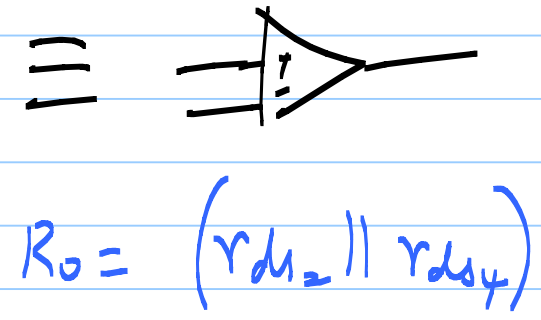
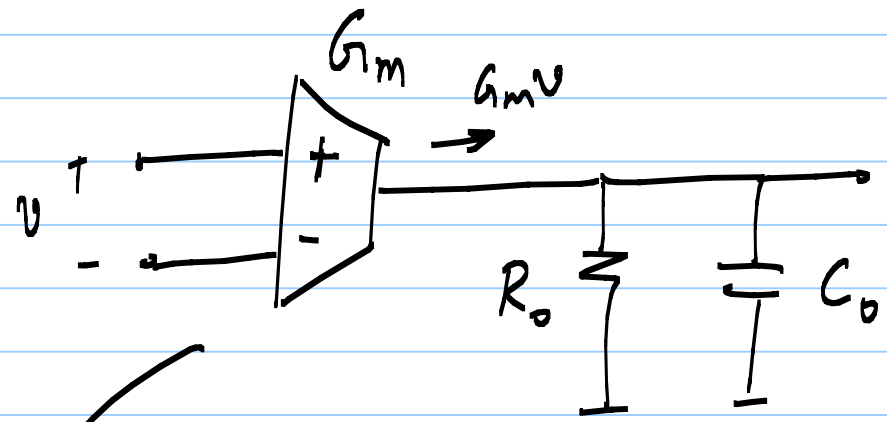
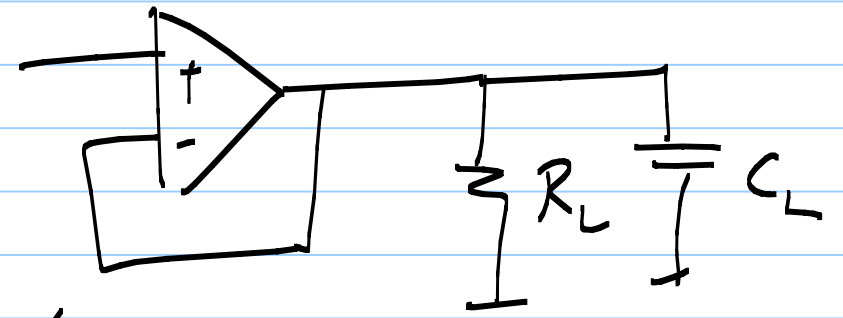


23/10/2020

Lecture 44



$$A_o = G_m R_o$$
$$\omega_d = \frac{1}{R_o C_o}$$
$$\omega_u = \frac{G_m}{C_o}$$



$$A_o' = G_m (R_o || R_L) ; \omega_d' = \frac{1}{(R_o || R_L)(C_o + C_L)}$$
$$\omega_u = G_m / (C_o + C_L)$$

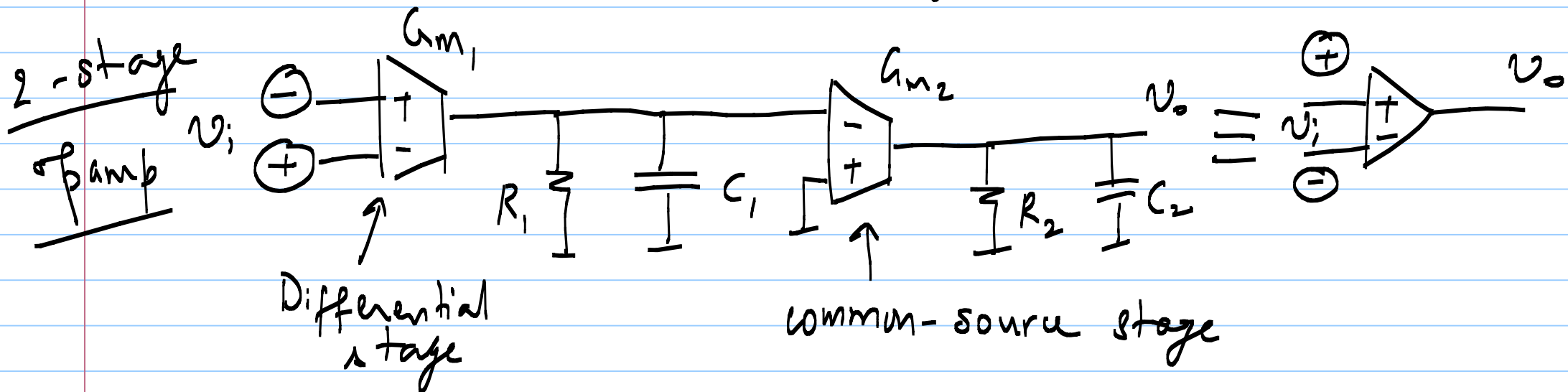
$$R_o \parallel R_L = R_L \parallel r_{ds2} \parallel r_{ds4} \approx R_L$$

$$A_v = g_{m1} (r_{ds2} \parallel r_{ds4})$$

$$A_v' = g_{m1} R_L \quad \text{extremely small compared to } A_v$$

steady state V_e can be large

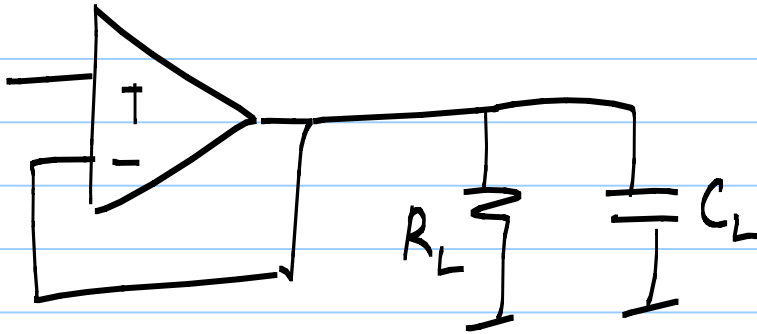
⇒ need a 2-stage opamp



$$A_0 = A_1 \cdot A_2$$

$$= G_{m1} R_1 \cdot G_{m2} R_2$$

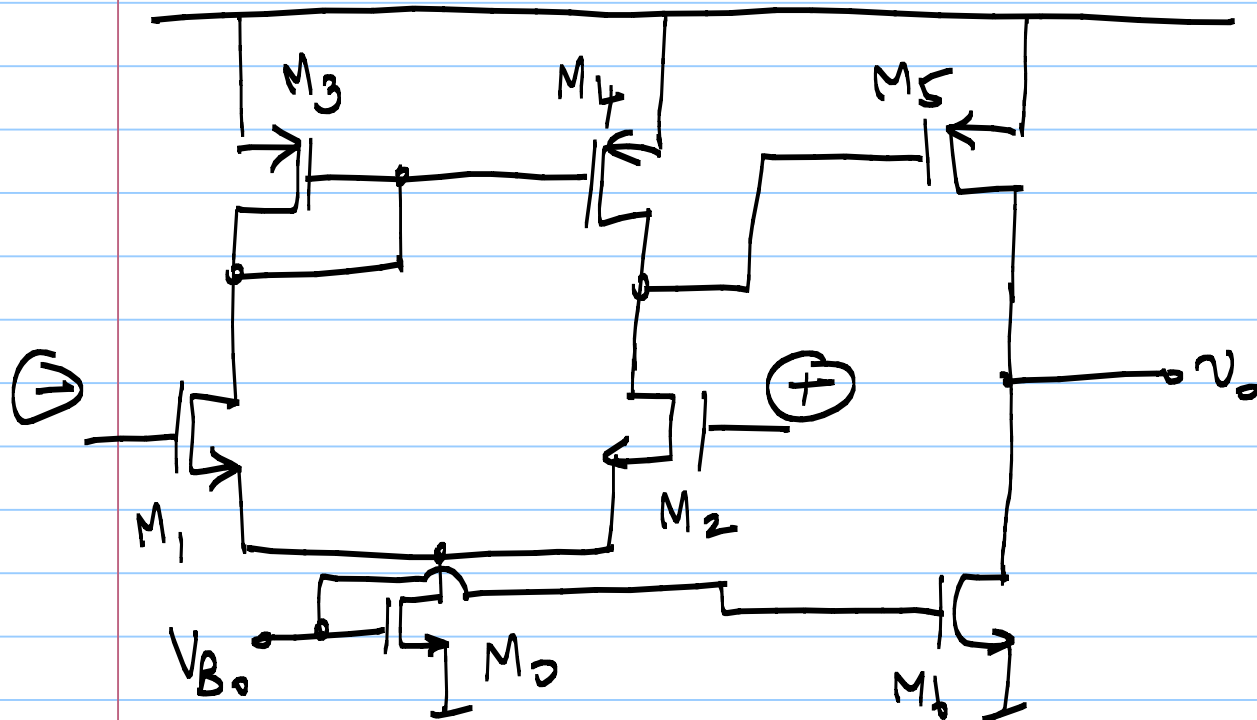
resistive load



$$A_0' = G_{m1} R_1 \cdot G_{m2} (R_L || R_L)$$

$$\approx G_{m1} R_1 \cdot G_{m2} R_L$$

DC gain from
1st stage is preserved



$$G_{m1} = g_{m1}$$

$$G_{m2} = g_{m5}$$

$$R_1 = r_{ds2} || r_{ds4}$$

$$R_2 = r_{ds5} || r_{ds6}$$

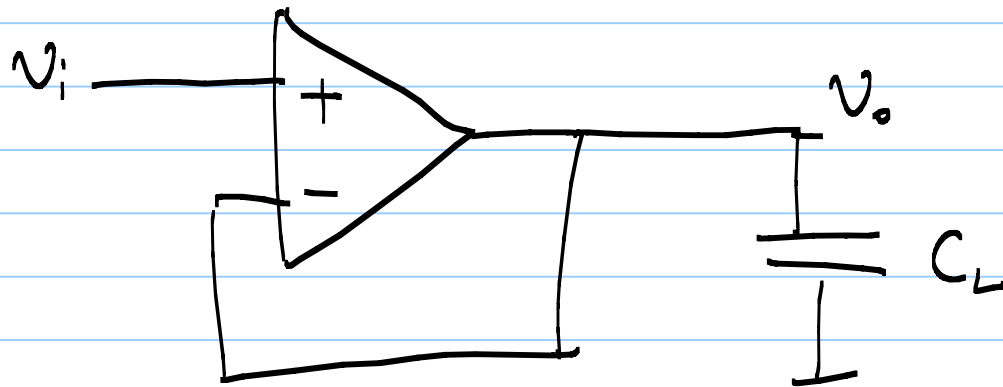
$$C_1 = C_{gs5} + C_{db4} + C_{db2} \approx C_{gs5}$$

$$C_2 = C_{db5} + C_{db6}$$

* \hat{I}_f opamp is driving C_L

check to see
if these are
valid

$$C_2 = C_L + C_{db5} + C_{db6} \approx C_L$$



$$A_1 = A_1(s)$$

$$A_2 = A_2(s)$$

$$A(s) = A_1(s) A_2(s)$$

↳ 2 poles

* How to choose ω_d ?

use PM, but: $PM \geq 60^\circ$

$PM_{min.} = 50^\circ$ etc.

\hookrightarrow sets ω_{dmax}

* As $\omega_d \downarrow \Rightarrow \omega_n \downarrow$

\rightarrow use BW spec. on closed loop amplifier