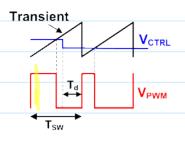
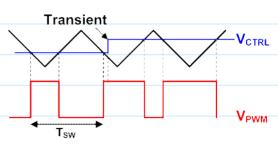
Single Edge vs. Dual Edge PWM



Transient V_{CTRL}



Trailing-Edge PWM

$$T_{d(\max)} = T_{OFF} = (1 - D) \cdot T_{SW}$$

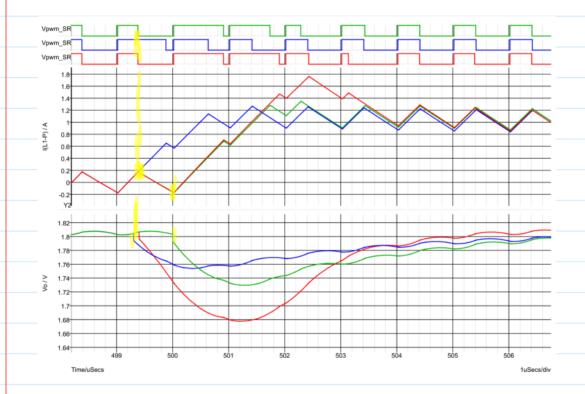
 $T_{d(\max)} \approx T_{SW} \quad for \ D \approx 0$

Leading-Edge PWM

$$\begin{split} T_{d(\text{max})} &= T_{ON} = D \cdot T_{SW} \\ T_{d(\text{max})} &= T_{SW} \text{ for } D \approx 1 \end{split}$$

Dual-Edge PWM

$$T_{d(\max)} = \frac{T_{\text{NB}}}{2}$$





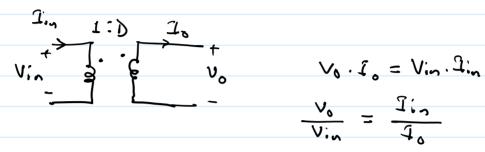
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Transformer Model of Buck Converter

$$V_0 = \delta \cdot V_0^{\circ} n$$

$$V_0 = \delta \cdot V_0^{\circ} n$$

Port = Pin under ideal condition (1=10%)



$$V_0 \cdot I_0 = V_{in} \cdot I_{in}$$

$$\frac{V_0}{V_0} = \frac{I_{in}}{I_0}$$

$$\frac{V_0}{V_{in}} = D \implies \bar{J}_{in} = D.\bar{J}_0$$

$$V_{in} = SV$$
, $V_0 = 2.SV$
 $D = 0.S^-$, $Q_0 = 1A$

$$\frac{V_{o} \gamma = \frac{\rho_{out}}{\rho_{in}} \times 100}{\gamma = \frac{\rho_{out}}{\rho_{in}} = \frac{V_{o} \hat{I}_{o}}{V_{in} \cdot l_{in}}}$$

$$\frac{\sqrt{N}}{\sqrt{N}} = D$$

under winder Loss

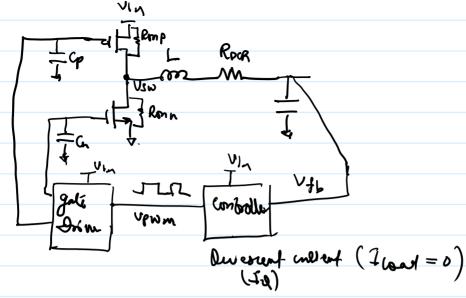
$$V_0 = D.Vin - Vlos$$

$$V_0 = \frac{D.Vin - Volon)I_0}{Vin \times I_0} = \frac{D.Vin I_0 - Vlus I_0}{Vin \times I_0}$$

$$\frac{2 \ln = 0.7_{0}}{0. \text{ Vin } 7_{0} - \text{Viss } 7_{0}} = \sqrt{1 - \frac{\text{Viss}}{0. \text{Vin}}}$$







Plan = conduction or RMS lays or religible lays

(lik) Denductor Dik layor

Switche Rm latter

Switche Rm latter

gate driver Powerfel- dead fimp magnetic

larger switchen layor

(cut) larger layor

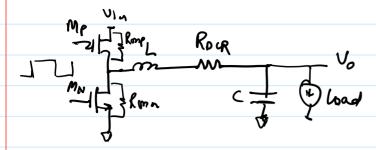
Quiescent Lasser (Ig)

Plans = Pand + Pen + Pa



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Conduction or RMS Loss







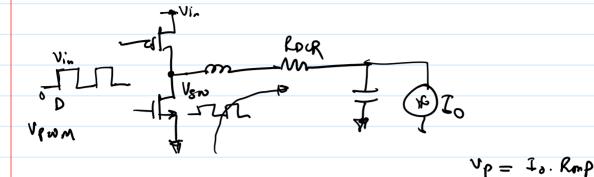
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$$D = 0.2$$

$$0 \cdot \text{Vi}_{n} = \text{V}_{0}$$



Calendating Ron & Rock losses



$$= 0 \cdot (V_{1n} - V_p) + (1-p)(-V_n)$$

Vn = fa - Rom