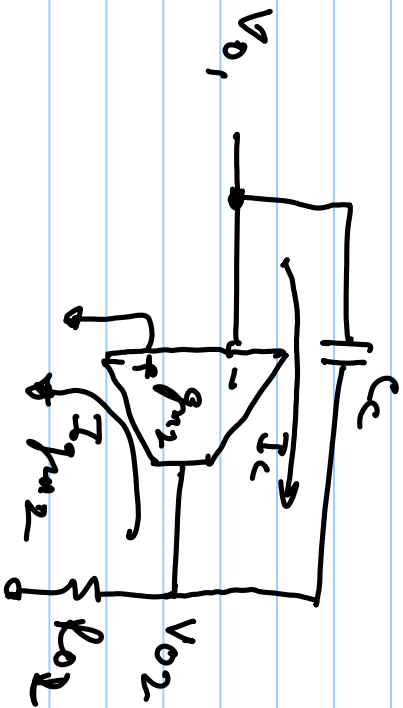
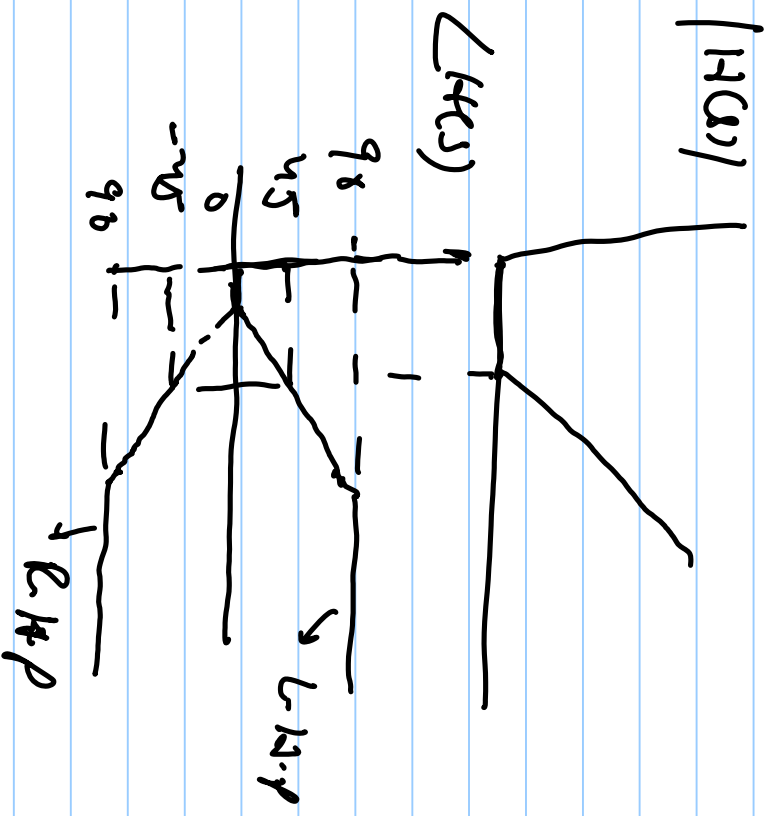


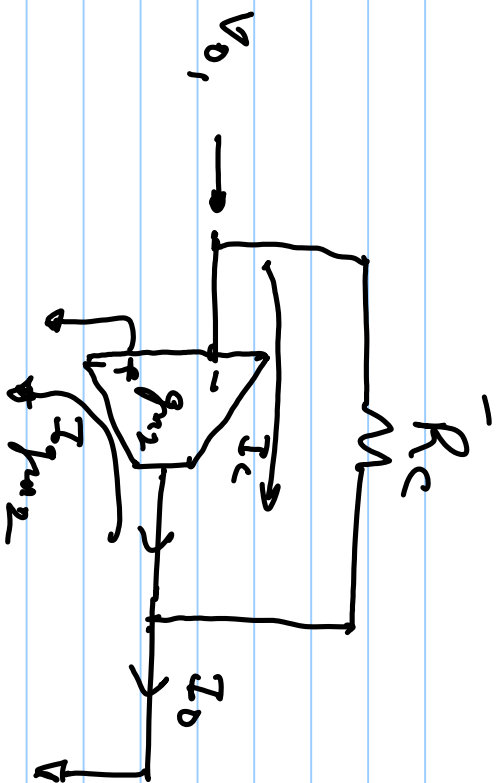
$$\omega_{P1} = \frac{1}{(g_{m2} R_{o2}) R_{o1} C_c}$$

$$\omega_{P2} = \frac{g_{m2}}{C_{o1} + C_{o2}}$$



$$H(s) = (1 + R_2 s)$$

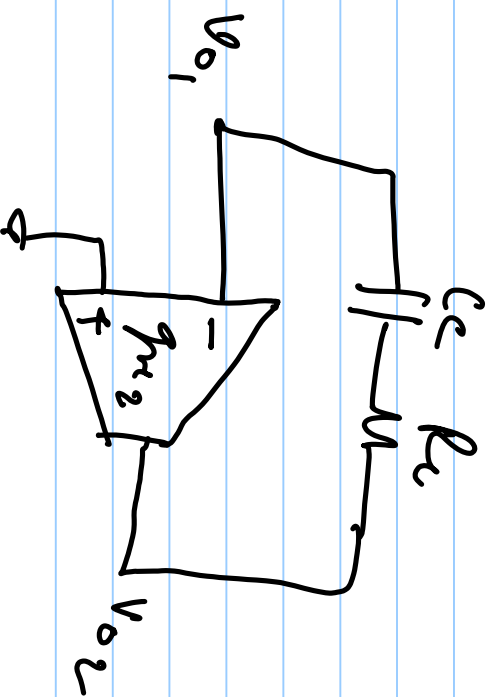




$$-V_{o1} g_{m2} * V_{o1} / R_c = 0$$

$$R_c > \frac{1}{g_{m2}}$$

g_{m2} path will always be stronger than R_c path



$$\omega_2 = \frac{g_{m3}}{c_c} \quad \text{with out } R_c$$

with R_c

$$\omega_2 = \frac{-1}{(R_c - \frac{1}{g_{m2}}) c_c}$$

$R_c \gg \frac{1}{g_{m2}}$ then ω_2 will be in R.17. p

$$R_c = \frac{1}{g_{m2}}, \quad \omega_2 \rightarrow \infty$$

$$\frac{V_{O2}}{V_{O1}} = \frac{A_0 \left[1 + \left(R_c - \frac{1}{g_{m2}} \right) s \right]}{(1 + s/\omega_{p1}) (1 + s/\omega_{p2})}$$

if $R_c > \frac{1}{g_{m2}}$ then R.H.P zero moves to L.H.P.

$$\omega_z = \omega_{p2}, \quad \omega_z = \frac{-1}{\left(R_c - \frac{1}{g_{m2}} \right) C_c}$$

$$H(s) = \frac{A_0}{(1 + s/\omega_{p1})}$$

pole-zero cancellation

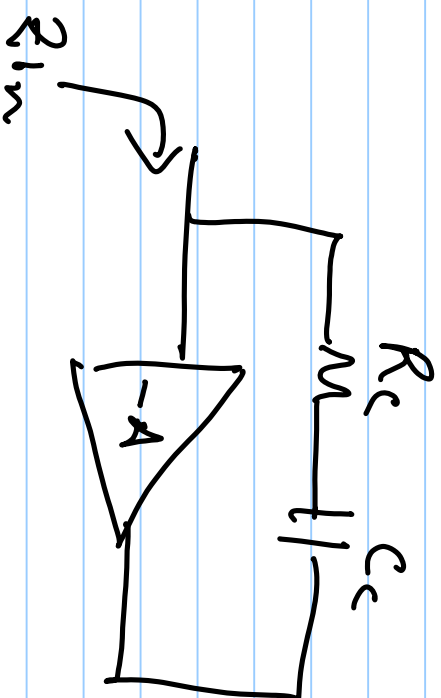
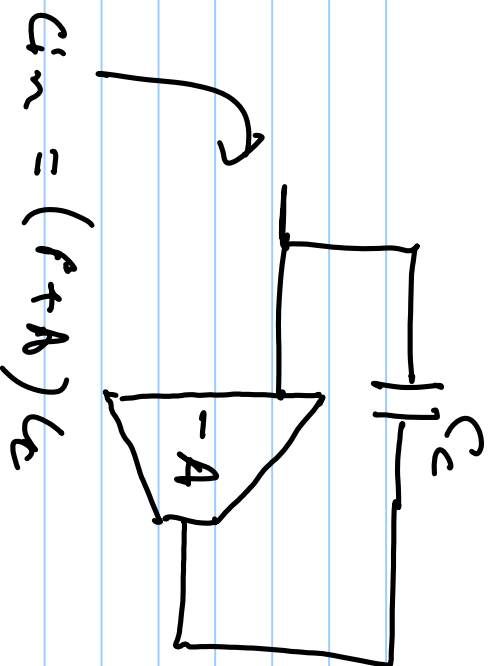
ω_z cancels ω_{p2}

We can design a higher B.W. amplifier by cancelling 2nd pole.

$$w_{p2} = \frac{g_{m2}}{C_{01} + C_{02}}, \quad w_{z2} = \frac{1}{(R_c - \frac{1}{g_{m2}}) C_c}$$

$$\frac{g_{m2}}{C_{01} + C_{02}} = \frac{g_{m2}}{(R_c g_{m2} - 1) C_c}$$

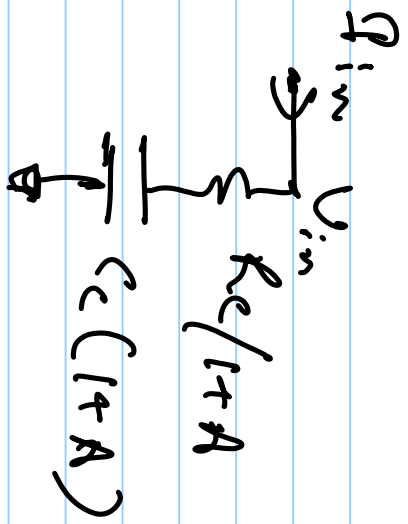
$$1 + \frac{C_{01} + C_{02}}{C_c} = R_c g_{m2} \Rightarrow R_c = \frac{1}{g_{m2}} \left(1 + \frac{C_{01} + C_{02}}{C_c} \right)$$



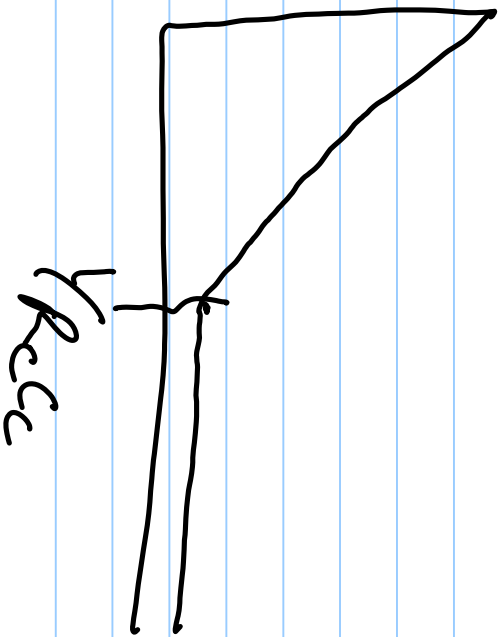
$$R_{in} = \frac{1}{1+A} \left(R_c + \frac{1}{sC_c} \right) = \left(\frac{R_c}{1+A} + \frac{1}{(1+A)Cs} \right)$$

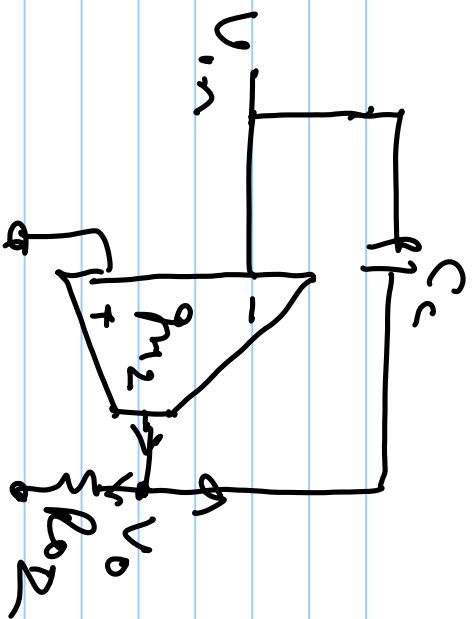
$$R_{in} \approx \frac{1}{(1+A)Cs} \Rightarrow C_{in} = (1+A)C_c$$

small



$$V_{in} = I_{in} \left(\frac{R_e}{1+A} + \frac{1}{C_c(1+A)s} \right)$$



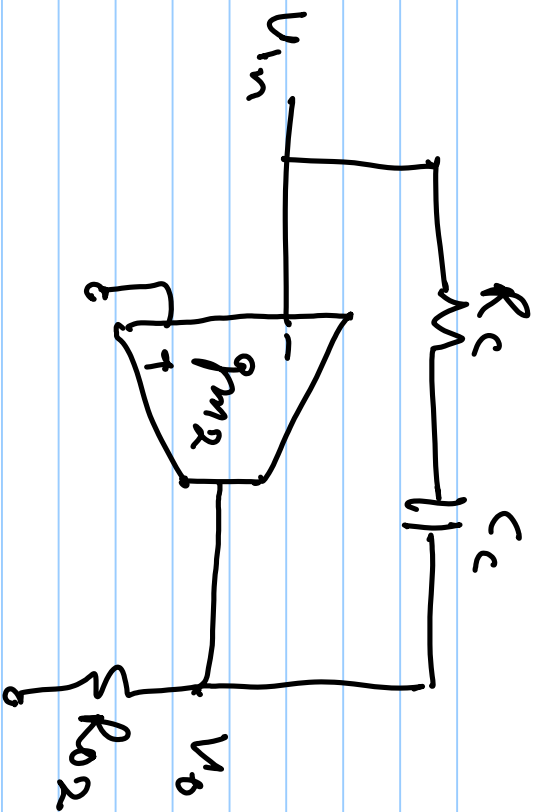


$$(V_o - V_{in})g_c + \frac{V_o}{R_{o2}} = -V_{in}g_{m2}$$

$$V_o g_c - V_{in} g_c + \frac{V_o}{R_{o2}} = -V_{in} g_{m2}$$

$$V_o \left(g_c + \frac{1}{R_{o2}} \right) = V_{in} (-g_{m2} + g_c)$$

$$\frac{V_o}{V_{in}} = \frac{-R_{o2} g_{m2} \cdot \left(1 - \frac{g_c}{g_{m2}} \right)}{1 + R_{o2} g_c}$$



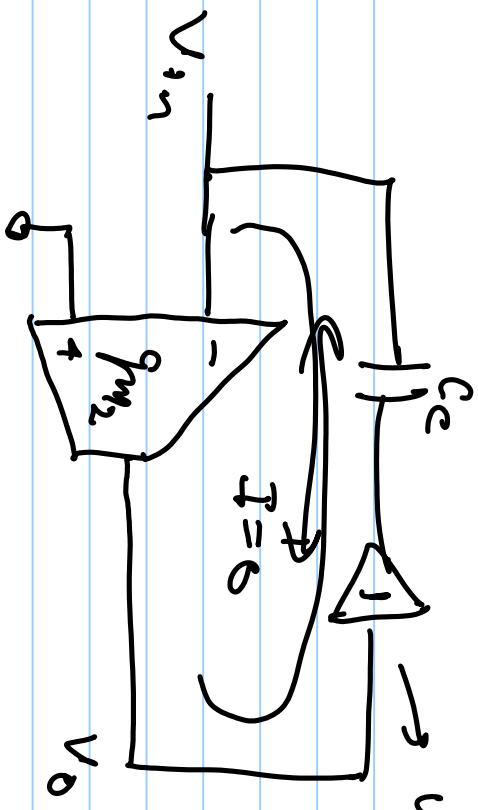
$$-V_{in} g_{m2} = \frac{V_o}{R_{o2}} + \frac{(V_o - V_{in})}{R_e + \frac{1}{g_{ec}}}$$

$$-V_{in} g_{m2} = \frac{V_o}{R_{o2}} + \frac{V_o g_{ec}}{1 + R_e g_{ec}} - \frac{V_{in} g_{ec}}{1 + R_e g_{ec}}$$

$$-V_{in} \left(g_{m2} - \frac{g_c c_s}{1 + R_c c_s} \right) = V_o \left(\frac{1}{R_{o2}} + \frac{g_c c_s}{1 + R_c c_s} \right)$$

$$-V_{in} \left(\frac{g_{m2} (1 + R_c c_s) - g_c c_s}{(1 + R_c c_s)} \right) = V_o \frac{1 + R_c c_s + R_{o2} c_s}{R_{o2} (1 + R_c c_s)}$$

$$\begin{aligned} \frac{V_o}{V_{in}} &= \frac{g_{m2} R_{o2} \left(1 + R_c c_s - \frac{c_s}{g_{m2}} \right)}{1 + (R_c + R_{o2}) c_s} \\ &= -g_{m2} R_{o2} \left[1 + \left(R_c - \frac{1}{g_{m2}} \right) c_s \right] / \left[1 + (R_c + R_{o2}) c_s \right] \end{aligned}$$



unity gain buffer