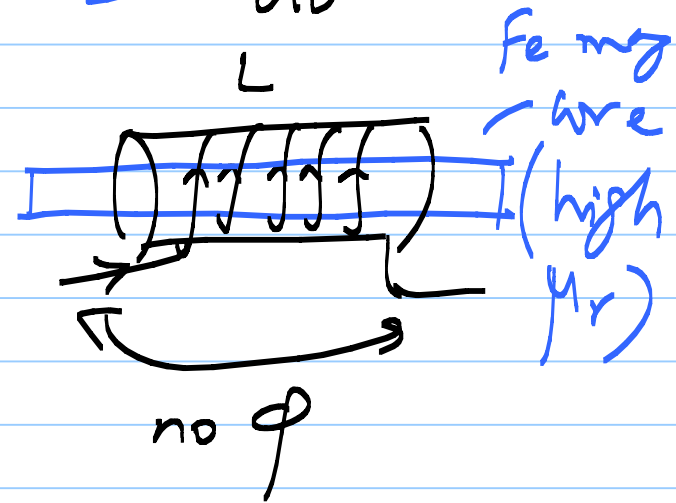


fundamental term: $\alpha_1 + \frac{3\alpha_3 A^2}{4}$ — gain compression at large $V_{GS} - V_T$
 — gain expansion at small $V_{GS} - V_T$

Spiral Inductors

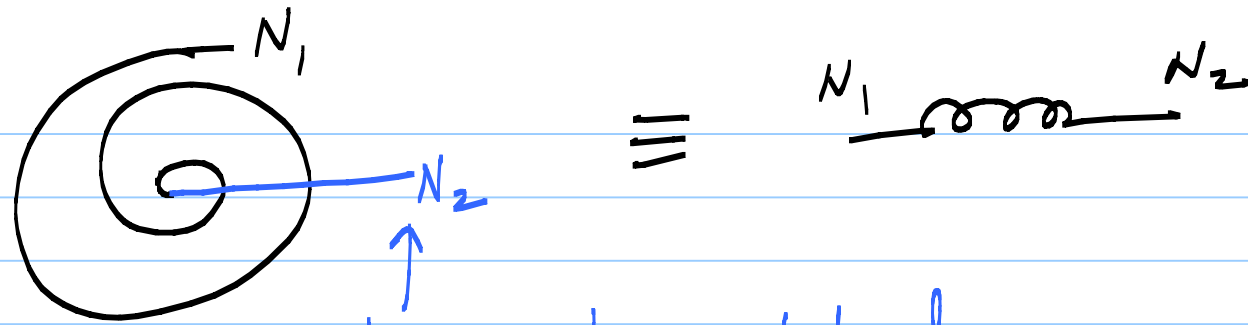


$$V = L \frac{dI(t)}{dt}$$



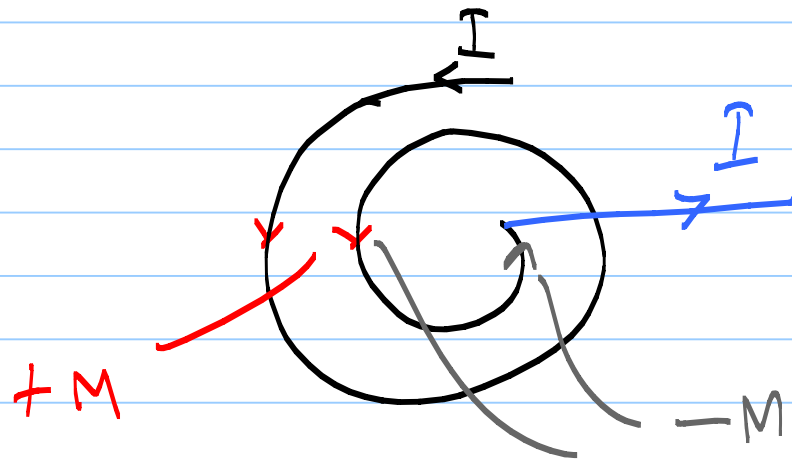
On silicon

- * Only air cored inductors
- * Only planar (or combination of planar) structures

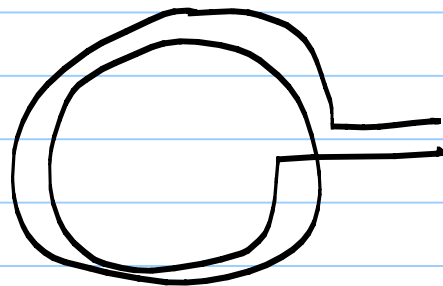


different metal layer

* If spiral has total wire length l ,
ensure that $l \ll \lambda$



\Rightarrow build inductors with
large inner diameters



nH inductors require
several 100s of μm to mm of
length

* Multilayer spirals are also possible
⇒ choose current directions to produce
additive M