

4-9-13

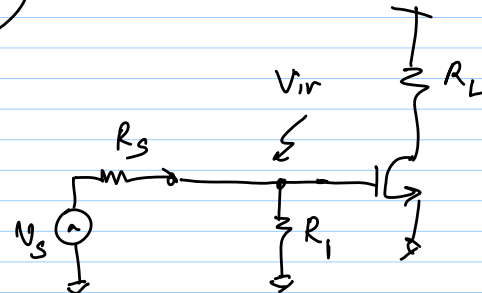
Lec 15

LNA topologies

- * NF of LNA adds to overall NF
- * gain - neutralise noise of succeeding blocks
 - NF - divided by A_{v1}^2 (available voltage gain)
 - $11\beta_3$ - divide by $\alpha_1^2 = (2A_{v1})^2$
- * @ Input - long PCB trace
 - BSF between Antenna & LNA

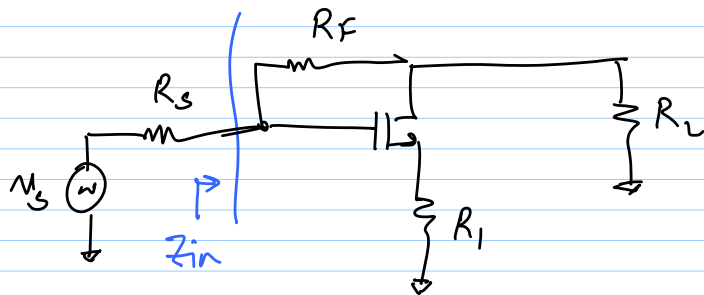
- match to 50 Ω @ input

1) Resistor match with CS stage



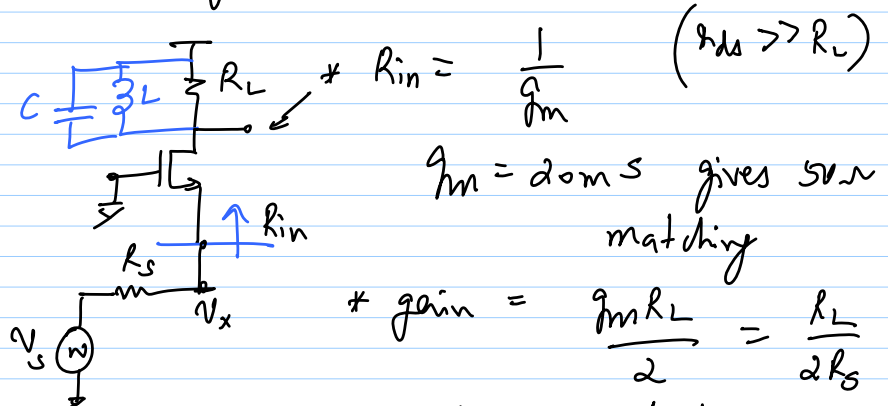
- * $R_1 = R_s$
- * broadband match
- * Attenuated signal
 $V_{in} = V_s/2$
- * R_1 - thermal noise
- * $F = 2 + \frac{4\gamma}{\alpha} \cdot \frac{1}{g_m R_s}$
- NF_{min} = 3dB

2) Shunt-series Amplifier



- * No attenuation @ input
Set $Re(Z_{in}) = R_s$
- * $F > F_{min}$

3) Common-gate amplifier



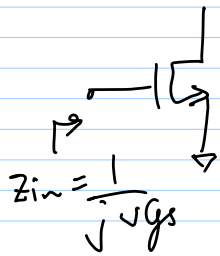
- * $R_{in} = \frac{1}{g_m}$ ($r_{ds} \gg R_L$)
- $g_m = \omega C_{gs}$ gives 50 Ω matching
- * gain = $\frac{g_m R_L}{2} = \frac{R_L}{2 R_s}$
- * $F = 1 + \gamma$ $\leftarrow$ (H.W) neglecting R_L noise
- * $F = 1 + \frac{\gamma}{\alpha} + \frac{4 R_s}{R_L}$

$$\gamma = 0.67 \Rightarrow F_{min} = 1.67 \approx 2.2 \text{ dB}$$

$$R_{in} = \frac{R_L + r_{ds}}{1 + g_m r_{ds}} \approx \frac{1}{g_m} \text{ if } R_L \ll r_{ds}$$

* Cascode CG — allows independent input matching

4) CS stage (narrowband)



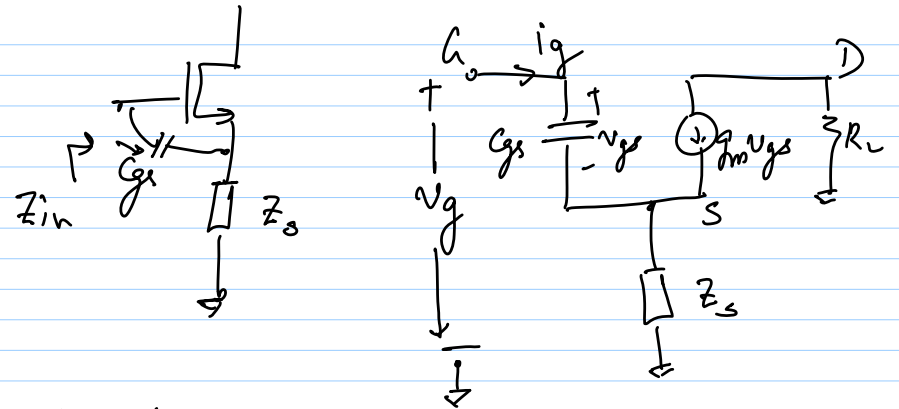
$$\Rightarrow v_g = i_g Z_s + (1 + g_m Z_s) \cdot \frac{i_g}{s C_{gs}}$$

$$Z_{in} = \frac{v_g}{i_g} = Z_s + \frac{1}{s C_{gs}} + \frac{g_m Z_s}{s C_{gs}}$$

a) $Z_s = R_o$

$$Z_{in} = R_o + \frac{1 + g_m R_o}{s C_{gs}} \Bigg\} C_x$$

$$Z_{in} = \frac{C_{gs}}{1 + g_m R_o} \approx \frac{1}{\omega_T R_s}$$



$$\frac{v_g - v_{gs}}{Z_s} = g_m v_{gs} + i_g$$

$$\Rightarrow v_g = i_g Z_s + (1 + g_m Z_s) v_{gs}$$

$$v_{gs} = i_g / s C_{gs}$$