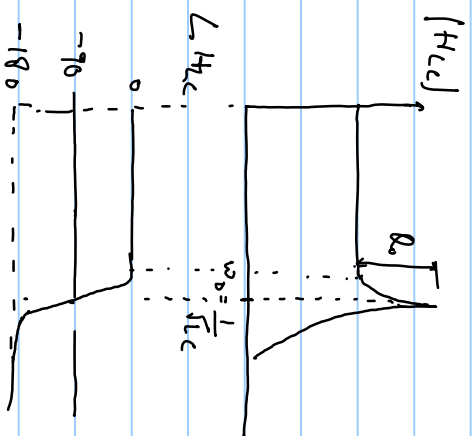


$$\beta_0 = \frac{\omega_0}{\frac{R_{load} C}{L} + \frac{1}{R_{load} C}} = \frac{1/\sqrt{LC}}{\frac{R_{load} C + L/R_{load}}{LC}}$$

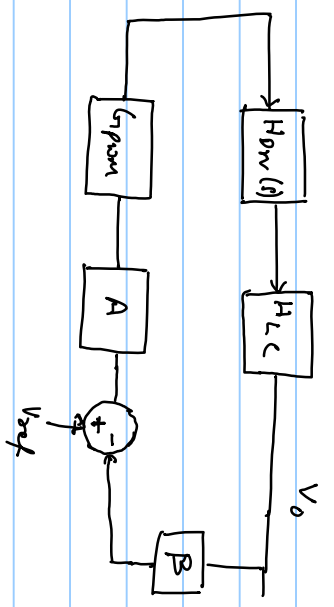
$$\beta_0 = \frac{\sqrt{LC}}{R_{load} C + L/R_{load}}$$



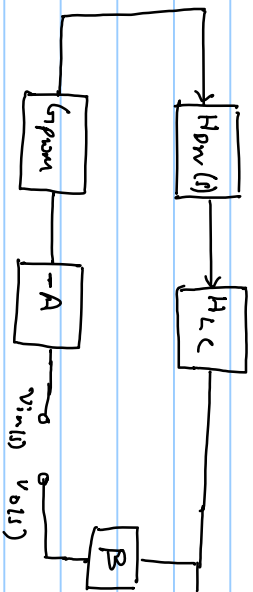
Qo \rightarrow max when $R_{load} = \infty$ (no load)

$$Qo \cdot max = \frac{\sqrt{L/C}}{R_{load} C} = \frac{1}{R_{load}} \sqrt{\frac{L}{C}}$$

Small Signal Model of a buck converter

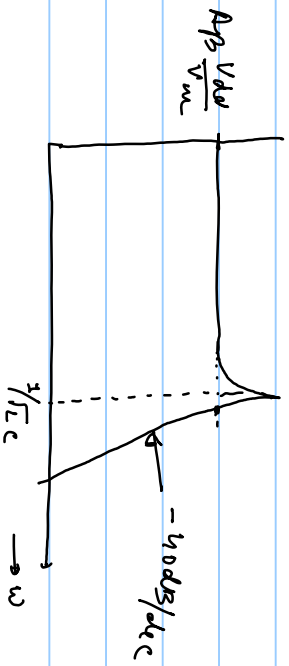


Loop Gain Analysis



$$\frac{V_o(s)}{V_{in}(s)} = L_G(s) = -A \beta G_{pm}(s) H_{pc}(s) H_{fc}(s)$$

$$|L_G(\omega)| = A \beta \left(\frac{1}{V_m} \right) (V_{dd}) \left(\frac{1/\omega_c}{s^2 + s \left(\frac{R_{out}}{L} + \frac{1}{R_{load} C} \right) + \frac{1}{LC}} \right)$$



$$\left(\frac{\omega_0}{\omega_{ngb}}\right)^2 \times \frac{A_p V_{dd}}{V_m} = 1$$

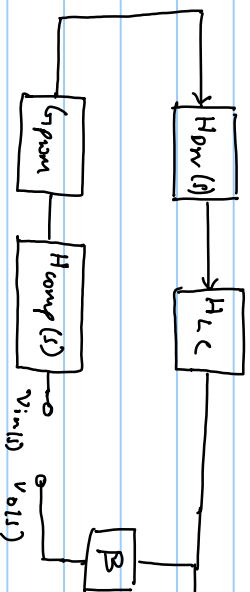
$$\omega_{ngb}^2 = \omega_0^2 \frac{A_p V_{dd}}{V_m}$$

$$\omega_{ngb} = \omega_0 \sqrt{\frac{A_p V_{dd}}{V_m}}$$

$$= \sqrt{\frac{A_p V_{dd}}{V_m L C}}$$

$\omega_{ngb} \gg \omega_0 \Rightarrow$ system is inherently unstable

We need to stabilize the system.



$$\frac{V_o(s)}{V_{in}(s)} = L_{comp}(s) = \beta H_{comp}(s) H_{DRV}(s) H_C(s)$$

$$= \beta H_{comp}(s) \left(\frac{1}{V_m} \right) (V_{dd}) \left(\frac{1}{s^2 + s \left(\frac{R_{on}}{L} + \frac{1}{R_{oad}C} \right) + \frac{1}{LC}} \right)$$

Assume

$$H_{comp}(s) = \frac{K}{s} = \frac{1}{H_C(s)}$$

$H_C(s)$ will cancel out

$$L_{comp}(s) = \beta \frac{V_{dd}}{V_m} \frac{K}{s} \Rightarrow \text{first order system}$$

stable

U.G.B. can be controlled by K

We can cancel complex poles due to LC by introducing complex zeros in $H_{comp}(s)$ at ω_0 .

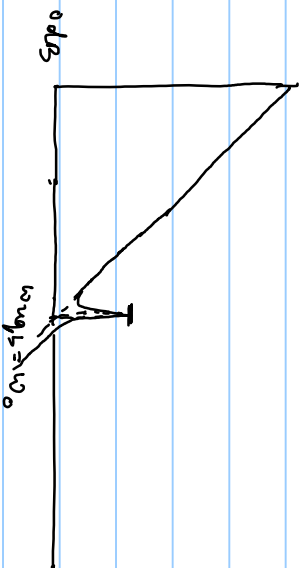
However, we can't practically implement complex zeros with $\omega_0 = \frac{1}{\sqrt{LC}}$ \rightarrow Practically this stability method is not feasible.

Lowest root pole compensation

We use integral or type-I compensation.

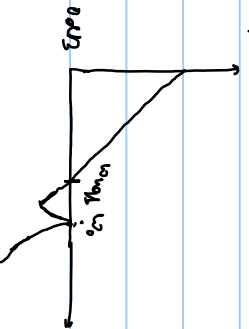
$$H_{comp}(s) = \frac{K_i}{s}$$

and put ω_0 outside ω_{ng}



Gain at ω_{ng} is > 0 dB & PM $\approx 0 \Rightarrow$ unstable.

$$\omega_{ng} = \frac{\omega_0}{R_0} \quad |L(s)|$$



unstable, because
gain > 0 dB at ω_0 (gain margin $= 0$ dB)

$$\omega_{\text{cgs}} < \frac{\omega_0}{D_0}$$

for -20dB gain margin

$$\omega_{\text{cgs}} = \frac{\omega_0}{10 D_0}$$

$$\frac{V_o(s)}{V_{in}(s)} = L_{\text{comp}}(s) = \beta H_{\text{comp}}(s) H_{\text{drv}}(s) H_z(s)$$

$$= \beta \frac{k_i}{s} \frac{V_{dd}}{V_{in}} H_z(s)$$

$$\beta \frac{V_{dd}}{V_{in}} = K_{\text{uo}}$$

$$L_{\text{comp}}(s) = K_{\text{uo}} \frac{k_i}{s} H_z(s)$$

$$K_{\text{uo}} k_i = \omega_{\text{cgs}} = \frac{\omega_0}{10 D_0}$$

$$k_i = \frac{\omega_0}{K_{\text{uo}} 10 D_0} = \frac{1}{10 K_{\text{uo}}} \left(\frac{R_{\text{uo}}}{1} + \frac{1}{R_{\text{oad}}} \right)$$