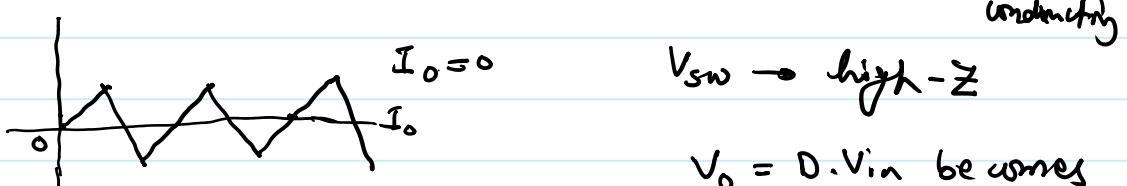
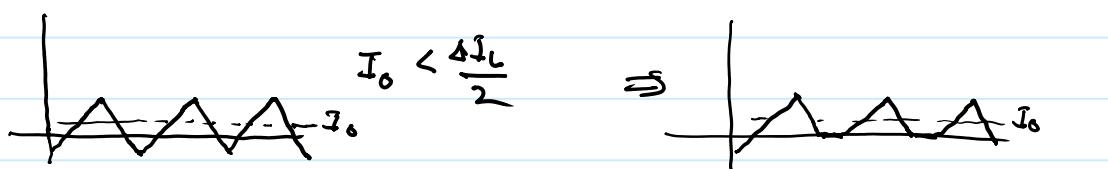
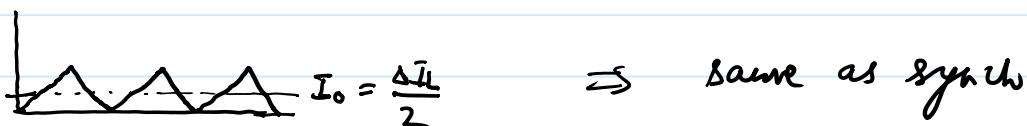
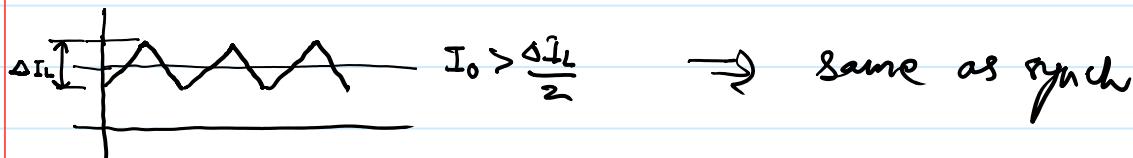
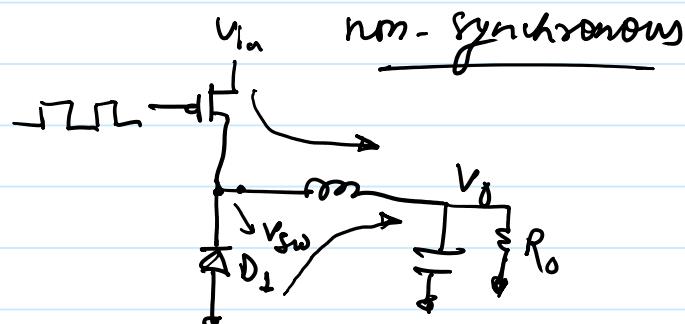
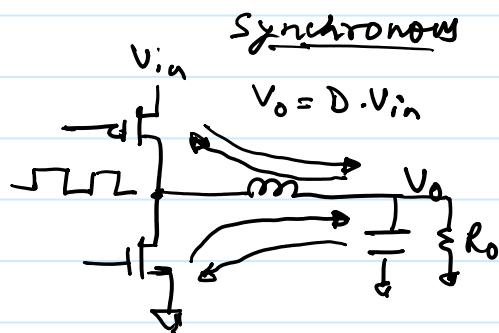


## CCM vs. DCM

CCM → Continuous conduction Mode

DCM → discontinuous " "



$V_{sw} \rightarrow \text{high-Z}$

$V_o = D \cdot V_{in}$  becomes invalid in DCM

$D_1 \rightarrow \text{no f. conductivity}$

## CCM vs. DCM

CCM

# Inductor is always conducting.  
⇒ losses are increased

# Output can be regulated for any load current

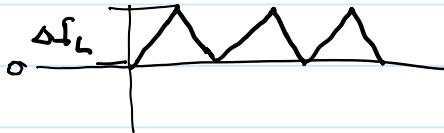
DCM

# inductor stops conducting  $I_o < 0$   
⇒ reduced losses

# output can't be regulated for load current where  $D < D_{min}$   
unless we reduce  $F_{sw}$   
⇒ higher output ripple

# output can't be regulated for  $I_o \leq 0$

## CCM-DCM Boundary Condition



$$I_0 = \frac{\Delta I_L}{2} = \frac{1}{2} \times \frac{V_0 (1-D)}{L} \times T_{SW}$$

$$I_0 = \frac{V_0}{R_0}$$

$$\frac{V_0}{R_0} = \frac{V_0 (1-D) T_{SW}}{2L}$$

$$1-D = \frac{2L}{R_0 T_{SW}} = K$$

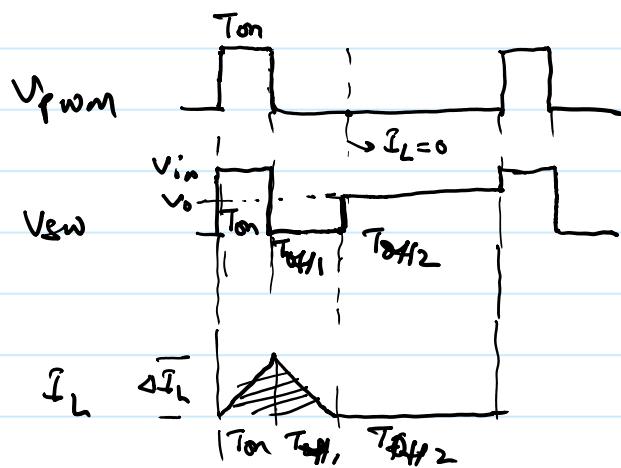
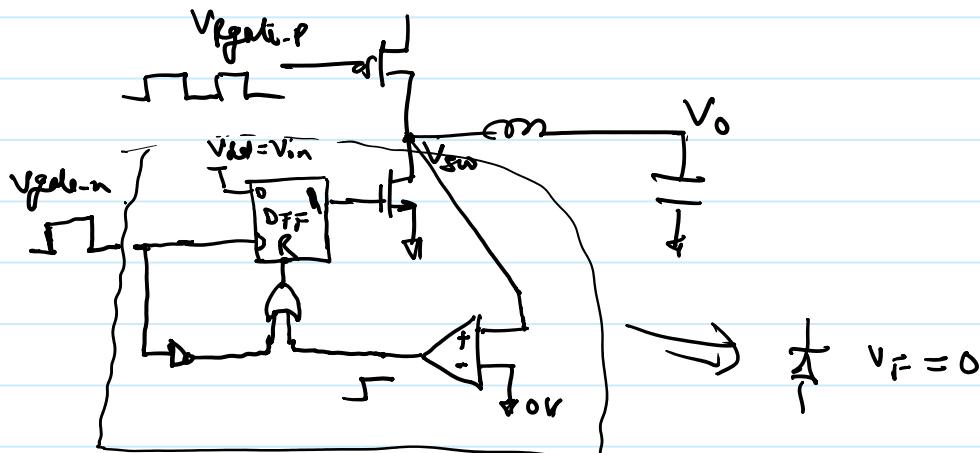
$$1-D = D'$$

$D' > K \rightarrow CCM$

$D' < K \rightarrow DCM$

# DCM Operation

DCM with synchronous buck



$$V_L(\text{avg}) = \frac{(V_{in} - V_o)T_{on} + (-V_o)T_{off}}{T_{sw}} = 0$$

$$V_{in}T_{on} = V_o(T_{on} + T_{off})$$

$$T_{on} + T_{off} = \frac{V_{in}}{V_o} \cdot T_{on} \quad \text{--- (1)}$$

$$I_L(\text{avg}) = \frac{\text{area under } \Delta}{T_{sw}} = \frac{1}{T_{sw}} \times \frac{1}{2} \times (T_{on} + T_{off}) \times \frac{V_{in} - V_o}{L} \cdot T_{on} \quad \text{--- (2)}$$

## Output Regulation in DCM

solve ①  $\rightarrow$  ② and substitute k

$$\frac{V_o}{V_{in}} = \frac{2}{1 + \sqrt{1 + 4K/D^2}}$$

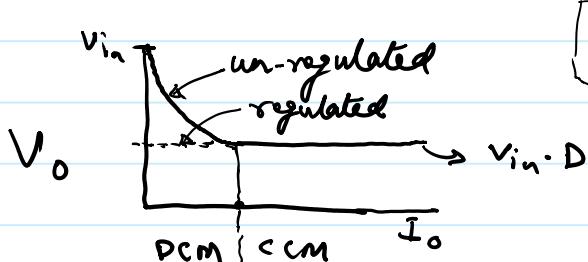
$$K = \frac{2L}{R_o T_{sw}}$$

Valid only for DCM ( $D < K$ )

For regulation  $\frac{V_o}{V_{in}} = \text{const.}$

$$\frac{K}{D^2} = \text{constant}$$

$$K = \frac{2L}{R_o T_{sw}} \Rightarrow \frac{K}{D^2} = \frac{2L}{R_o T_{sw}^2}$$



$R_o \uparrow T_{on} \downarrow$  for regulation

$$T_{on} < T_{on,min}$$

$R_o \uparrow T_{sw} \uparrow$  for regulation

