

Case-1: Load Transient is limited by bandwidth.

Using 1st order approximation.

time constant (in closed loop)

$$\tau = \frac{1}{\omega_{cpl}} = \frac{1}{2\pi f_{cpl}}$$



$$I = C \frac{dV_o}{dt}$$

$$dt = \tau, I = I_{load}$$

$$\Delta V_o = dV_o = \frac{I}{C} \times \tau = \frac{I_{load}}{2\pi f_{cpl} C}$$

$$f_{cpl} = \frac{F_{cpl}}{10} = 1 \text{ MHz}$$

$$C = 0.34 \mu\text{F}, I_{load} = 1 \text{ A}$$

$$\Delta V_o = \frac{1}{2\pi (10^6)(0.34 \times 10^{-6})} = \frac{1000 \text{ mV}}{2} \approx 500 \text{ mV}$$

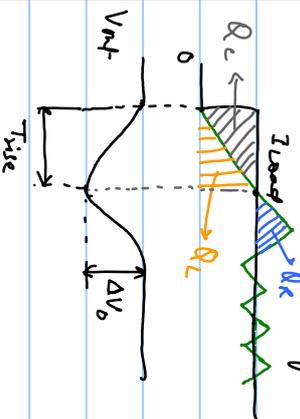
spec for $\Delta V_0 < 5\%$ of V_{out}

$$\Delta V_0 = 5\% \cdot 1.2V = 60mV$$

C required will be approx. 10x more to meet $\Delta V_0 < 60mV$

$$C = 10 \times 0.34 \mu F = 3.4 \mu F$$

Case-2: Load transient is limited by inductor slew rate
(BW is very high \rightarrow non-linear capacitor)



$R_L \rightarrow$ Voltage supplied by the capacitor before $I_L = I_{Load}$

$R_L \rightarrow$ " " " " Inductor. " " "

$R_L \rightarrow$ Recovery voltage to bring V_{out} back to final value (supplied by the inductor)

$Q_c =$ Area under the triangle.

$$= \frac{1}{2} T_{rise} \times I_{load} \quad \text{--- (1)}$$

$$\Delta I_L = \frac{V_{dd} - V_0}{L} \times T_{rise} = I_{load}$$

$$T_{rise} = \frac{I_{load} \times L}{V_{dd} - V_0} \quad \text{--- (2)}$$

Substitute in (1)

$$Q_c = \frac{1}{2} I_{load}^2 \times \frac{L}{V_{dd} - V_0}$$

$$Q_c = CV = C \Delta V_0$$

$$\Delta V_0 = \frac{Q_c}{C} = \frac{1}{2} \frac{I_{load}^2}{(V_{dd} - V_0)} \left(\frac{L}{C} \right)$$

$I_{load} = 1A$, $L = 165\mu H$, $V_{dd} = 1.8V$, $V_o = 1.2V$

$$\Delta V_o = \frac{1}{2} \frac{1}{0.6} \times \frac{0.165 \times 10^{-6} C}{0.34 \times 10^{-8} s} \approx 400mV$$

$C = 0.34\mu F$ is not sufficient to meet $\Delta V_o < 60mV$ spec.

$$L = 165\mu H$$

$$\Delta I_L (max) = \frac{V_{dd} D(1-D)}{L} \times T_{sw} \quad \left| \begin{array}{l} \text{at } D=0.5 \end{array} \right.$$

$$= \frac{1.8 \times 0.25}{165 \times 10^{-6}} \times 100 \times 10^{-9} \approx 0.27A$$

