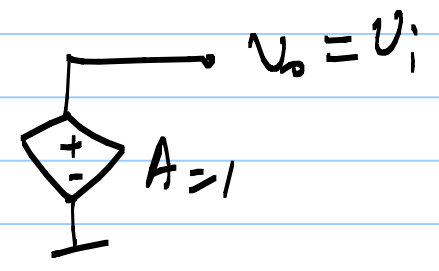
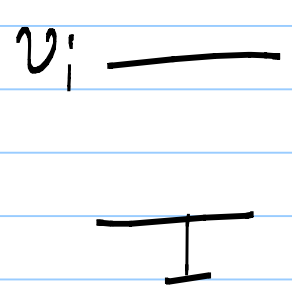
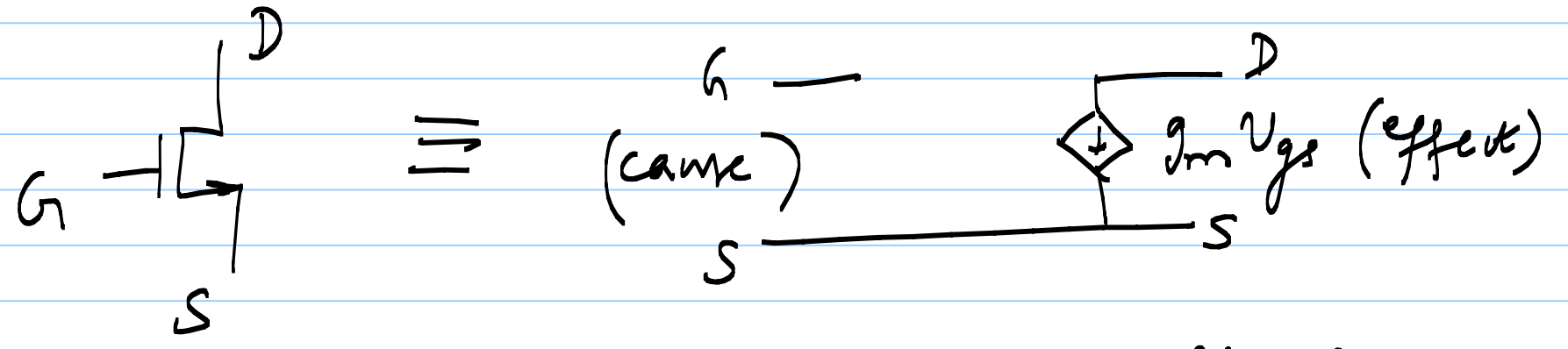


9/9/20

# Lecture 21

MOSFET VCVS, gain = 1,  $v_o = v_i$   
using negative f.b.



$$v_o = v_i$$
$$\Rightarrow \underbrace{v_i - v_o}_{\text{comparison}} = 0$$

use this  $(v_i - v_o)$  ← action  
to change  $v_o$

Sense  $i_d$  or  $i_s$  (relate to  $v_o$ )

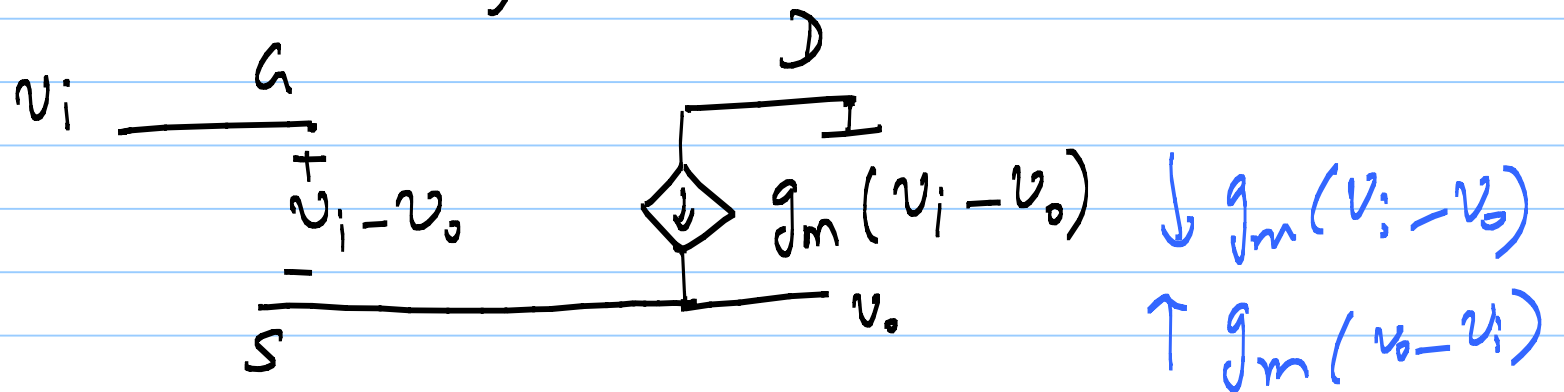
drive back to  $v_{gs}$  (relate to  $v_i - v_o$ )

$i_d, i_s, v_g, v_s$  etc. are small signal quantities

$v_i, v_o \longleftrightarrow v_g, v_s$  (cause)

$v_o \longleftrightarrow v_d, v_s$  (effect  $i_d$  or  $i_s$ )

$$\left. \begin{array}{l} v_o \rightarrow v_s \\ v_i \rightarrow v_g \end{array} \right) v_i - v_o = v_{gs}$$

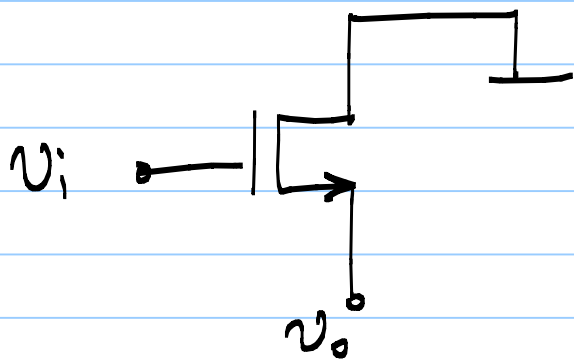


Check for -ve f.b.:

If  $v_o > v_i \Rightarrow g_m (v_o - v_i)$  will flow out of  
Ⓢ node  $\Rightarrow v_o \downarrow$

If  $v_o < v_i \Rightarrow g_m (v_i - v_o)$  will flow into Ⓢ  
node  $\Rightarrow \uparrow v_o$

$v_o = v_i \Rightarrow i_d = 0$

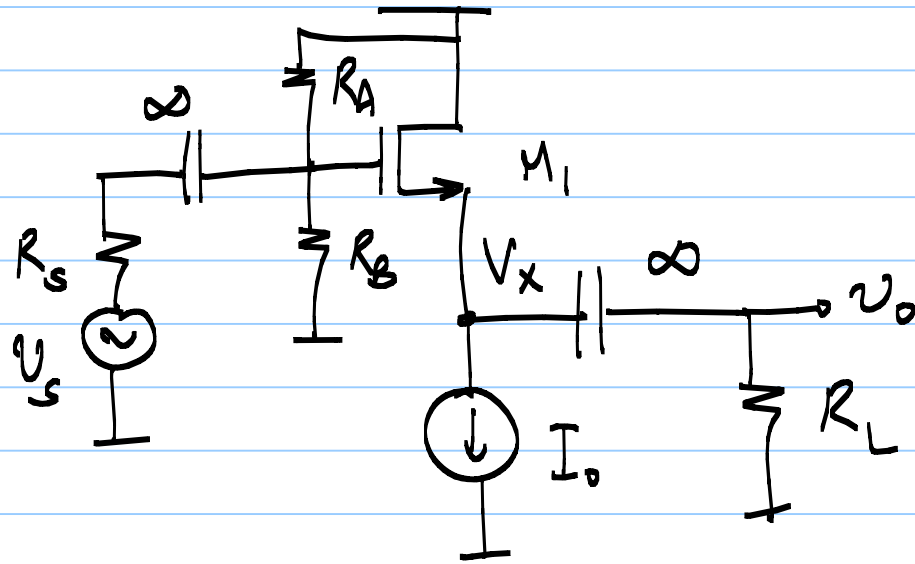


Common Drain Amplifier

# Common Drain Amplifier

(ov)

Source follower



$$V_x = \frac{R_B}{R_A + R_B} V_{DD} - V_T$$

$$= \sqrt{\frac{2I_0}{\mu_n C_{ox} \left(\frac{W}{L}\right)}}$$

- 1) choose large  $R_A, R_B$  (large  $Z_{in}$ )
- 2) As  $g_m \rightarrow \infty$ , gain  $\rightarrow 1$  (gain  $< 1$  if  $R_{ds}$  is significant)
- 3) As  $g_m \rightarrow \infty$ ,  $Z_{out} \rightarrow 0$

$$\frac{v_o}{v_s} = \frac{g_m}{g_m + g_{ds} + G_L}$$

$$g_m \gg G_L$$

$$g_m \gg g_{ds}$$

## Swing limits

$$v_s = V_A \sin \omega t$$

1) Cutoff limit

$$I_D = I_Q + i_d$$

$$= I_0 + i_d$$

assume  $f_{ds}$  is very small

$$i_d = \frac{v_o}{R_L} = \frac{1}{R_L} \cdot \frac{g_m R_L}{1 + g_m R_L} \cdot v_s$$

$$I_D = I_0 + \frac{g_m R_L}{1 + g_m R_L} \cdot \frac{V_A \sin \omega t}{R_L}$$

$$\text{Set } I_D = 0 \Rightarrow V_{A_1} = I_0 \cdot R_L \left[ 1 + \frac{1}{g_m R_L} \right]$$

2) Triode limit

$$V_D - V_S = V_G - V_S - V_T$$
$$V_D = V_G - V_T$$

$$V_{DD} = \frac{V_{DD} \cdot R_B}{R_A + R_B} + V_{A_2} \sin \omega t - V_T$$

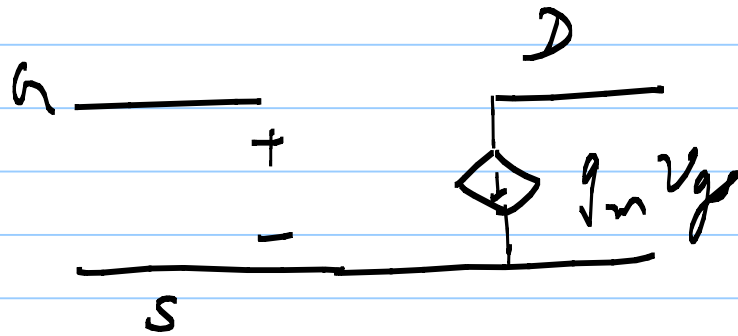
$$V_{A_2} = \frac{R_A}{R_A + R_B} \cdot V_{DD} + V_T$$

$$V_{A_{\max}} = \min. \{ V_{A_1}, V_{A_2} \}$$

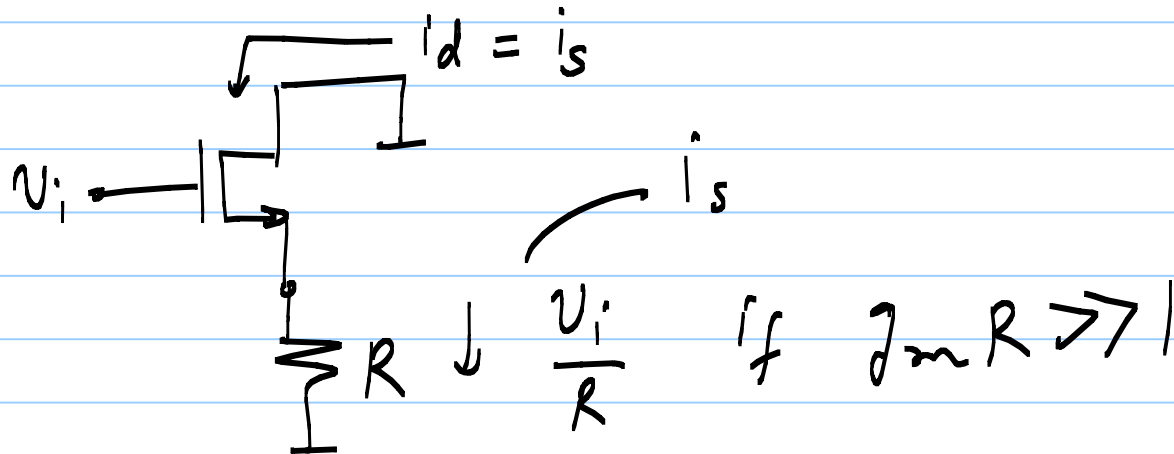
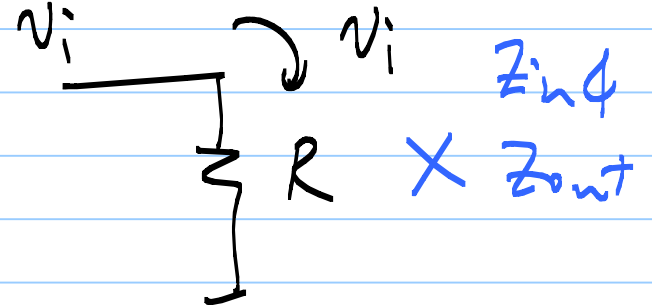
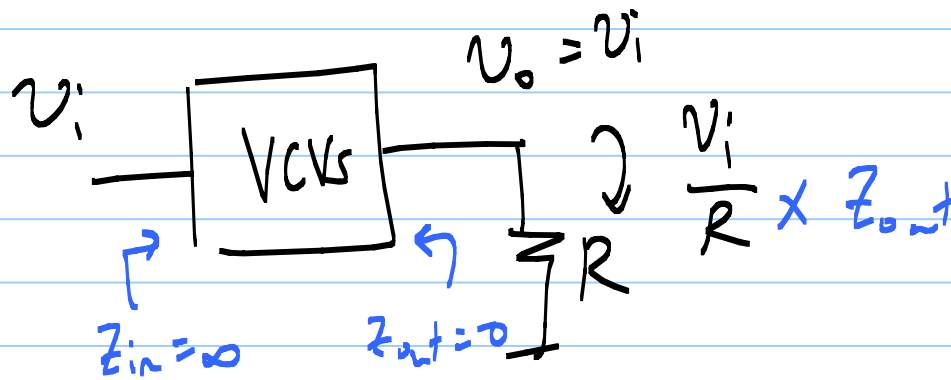
# MOSFET VCCS

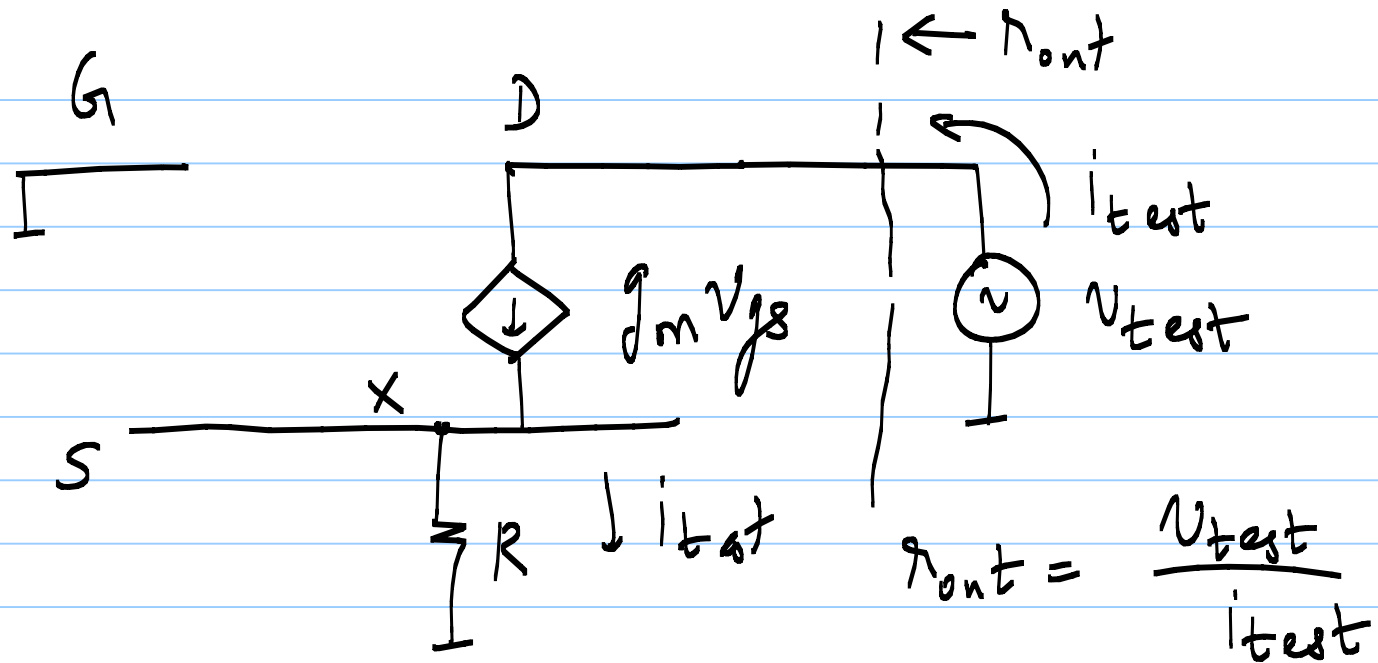
$$i_o = G \cdot v_i = \frac{v_i}{R}, \quad Z_{in} = \infty$$

$$Z_{out} = \infty$$



controlling -  $v_{gs}$   
 controlled -  $i_d$





$$v_x = i_{test} \cdot R$$

$$g_m v_{gs} = -g_m v_x = -g_m R \cdot i_{test} = i_{test}$$

$$i_{test} = 0 \Rightarrow Z_{out} = \infty$$

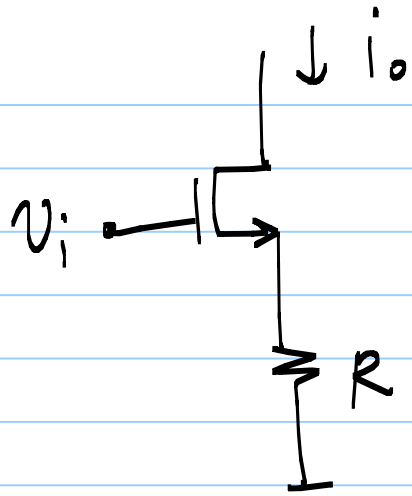
HW

#6

Calculate  $Z_{out}$  if  $r_{ds}$  is finite

$$Z_{out} = r_{ds} + g_m R r_{ds} + R$$





Trans admittance  
amplifier

