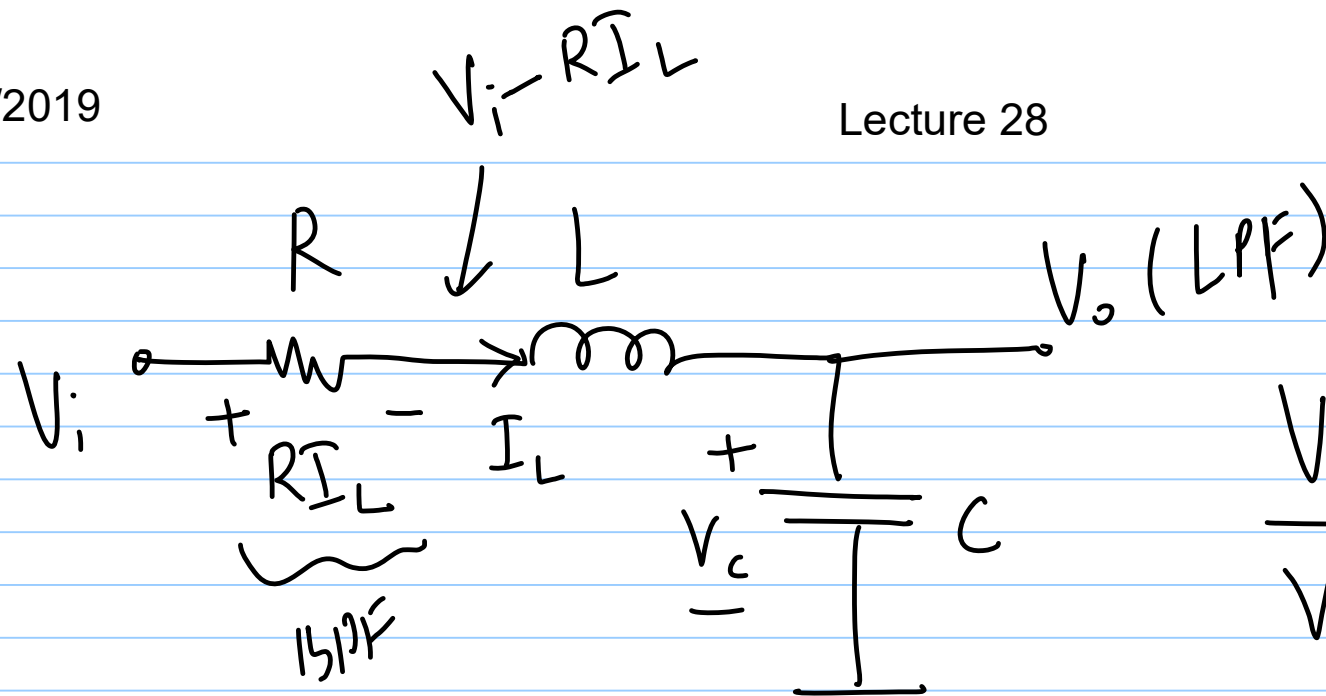


16/03/2019

Lecture 28



$$\frac{V_o(s)}{V_i(s)} = \frac{1}{1 + sCR + s^2LC}$$

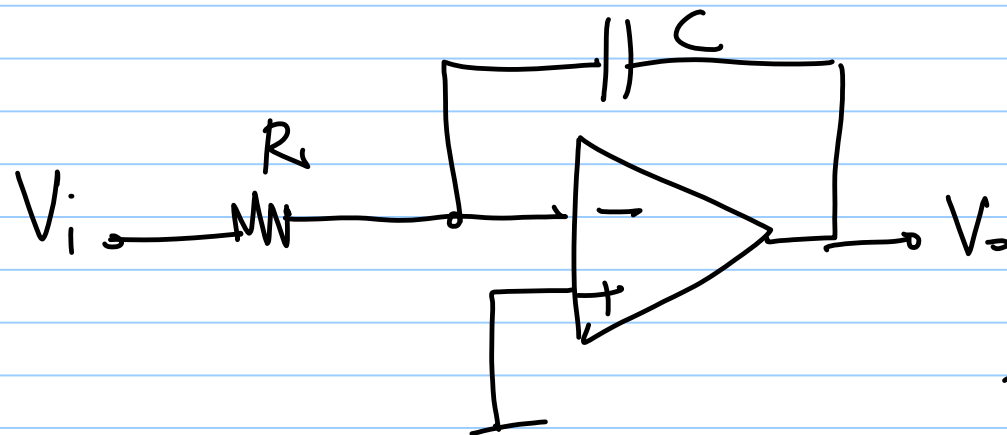
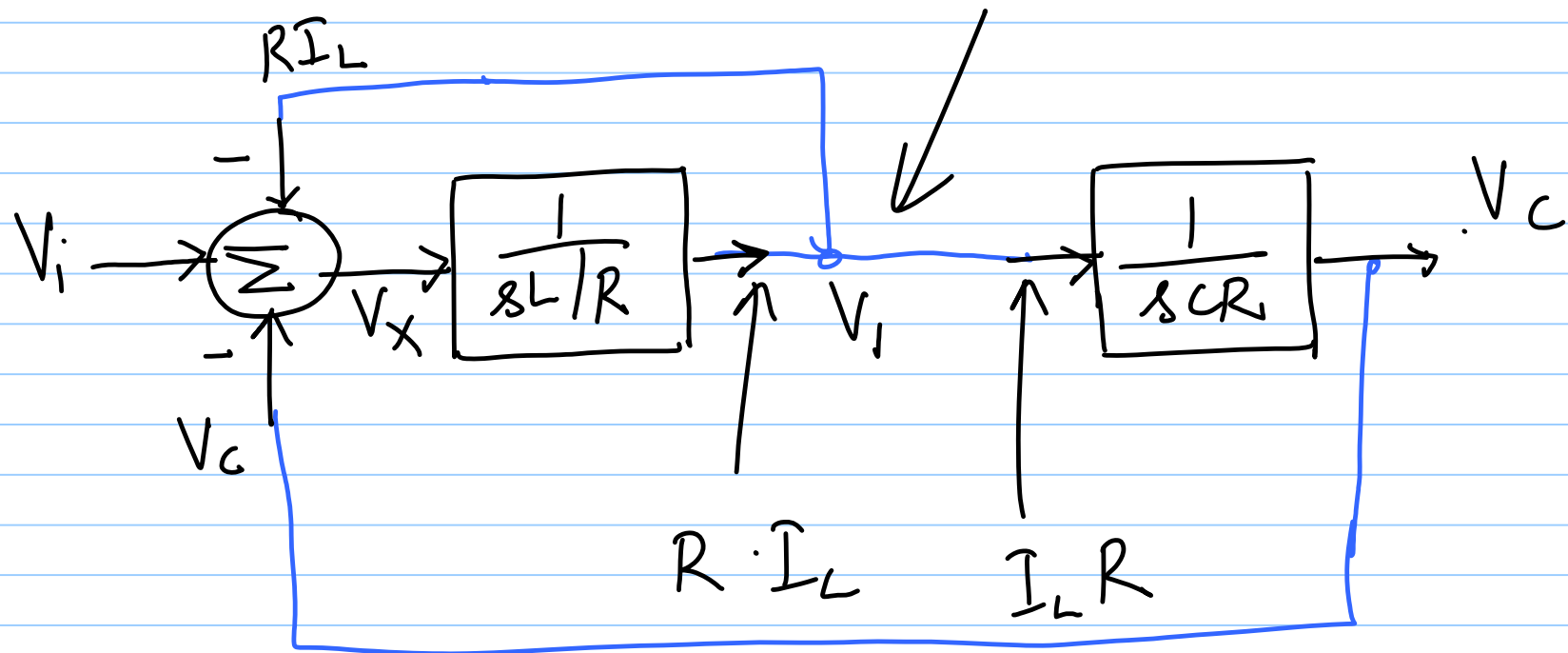
State variables of a network;

- 1) currents through inductors
- 2) voltages across the capacitors

$$V_c = \frac{I_c}{sC} = \frac{\cancel{V_i - V_c}}{\cancel{sCR}} \quad \frac{I_L}{sC} = \frac{I_L \cdot R}{sCR}$$

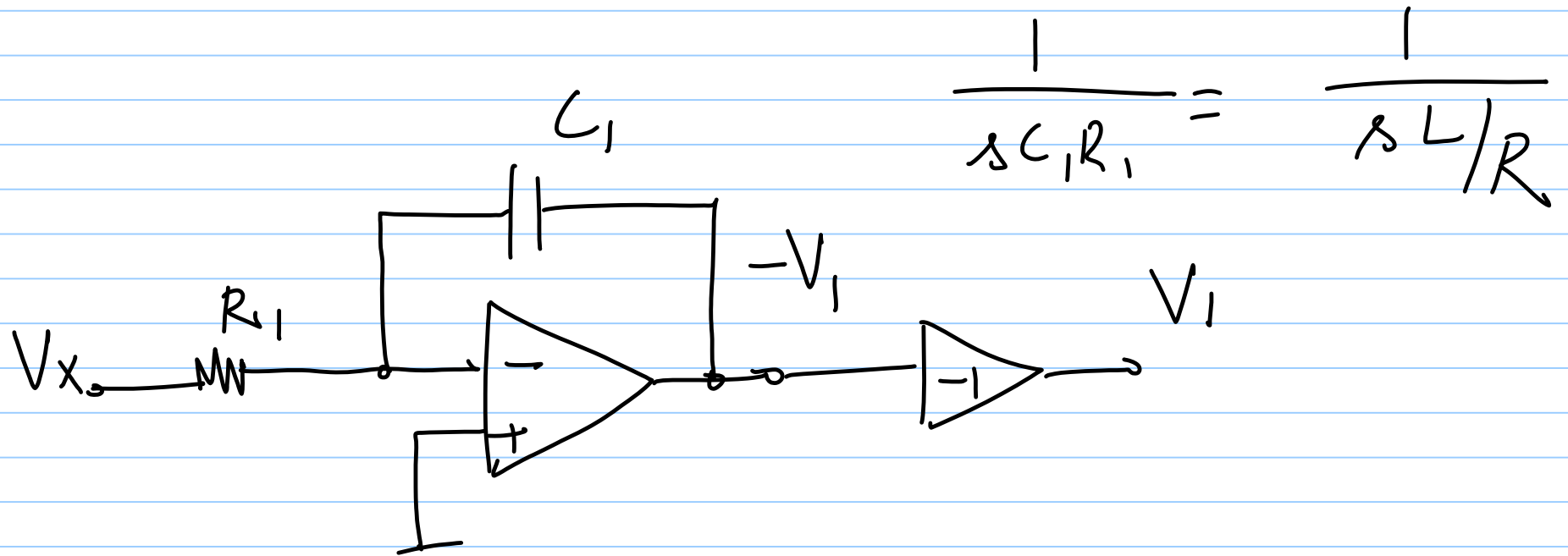
$$I_L = \frac{V_i - V_c}{R + sL} \quad \text{--- (1)} \quad \frac{(\quad)}{s(\quad)}$$

$$RI_L = \frac{V_i - RI_L - V_c}{sL/R} \quad \text{--- (2)}$$



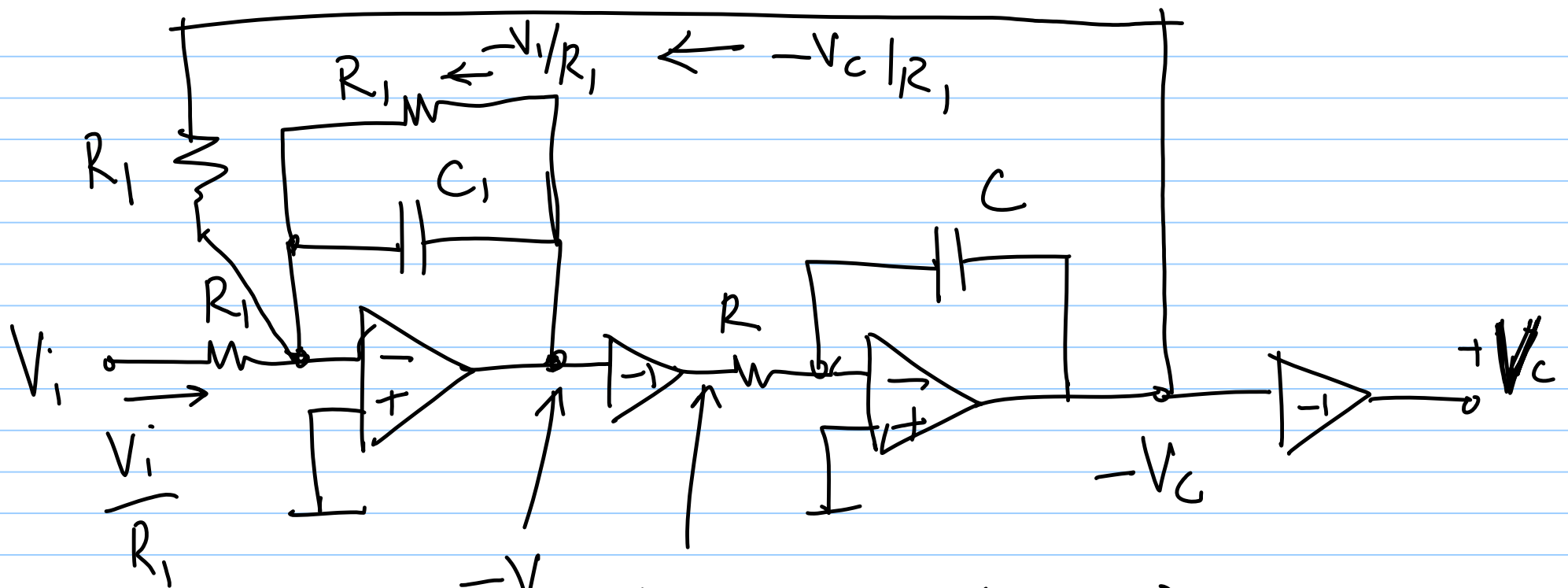
Integrator

$$\frac{V_o}{V_i} = \frac{-1}{sCR}$$



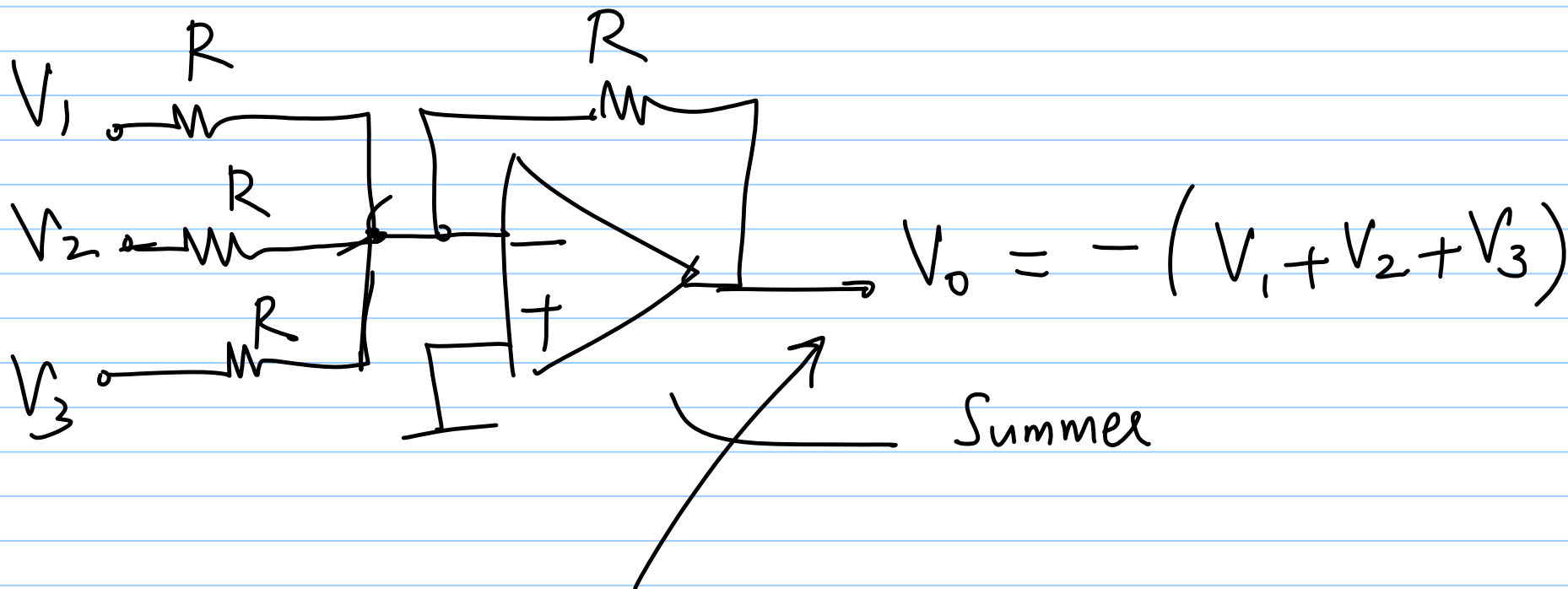
$$\frac{1}{sC_1R_1} = \frac{1}{sL/R}$$

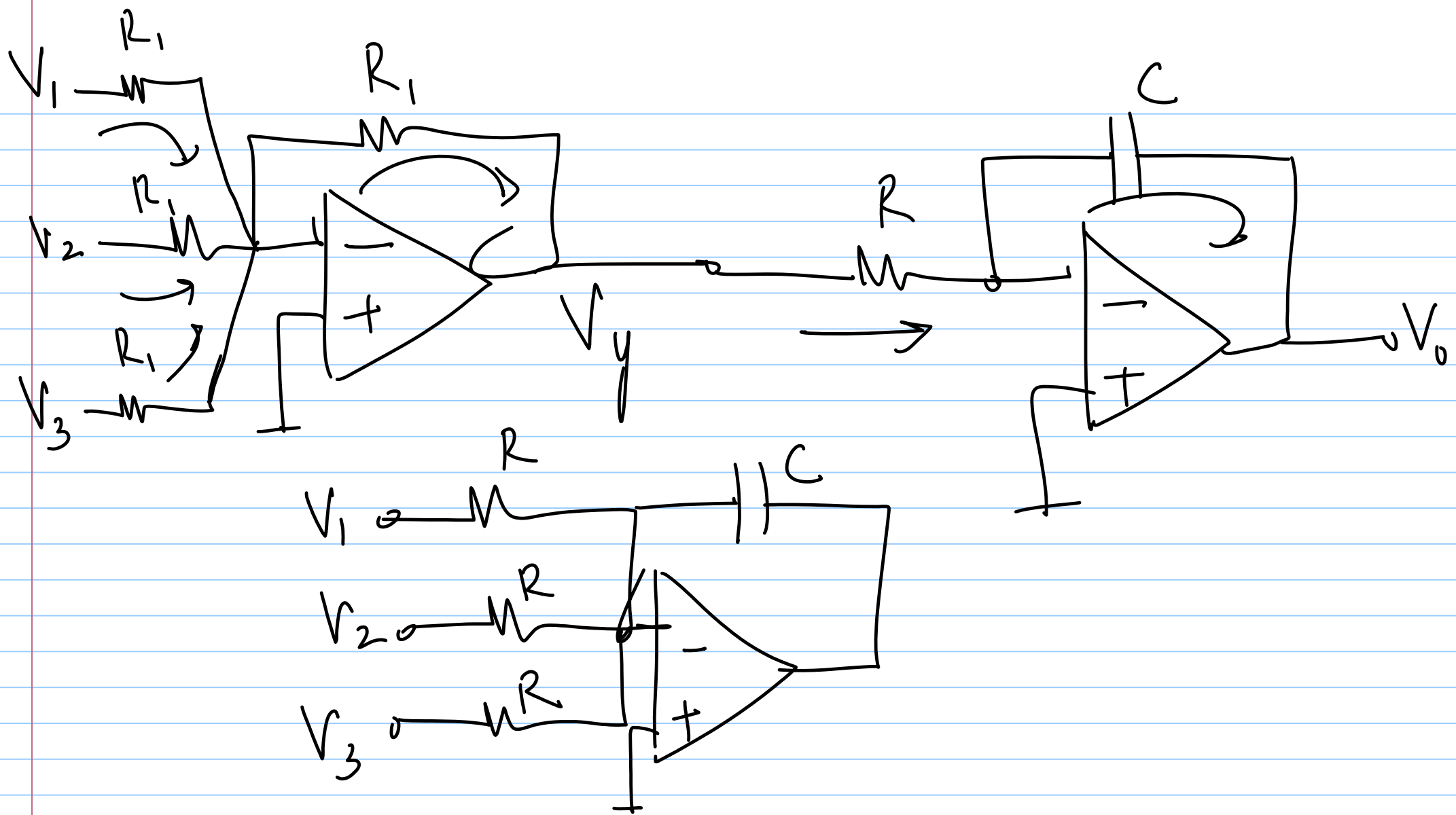
$$R_1C_1 = \frac{L}{R}$$



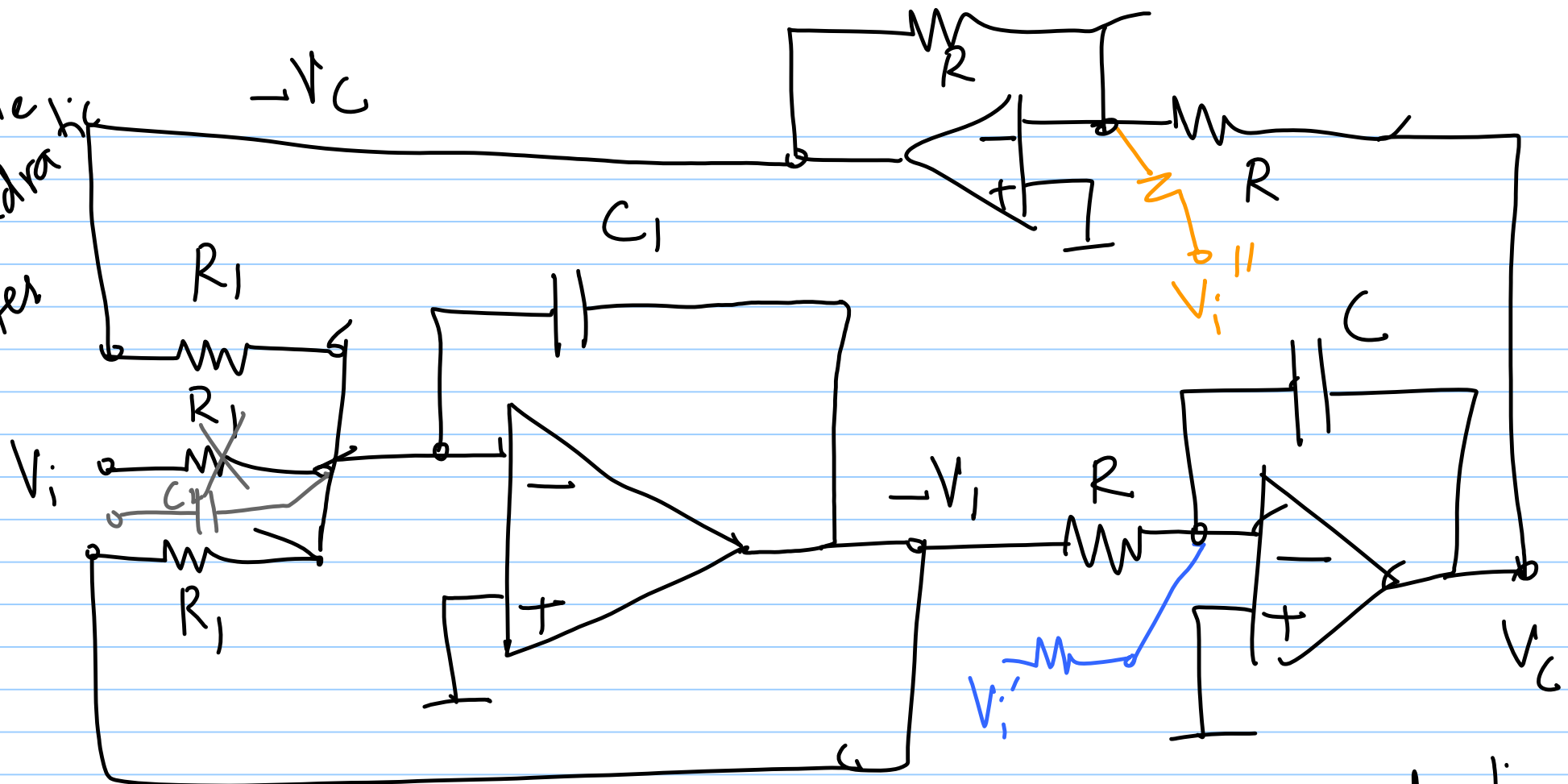
$$-V_1 + V_1 \rightsquigarrow (I_L \cdot R)$$

$$\left(\frac{V_i}{R_1} - \frac{V_c}{R_1} - \frac{V_1}{R_1} \right) \times \frac{-1}{sC_1} = -V_1$$





State
Variable
Biquadratic
Filter



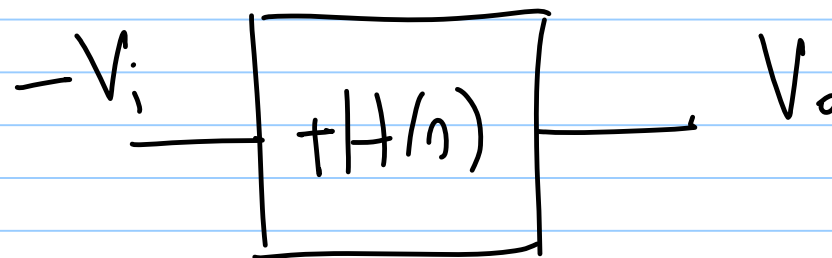
Tow-
Thomas
Biquad
filter

$$V_c = \frac{V_1}{sCR} = - \left(\frac{-V_1}{sCR} \right)$$

Biquadratic
filter $\frac{N_2(s)}{D_2(s)}$

$$-V_i = - \left[\frac{V_i - V_i - V_c}{s C_1 R_1} \right] \quad \pm H(\omega)$$

$$= \frac{-1}{s C_1 R_1} \left[+V_i - V_i - V_c \right]$$



$$\frac{V_c(s)}{V_i(s)} = \frac{1}{1 + sCR + s^2 LC} \quad \leftarrow \text{Lowpass filter}$$

$$= \frac{1}{1 + sCR + s^2 C \cdot C_1 R R_1}$$

$$\frac{L}{R} = R_1 C_1 \Rightarrow L = R R_1 C_1$$

$$\frac{V_1(s)}{V_i(s)} = \frac{V_c}{V_i} \cdot sCR = \frac{sCR}{1 + sCR + s^2 LC} \quad \leftarrow \text{Bandpass response}$$

$$\left| \frac{V_1}{V_i} \right|$$

BPF

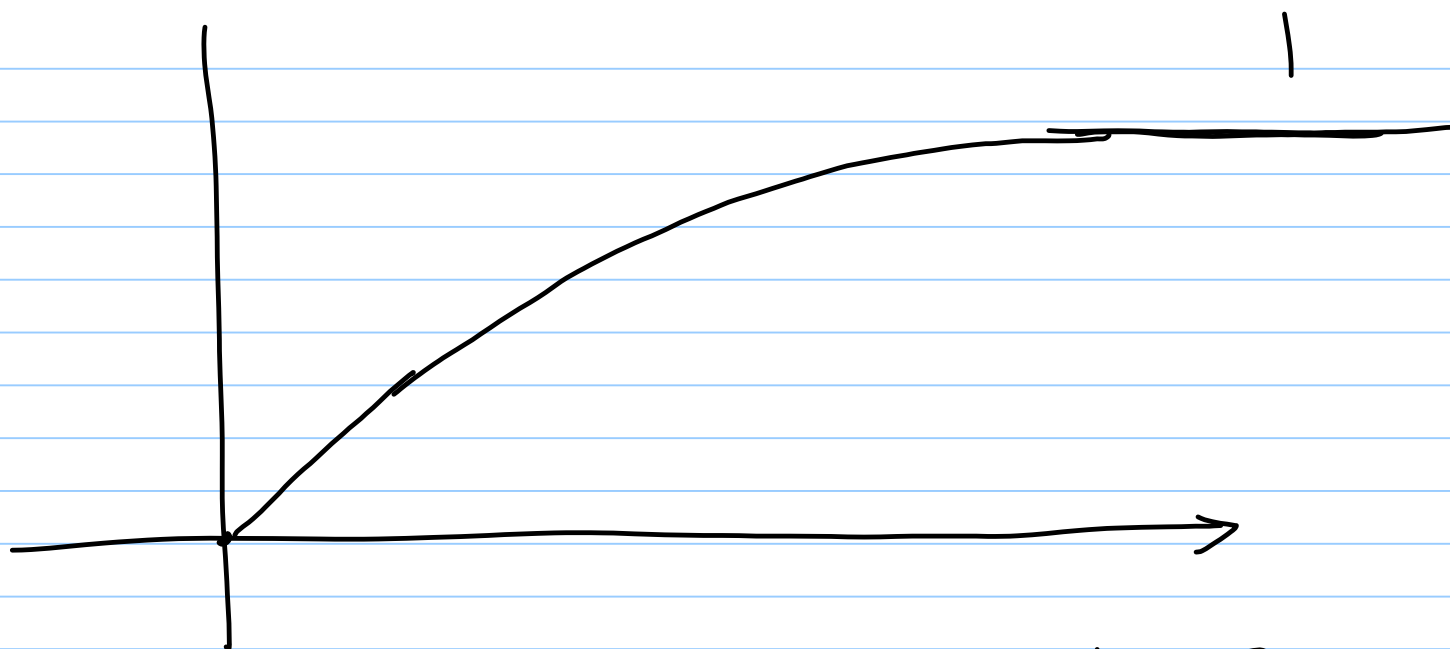
$$\frac{V_c(s)}{I_i(s)}$$

New V_i (with C_2)

$$\frac{V_c(s)}{\cancel{\left| \frac{V_i(s)}{R_1} \right|}} = \frac{s C_2 R_1}{1 + s C R + s^2 L C}$$

$$V_1/V_i(\omega) = \frac{s^2 C_2 R_1 C R}{1 + s C R + s^2 L C}$$

$$\left| \frac{V_1}{V_i} \right|$$



$$C_2 = C_1$$

H PF

